# Interchange Justification Report for <br> I-75 (SR 93) Interchange at NW 49 ${ }^{\text {th }}$ Street Project Development \& Environment Study Marion County, Florida 

Financial Project ID: 435209-1-22-01

Florida Department of Transportation
District Five

## Interchange Justification Report (IJR)

I-75 (SR 93) Interchange at NW 49th Street PD\&E Study
FPID: 435209-1-22-01

## Florida Department of Transportation Determination of Safety, Operational and Engineering Acceptability

Acceptance of this document indicates successful completion of the review and determination of safety, operational and engineering acceptability of the Interchange Access Request. Approval of the access request is contingent upon compliance with applicable Federal requirements, specifically the National Environmental Policy Act (NEPA) or Department's Project Development and Environment (PD\&E) Procedures. Completion of the NEPA/PD\&E process is considered approval of the project location design concept described in the environmental document.

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## PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am a registered professional engineer in the State of Florida practicing with Metric Engineering, Inc., authorized under the provisions of Section 471.023, Florida Statutes, to offer engineering services to the public through a Professional Engineer, duly licensed under Chapter 471, Florida Statutes, Certificate of Authorization (CA) No. 2294, by the State of Florida Department of Professional Regulation, Board of Professional Engineers, and that I have prepared or approved the evaluation, findings, opinions, conclusions, or technical advice hereby reported for:

Financial Project Number: 435209-1-22-01
Federal Aid Number: N/A

Project: I-75 (SR 93) Interchange at NW 49 ${ }^{\text {th }}$ Street PD\&E Study Interchange Justification Report (IJR)
County: Marion

I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of transportation engineering as applied through professional judgment and experience.

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# QUALITY CONTROL CERTIFICATION FOR INTERCHANGE ACCESS REQUEST SUBMITTAL 

Submittal Date: 01/08/2021

FM Number: 435209-1-22-01

Project Title: I-75 (SR 93) Interchange at NW 49th Street PD\&E Study Interchange Justification Report

District: Five

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## Quality Control (QC) Statement

This document has been prepared following FDOT Procedure Topic No. 525-030-160 (New or Modified Interchanges) and complies with the FHWA two policy requirements. Appropriate District level quality control reviews have been conducted and all comments and issues have been resolved to their satisfaction. A record of all comments and responses provided during QC review is available in the project file or Electronic Review Comments (ERC) system.

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## 1 Executive Summary

### 1.1 Introduction

This Interchange Justification Report (IJR) is being conducted on behalf of the Florida Department of Transportation (FDOT) as part of the I-75 at NW 49 ${ }^{\text {th }}$ Street Project Development \& Environment (PD\&E) Study for a new interchange on Interstate 75 (I-75) along the proposed extension of NW 49 ${ }^{\text {th }}$ Street in Marion County, Florida. This IJR follows a previously approved IJR completed in 2016 on behalf of Marion County. The 2016 IJR evaluated the No Build and Urban Diamond Interchange alternatives. This new IJR is being developed as part of the I-75 at NW 49 ${ }^{\text {th }}$ Street PD\&E Study which updates the traffic forecasting and evaluates additional alternatives. Figure 1-1 shows the project location and Area of Influence (AOI). The proposed interchange is needed to support the economic viability of the Ocala 489, a 489 acre industrial and commercial development, and contiguous commerce district/employment center. This commerce park is composed of a recently constructed FedEx Ground Distribution Hub; Chewy distribution center; an AutoZone distribution center, designated as a CSX Select Site; the Florida Crossroads Logistics Center, a Red Rock Development; and the remaining undeveloped sites. Development in this area will result in traffic volume increases along I-75 and the entire local roadway network; adding a projected $25,000+$ daily trips to the roadway network upon fullbuildout, $12 \%$, or 3,000 vehicles of which are projected to be trucks.

### 1.2 Project Purpose and Need

The purpose of a new I-75 interchange at NW $49^{\text {th }} / 35^{\text {th }}$ Street is to provide relief to the congestion and operational deficiencies at both existing contiguous I-75 interchanges, by providing an alternate access to I-75 for the projected increase in truck volumes resulting from the future commerce district. The need for an interchange at I-75 and NW 49 ${ }^{\text {th }}$ Street can be summarized into four (4) different discussion areas:

- Economic Viability and Job Creation: The proposed interchange is needed to support the economic viability of the Ocala 489, which is intended to serve as an economic engine for job creation in the region and is envisioned as a strategic central inland hub for freightrelated traffic.
- Improve Interstate and Regional Mobility: The proposed interchange is needed to provide a more direct and efficient access to I-75 thus facilitating interstate and regional mobility. In particular, the interchange is needed to serve the "long haul" trips associated
with the Ocala 489. From a regional perspective, Marion County is approximately midway between Miami and Atlanta and occupies a strategic location due to its relative proximity to other important metropolitan areas. The proposed interchange is thus needed to support the efficient movements of goods.
- Address Locally Supported Long Term Regional Needs: The proposed project is needed to provide important access to I-75 as part of a locally supported long range vision to develop an east-west corridor parallel to US 27 and SR 326.
- Accommodate Future Traffic Growth: The proposed interchange is needed to accommodate projected future year traffic volumes. Marion County has experienced a significant and sustained growth in population since 1970. It is projected that build-out in design year 2045 will add 25,000 daily trips to the roadway network with approximately $12 \%$, or 3,000 vehicles, of which are projected to be trucks. As a result of this growth, traffic volumes are increasing and will continue to increase in the future.

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Figure 1-1: Project Location and Area of Influence
1.3 Qualifying Provisions

Via a Programmatic Agreement between the Federal Highway Administration (FHWA) and FDOT, the I-75 at NW 49 ${ }^{\text {th }}$ Street IJR will be reviewed for approval by FDOT. Per the Methodology Letter of Understanding (MLOU) along with the MLOU Amendment, and consistent with the 2020 FDOT Interchange Access Request User's Guide (IARUG), this document follows the two FHWA policy requirements. Therefore, the following specific evaluation criteria, termed FHWA's Policy Requirements, serve as the basis for review and approval of the proposed project as documented in the 2020 IARUG.

1. An operational and safety analysis has concluded that the proposed change in access does not have a significant adverse impact on the safety and operation of the interstate facility (which includes mainline lanes, existing, new or modified ramps, ramp intersections with crossroads) or on the local street network based on both the current and the planned future traffic projections. The analysis shall, particularly in urbanized areas, include at least the first adjacent existing or proposed interchange on either side of the proposed change in access (23 CFR 625.2(a), 655.603(d) and 771.111(f)). The crossroads and the local street network, to at least the first major intersection on either side of the proposed change in access, shall be included in this analysis to the extent necessary to fully evaluate the safety and operational impacts that the proposed change in access and other transportation improvements may have on the local street network (23 CFR 625.2(a) and 655.603(d)). Requests for a proposed change in access must include a description and assessment of the impacts and ability of the proposed changes to safely and efficiently collect, distribute and accommodate traffic on the interstate facility, ramps, intersection of ramps with crossroad and local street network (23 CFR 625.2(a) and 655.603(d)). Each request also must include a conceptual plan of the type and location of the signs proposed to support each design alternative (23 U.S.C. 109(d) and 23 CFR 655.603(d)).

A traffic operational analysis was conducted as part of this study. The analysis was performed for the AM and PM peak hours using the methodologies documented in the Highway Capacity Manual (HCM) 2010 as applied using the Highway Capacity Software (HCS) 6.8, Synchro 10 and Vissim 2020.00-07.

The operational analysis provided a performance evaluation for each individual element within the system (for example freeway segments, freeway ramp junctions, crossroad ramp terminals and other crossroad intersections). The analysis indicated that the proposed Diverging Diamond

Interchange (DDI) is the recommended alternative and is not projected to have a significant adverse impact on operations along the I-75 mainline system or the existing adjacent interchanges within the study limits.

Figures 1-2 and 1-3 present the segmented breakdown of the I-75 mainline and interchange ramps under the No Build and DDI alternatives; along with the summarized results for the 2045 AM segment and merge/diverge analysis. The differences between No Build and the DDI alternatives are as follow:
o 2045 AM Northbound:

- No Build conditions
- I-75 south of US 27 including the off-ramp diverge operates at Level of Services (LOS) F and the basic segment between US 27 and SR 326, operates at LOS E.
- Build conditions
- Similar to No Build, I-75 south of US 27 operates at LOS F.
- Shifts in travel patterns reflect the use of I-75 as a by-pass between US 27 and NW 49 ${ }^{\text {th }}$ Street. Under No Build, for segment densities that are close to the LOS D maximum threshold of $35 \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$; the shift in traffic from improved connectivity corresponds to a minimal density increase resulting in LOS E segments under Build.
- North of US 27 interchange, through the NW 49 ${ }^{\text {th }}$ Street interchange LOS are the same or better than under No Build.
- SR 326 diverge segment, the minimal increase in density is at the $35 \mathrm{pc} / \mathrm{mi} / \mathrm{In}$ LOS D target threshold.


## o 2045 AM Southbound:

- No Build conditions
- I-75 south of US 27 including the on-ramp merge operates at LOS E.
- Build conditions
- I-75 at the US 27 on-ramp merge condition; the traffic pattern shift from improved connectivity creates a slight increase in density where the LOS E threshold is exceeded.
- All remaining locations meet the LOS D target.

Figures 1-4 and 1-5 present the 2045 PM segment and merge/diverge analysis results for the No Build and DDI alternatives. Along with the directional peak change, the shifts in travel patterns, reflecting decreases and increases in traffic are similar to those observed for the AM.

Figure 1-2: No Build 2045 AM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 1-3: DDI Alternative 2045 AM I-75 Segment \& Merge/Diverge Analysis Summary

| dDI2045 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Distance (tt) |  |  | 1,500 | 3,168 | 1,500 | 3,676 | 1,500 | 7,530 | 1,500 | 2,307 | 1,500 | 380 | 1,500 | 1,815 | 1,500 |  |
|  | Accel/Decel Lanes (tt) |  | 800 | N/A | 616 |  | 1,010 | N/A | 580 |  | 1,073 | N/A | 1,500 | N/A | 268 |  |
|  | Speed (mph) | 53.4 | 53.4 | 63.5 | 64.8 | 61.0 | 59.5 | 66.9 | 64.5 | 64.9 | 63.2 | 69.0 | 63.1 | 73.7 | 67.9 | 72.1 |
|  | Los | E | F | D | D | D | D | c | D | D | c | c | c | c | c | c |
|  | Density ( $\mathrm{p} / \mathrm{mi} / \mathrm{ln}$ ) | 44.9 | 37.8 | 30.6 | 31.6 | 34.1 | 31.5 | 25.7 | 29.4 | 28.7 | 26.4 | 25.2 | 24.7 | 18.2 | 27.9 | 20.9 |
|  | segment Type | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic |
|  | Truck\% | 11.0 | 14.0 | 11.0 | 6.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 23.0 | 12.0 | 23.0 | 12.0 | 23.0 | 10.0 |
|  |  |  |  | $\geqslant$ |  |  |  | $\mathbb{R}: 1$ |  |  |  | E/ |  |  |  |  |
|  |  |  |  | $\leftarrow$ |  |  |  | $\leftarrow$ |  |  |  | $\leftarrow$ |  |  |  |  |
|  |  |  |  | $\ldots$ |  |  |  | $\cdots$ |  |  |  |  | - |  |  |  |
|  |  |  |  | $\longleftarrow$ |  |  |  | $\longleftarrow$ |  |  |  | , | - |  |  |  |
|  | Volumes |  | 5,825 | 1,092 | 4,733 | 306 | 5,039 | 883 | 4,156 | 351 | 4,507 | 307 | 4,200 | 959 | 3,241 | 442 | 3,683 |
|  |  |  | us 27 |  |  |  | NW 49 Street |  |  |  |  | SR326 |  |  |  |  |  |
| $\begin{aligned} & \substack{0 \\ \underline{n} \\ \underline{n}} \end{aligned}$ | Volumes | 6.501 | 1,043 | 5,458 | 335 | 5,793 | 746 | 5,047 | 415 | 5,462 | 1,250 |  | 4,212 | 726 |  | 338 |
|  |  |  |  | $\longrightarrow$ |  |  |  | $\rightarrow$ |  |  |  |  |  |  |  |  |
|  |  |  |  | $\longrightarrow$ |  |  |  | $\longrightarrow$ |  |  |  | $\cdots$ |  |  |  |  |
|  |  |  |  | $\longrightarrow$ |  |  |  | $\longrightarrow$ |  |  |  | $\square$ |  |  |  |  |
|  |  |  |  | $\pi$ |  |  |  | $1 \text { 可 }$ |  |  |  |  | Y |  | - | - |
|  | Truck\% | 11.0 | 14.0 | 11.0 | 6.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 23.0 |  | 12.0 | 23.0 |  |  |
|  | Segment type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge |  | Basic | Merge |  | sic |
|  | Distance (tt) |  | 1,500 | 3,029 | 1,500 | 1,585 | 1,500 | 10,173 | 1,500 | 1,900 | 1,500 |  | 2,809 | 1,500 |  |  |
|  | Accel/Decel Lanes (tt) |  | 671 | N/A | 847 | 3,247 | 491 | N/A | 1,057 | 3,172 | 671 |  | N/A | 941 |  |  |
|  | Speed (mph) | 44.8 | 60.5 | 57.3 | 56.4 | 53.5 | 63.3 | 60.9 | 54.7 | 57.0 | 62.0 |  | 68.9 | 61.1 |  | 3.5 |
|  | Los | F | f | E | E | E | E | - | E | E | E |  | c | D |  |  |
|  | Density (pc/mi/n) | 59.7 | 44.0 | 39.2 | 35.9 | 44.8 | 38.4 | 34.3 | 36.0 | 39.6 | 35.0 |  | 25.3 | 30.9 |  | 1.8 |

Figure 1－4：No Build 2045 PM I－75 Segment \＆Merge／Diverge Analysis Summary


Figure 1－5：DDI Alternative 2045 PM I－75 Segment \＆Merge／Diverge Analysis Summary

| DDI 2045 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Distance（tt） |  | 1，500 | 3，168 | 1，500 | 3，676 | 1，500 | 7，530 | 1，500 | 2，307 | 1，500 | 380 | 1，500 | 1，815 | 1，500 |  |
|  | Accel／Decel Lanes（tt） |  | 800 | N／A | 616 |  | 1，010 | N／A | 580 |  | 1，073 | N／A | 1，500 | n／A | 268 |  |
|  | Speed（mph） | 43.0 | 42.9 | 57.4 | 64.3 | 53.6 | 55.4 | 61.0 | 64.0 | 57.2 | 59.6 | 60.9 | 58.7 | 69.1 | 67.5 | 65.6 |
|  | os | F | F | E | E | E | E | D | D | E | D | D | D | c | D | D |
|  | Density（pc／mi／n） | 63.3 | 42.3 | 39.1 | 37.1 | 44.6 | 35.4 | 34.1 | 33.9 | 39.4 | 31.9 | 35.0 | 30.4 | 25.0 | 33.2 | 29.3 |
|  | Segment Type | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic |
| 告 | Truck\％ | 11.0 | 14.0 | 11.0 | 6.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 23.0 | 12.0 | 23.0 | 12.0 | 23.0 | 10.0 |
| $\left\|\begin{array}{l} \stackrel{\rightharpoonup}{\mathbf{u}} \\ \stackrel{\rightharpoonup}{n} \\ \underline{-} \end{array}\right\|$ |  |  |  | $E \geqslant$ |  |  |  | $k \geqslant$ |  |  |  | ＋ | $\square$ |  |  |  |
|  |  | $\square$ |  | $\leftarrow$ |  |  |  | $\leftarrow$ |  |  |  |  |  |  |  |  |
|  |  |  |  | $\longleftarrow$ |  |  |  | － |  |  |  |  |  |  |  |  |
|  |  |  |  | － |  |  |  | $\leftarrow$ |  |  |  | $\leftarrow$ |  |  |  |  |
|  | Volumes | 6，626 | 1，175 | 5，451 | 330 | 5，781 | 746 | 5，035 | 415 | 5，450 | 299 | 5，151 | 967 | 4，184 | 506 | 4，690 |
|  | Interchange |  |  | Us 27 |  |  |  | NW | Street |  |  |  |  | S 326 |  |  |
|  | Volumes | 5，996 | 1，110 | 4，686 | 346 | 5，032 | 883 | 4，149 | 351 | 4，500 | 1.340 |  | 160 | 707 |  | 67 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | $\longrightarrow$ |  |  |  | $\longrightarrow$ |  |  |  | － |  |  |  |  |
|  |  |  |  | $\longrightarrow$ |  |  |  | $\longrightarrow$ |  |  |  |  |  |  |  |  |
|  |  |  |  | $N .$ |  |  |  | N 友 |  |  |  |  | 多 | $\square$ |  |  |
| $\begin{aligned} & \overline{5} \\ & \stackrel{y}{2} \end{aligned}$ | Truck\％ | 11.0 | 14.0 | 11.0 | 6.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 23.0 |  | 2.0 | 23.0 |  |  |
| $\stackrel{4}{2}$ | Segment Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge |  | asic | Merge |  | sic |
|  | Distance（ft） |  | 1，500 | 3，029 | 1，500 | 1，585 | 1，500 | 10，173 | 1，500 | 1，900 | 1，500 |  | 809 | 1，500 |  |  |
|  | Accel／Decel Lanes（tt） |  | 671 | N／A | 847 | 3，247 | 491 | N／A | 1，057 | 3，172 | 671 |  | N／A | 941 |  |  |
|  | Speed（mph） | 53.7 | 60.9 | 63.9 | 60.2 | 61.0 | 63.2 | 66.9 | 46.2 | 64.9 | 62.1 |  | 4.0 | 64.3 |  |  |
|  | cos | E | E | D | D | D | D | c | E | D | D |  | в | c |  |  |
|  | Density（pc／mi／n） | 44.4 | 36.5 | 30.2 | 32.0 | 34.1 | 33.7 | 25.6 | 38.8 | 28.6 | 31.0 |  | 7.7 | 24.8 |  |  |

The differences between the No Build and DDI alternatives under 2045 PM are as follow:
o 2045 PM Northbound:

- No Build conditions
- I-75 mainline segment south of US 27 operates at LOS E.
- All remaining locations meet the LOS D target.
- Build conditions
- For the US 27 off-ramp diverge; shift in travel pattern from improved connectivity corresponds to a minimal increase in density where the LOS D target threshold is exceeded at LOS E.
- The NW 49 ${ }^{\text {th }}$ Street on-ramp merge operates at LOS E; both adjacent mainline segments meet the LOS D target.
- Remaining northbound segments meet the LOS D target.


## o 2045 PM Southbound:

- No Build conditions
- I-75 on-ramp merge from US 27 and adjacent mainline segment operate at LOS F.
- I-75 segment between US 27 and SR 326 operates at LOS E.
- Build conditions
- I-75 off-ramp diverge to US 27 and adjacent mainline segment, the ramp volume increase from improved connectivity creates a minor increase in density resulting in LOS E.
- Remaining southbound segments operate similar to No Build conditions.

As shown in the No Build segment and merge/diverge analysis results, the segments of I-75 between US 27 and SR 326 do not meet the LOS D target in year 2045 and are anticipated to operate at LOS E during either the AM or PM peak hours. The proposed interchange along NW $49^{\text {th }}$ Street is projected to meet the LOS D target; however, similar No Build I-75 segment operations (segments operating at LOS E) are also projected under build conditions. Therefore, a year of failure analysis was performed for the DDI alternative where I-75 segments reach LOS E in 2045. The analysis was conducted by interpolating volumes between years 2035 and 2045; then entering the volume for each year into HCS, until LOS E results were reached. Analysis results are summarized as follow:

## o AM Northbound:

- I-75 mainline segment south of US 27-2035
- I-75 mainline segment between US 27 and NW 49 ${ }^{\text {th }}$ Street - 2037
- NW $49^{\text {th }}$ Street off-ramp diverge condition -2041
- NW 49 ${ }^{\text {th }}$ Street on-ramp merge condition - 2044
- I-75 mainline segment between NW 49 ${ }^{\text {th }}$ Street and SR 326 - 2041


## o PM Southbound:

- I-75 south of US 27-2035
- I-75 mainline segment between SR 326 and NW $49^{\text {th }}$ Street -2041
- NW 49 ${ }^{\text {th }}$ Street on-ramp merge condition -2045
- I-75 mainline segment between NW 49 ${ }^{\text {th }}$ Street and US $27-2037$

Based on the year of failure analysis, additional I-75 mainline improvements may be required in order for I-75 to meet the LOS D target through design year. The analysis also shows that the proposed DDI at the NW 49 ${ }^{\text {th }}$ Street interchange will not have a significant adverse impact on operations along the I-75 mainline system or the existing adjacent interchanges within the study limits, when compared to No Build conditions; therefore, meeting this FHWA policy requirement. To address identified mainline deficiencies, the District is looking into potential improvements via separate projects or other methods such as the I-75 PD\&E Study (FM Number 443623-1-2201 \& 443624-1-22-01) to improve overall operations on the I-75 mainline. The results and recommendations of this IJR will be shared with the I-75 PD\&E Study team and District Traffic Operations group.

Table 1-1 presents the 2045 No Build and DDI alternative intersection delay and LOS during the AM and PM peak hours. Under No Build conditions, none of the signalized intersections meet the LOS D target except for the intersection of I-75 northbound ramps at US 27; however, the northbound off-ramp approach fails.

For Build conditions, the only signalized intersections within the AOI operating at the LOS D Target or better are the US 27 northbound ramps and the SR 326 northbound ramps intersections. The shift in traffic patterns from improved connectivity is expected to reduce total ramp volumes at both existing interchanges (US 27 and SR 326) by approximately 1,000 vehicles per day under the build condition. Although not meeting the LOS D Target for some intersections, during the AM peak hour, all intersection delays are reduced when compared to No Build conditions. During the PM peak hour, delays are decreased at all but three intersections. The difference in overall intersection delay, compared to No Build is not significant at the three intersections.

Table 1-1: 2045 No Build \& DDI Alternative Intersection Delay and LOS

| \# | Intersection | DIR | No Build |  |  |  |  |  | Build DDI |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM |  |  | PM |  |  | AM |  |  |  | PM |  |  |  |
|  |  |  | App. Delay ${ }^{2}$ LOS |  | Int. <br> Delay $^{2}$ LOS | $\begin{gathered} \text { App. } \\ \text { Delay }^{2} \text { LOS } \end{gathered}$ |  | Int. | $\begin{gathered} \text { App. } \\ \text { Delay }{ }^{2} \text { LOS } \end{gathered}$ |  | Int. <br> Delay $^{2}$ LOS |  | App. <br> Delay ${ }^{2}$ LOS |  | Int. <br> Delay ${ }^{2}$ LOS |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | NW 44 Ave at US 27 | EB <br> WB <br> NB <br> SB | $\begin{array}{r} 151.8 \\ 34.4 \\ 64.2 \\ 51.5 \end{array}$ |  | 89.5 F | $\begin{array}{r} 54.3 \\ 153.7 \\ 66.2 \\ 50.5 \end{array}$ | $\begin{gathered} \mathrm{D} \\ \mathrm{~F} \\ \mathrm{E} \\ \mathrm{D} \end{gathered}$ | 105.1 F | 111.1 <br> 33.0 <br> 49.7 <br> 45.9 | $\begin{aligned} & \mathrm{F} \\ & \mathrm{C} \\ & \mathrm{D} \\ & \mathrm{D} \end{aligned}$ | 70.5 | E | $\begin{gathered} 39.0 \\ 171.5 \\ 60.4 \\ 48.3 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ \mathrm{~F} \\ \mathrm{E} \\ \mathrm{D} \end{gathered}$ | 111.1 | F |
| 2 | $\begin{aligned} & \mathrm{I}-75 \mathrm{SB} \\ & \text { at US } 27 \end{aligned}$ | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { SB } \end{gathered}$ | $\begin{array}{r} 142.4 \\ 73.3 \\ 59.6 \end{array}$ | $\begin{gathered} \mathrm{F} \\ \mathrm{E} \\ \mathrm{E} \end{gathered}$ | 108.3 F | $\begin{aligned} & 77.5 \\ & 63.7 \\ & 59.2 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | 68.8 E | $\begin{aligned} & 90.5 \\ & 21.4 \\ & 50.7 \end{aligned}$ | $\begin{aligned} & \text { F } \\ & \text { C } \\ & \text { D } \end{aligned}$ | 57.6 | E | $\begin{aligned} & 62.2 \\ & 53.7 \\ & 97.9 \end{aligned}$ | E <br> D <br> F | 58.5 | E |
| 3 | $\begin{aligned} & \text { I-75 NB } \\ & \text { at US } 27 \end{aligned}$ | EB <br> WB <br> NB | $\begin{array}{r} 6.7 \\ 21.8 \\ 60.8 \end{array}$ | A <br> C <br> E | 25.4 C | $\begin{array}{r} 1.2 \\ 36.3 \\ 119.6 \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{D} \\ & \mathrm{~F} \end{aligned}$ | 46.2 D | $\begin{gathered} 2.2 \\ 19.4 \\ 33.7 \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { B } \\ & \text { C } \end{aligned}$ | 15.5 | B | $\begin{gathered} 1.5 \\ 45.4 \\ 77.3 \end{gathered}$ | A <br> D <br> E | 39.6 | D |
| 4 | NW 35 Ave Rd at US 27 | $\begin{gathered} \text { EB } \\ \mathrm{WB} \\ \mathrm{NB} \\ \mathrm{SB} \end{gathered}$ | $\begin{array}{r} 66.5 \\ 69.0 \\ 57.4 \\ 415.1 \end{array}$ | $\begin{gathered} \mathrm{E} \\ \mathrm{E} \\ \mathrm{E} \\ \mathrm{~F} \end{gathered}$ | 125.6 F | $\begin{array}{r} 101.1 \\ 178.3 \\ 54.8 \\ 463.0 \end{array}$ | $\begin{gathered} \text { F } \\ \text { F } \\ \text { D } \\ \text { F } \end{gathered}$ | 199.2 F | $\begin{gathered} 49.0 \\ 60.6 \\ 55.0 \\ 397.8 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ \mathrm{E} \\ \mathrm{E} \\ \mathrm{~F} \end{gathered}$ | 112.7 | F | $\begin{gathered} 99.6 \\ 193.5 \\ 55.0 \\ 517.8 \end{gathered}$ | $\begin{aligned} & F \\ & F \\ & D \\ & \text { F } \end{aligned}$ | 218.1 | F |
| 5 | NW 44 Ave at NW 49 ST | $\begin{gathered} \mathrm{EB} \\ \mathrm{WB} \\ \mathrm{NB} \\ \mathrm{SB} \end{gathered}$ | $\begin{array}{r} 61.6 \\ 81.6 \\ 208.6 \\ 37.7 \end{array}$ | $\mathrm{E}$ F F D | 96.8 F | $\begin{array}{r} 64.7 \\ 159.6 \\ 64.9 \\ 25.3 \end{array}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{~F} \\ & \mathrm{E} \\ & \mathrm{C} \end{aligned}$ | 88.4 F | $\begin{aligned} & 43.0 \\ & 36.1 \\ & 25.0 \\ & 27.2 \end{aligned}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{D} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 30.1 | C | $\begin{aligned} & 42.6 \\ & 33.2 \\ & 21.8 \\ & 27.2 \end{aligned}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \hline \end{aligned}$ | 28.4 | C |
| 6 | NW 44 Ave/ I-75 SB Off at SR 326 | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{r} 22.7 \\ 47.6 \\ 111.5 \\ 116.3 \end{array}$ | C <br> D <br> F <br> F | 68.6 E | $\begin{array}{r} 25.6 \\ 43.2 \\ 145.5 \\ 96.8 \end{array}$ | $\begin{aligned} & C \\ & D \\ & \text { F } \\ & \text { F } \end{aligned}$ | 74.2 E | $\begin{aligned} & 15.8 \\ & 15.9 \\ & 28.3 \\ & 24.2 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~B} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 19.4 | B | $\begin{aligned} & 19.8 \\ & 20.5 \\ & 32.7 \\ & 31.5 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 24.9 | C |
| 7 | $\begin{aligned} & \text { I-75 SB On- } \\ & \text { Ramp (Loop) } \\ & \text { at SR } 326 \\ & \text { Unsignalized } \end{aligned}$ | EB <br> WB <br> NB | $\begin{array}{r} 0.0 \\ 17.1 \\ 15 \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 10.4 B | $\begin{array}{r} 0.0 \\ 2.2 \\ 14.7 \end{array}$ | $\begin{gathered} \text { A } \\ \text { A } \\ \text { B } \end{gathered}$ | 1.5 A | $\begin{gathered} 0.0 \\ 6.5 \\ 13.6 \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { A } \\ \text { B } \end{gathered}$ | 4.4 | A | $\begin{gathered} 0.0 \\ 1.5 \\ 12.6 \end{gathered}$ | A <br> A <br> B | 1.2 | A |
| 8 | $\begin{aligned} & \text { I- } 75 \text { NB Off/ } \\ & \text { I75 NB On } \\ & \text { at SR } 326^{1} \end{aligned}$ | EB <br> WB <br> NB | $\begin{array}{r} 45.7 \\ 329.8 \\ 851.8 \end{array}$ | D <br> F <br> F | 418.3 F | $\begin{array}{r} 95.7 \\ 395.6 \\ 409.4 \end{array}$ | $\begin{aligned} & \mathrm{F} \\ & \mathrm{~F} \\ & \mathrm{~F} \end{aligned}$ | 332.0 F | $\begin{gathered} 13.9 \\ 251.1 \\ 774.4 \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \mathrm{~F} \\ \mathrm{~F} \end{gathered}$ | 365.7 | F | $\begin{gathered} 57.8 \\ 431.3 \\ 431.2 \end{gathered}$ | $\mathrm{E}$ F F | 367.2 | F |
| 9 | $\begin{gathered} 175 \mathrm{SB} \\ \text { at NW } 49 \mathrm{ST}^{1} \end{gathered}$ | $\begin{gathered} \text { SBR } \\ \text { SBL } \\ \text { EBT } \\ \text { WBT } \end{gathered}$ |  |  |  |  |  |  | 21.4 <br> 34.8 <br> 18.2 $13.8$ | $\begin{gathered} \mathrm{C} \\ \mathrm{C} \\ \text { B } \\ \text { B } \end{gathered}$ | 18.2 | B | $\begin{gathered} 20.8 \\ 28.3 \\ 9.9 \\ 18.4 \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{~A} \\ & \mathrm{~B} \end{aligned}$ | 17.3 | B |
| 10 | $\begin{aligned} & 175 \text { NB } \\ & \text { at NW } 49 \text { ST }^{1} \end{aligned}$ | $\begin{gathered} \text { NBL } \\ \text { NBR } \\ \text { EBT } \\ \text { WBT } \end{gathered}$ |  |  |  |  |  |  | 32.4 <br> 16.3 <br> 13.6 <br> 18.6 | $\begin{aligned} & \text { C } \\ & \text { B } \\ & \text { B } \\ & \text { B } \end{aligned}$ | 20.5 | B | $\begin{gathered} 30.1 \\ 19.3 \\ 7.3 \\ 20.2 \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~B} \\ & \mathrm{~A} \\ & \mathrm{C} \end{aligned}$ | 19.3 | B |

[^0]Table 1-2 summarizes the network performance from the Vissim analysis. The benefits of the build alternative are visibly higher during the AM peak period. During the PM peak period, the benefits are not as significant due to the higher demand volumes, which results in higher congestion on I-75 southbound at the US 27 interchange. Overall, all performance measures show improvement under the DDI alternative compared to No Build. Network statistic improvements are as follow:

- AM Peak
o Total Delay: Reduced by $37 \%$
o Total Stops: Reduced by $47 \%$
o Average Speed: Increased by 3 mph
o Vehicles Arrived: Increased by 1,188 vehicles
o Vehicle-Miles Traveled: Increase by 15,464 miles
o Latent Delay: Reduced by 387 hours
o Latent Demand: Reduced by 1,697 hours


## - PM Peak

o Total Delay: Reduced by $15 \%$
o Total Stops: Reduced by $25 \%$
o Average Speed: Increased by 2 mph
o Vehicles Arrived: Increased by 1,466 vehicles
o Vehicle-Miles Traveled: Increase by 16,387 miles
o Latent Delay: Reduced by 51 hours
o Latent Demand: Reduced by 217 hours

Table 1-2 2045 Vissim Network Performance Summary

| Peak Hour | $\begin{aligned} & 15-\mathrm{min} \\ & \text { Period } \end{aligned}$ | No Build |  |  |  |  |  |  | DDI |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | VehicleMiles Traveled | Latent Delay (Hours) | Latent Demand (Vehicles) | $\begin{aligned} & \hline \text { Total } \\ & \text { Delay } \\ & \text { (Hours) } \\ & \hline \end{aligned}$ | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | VehicleMiles Traveled | Latent Delay (Hours) | Latent Demand (Vehicles) |
| AM | 1 | 21 | 1,980 | 58 | 2,854 | 13,513 | 0 | 0 | 24 | 2,152 | 56 | 2,874 | 14,262 | 0 | 0 |
|  | 2 | 33 | 3,034 | 56 | 3,558 | 16,829 | 0 | 0 | 36 | 3,142 | 55 | 3,565 | 17,796 | 0 | 0 |
|  | 3 | 43 | 3,981 | 55 | 4,048 | 18,965 | 0 | 1 | 46 | 4,026 | 54 | 4,081 | 19,997 | 0 | 1 |
|  | 4 | 53 | 5,095 | 54 | 4,283 | 20,027 | 0 | 1 | 53 | 4,666 | 54 | 4,359 | 21,230 | 0 | 1 |
|  | 5 | 93 | 9,964 | 50 | 4,667 | 22,275 | 0 | 3 | 83 | 7,802 | 51 | 4,746 | 23,652 | 1 | 5 |
|  | 6 | 165 | 18,817 | 44 | 4,878 | 22,897 | 9 | 97 | 127 | 13,118 | 47 | 5,087 | 24,632 | 3 | 19 |
|  | 7 | 215 | 24,529 | 40 | 4,832 | 22,799 | 47 | 293 | 166 | 17,774 | 44 | 5,032 | 24,507 | 14 | 109 |
|  | 8 | 211 | 23,218 | 39 | 4,694 | 21,326 | 75 | 326 | 160 | 17,568 | 43 | 4,797 | 22,682 | 22 | 89 |
|  | 9 | 187 | 20,770 | 40 | 4,496 | 20,691 | 84 | 347 | 133 | 14,654 | 45 | 4,602 | 22,012 | 21 | 79 |
|  | 10 | 182 | 20,154 | 41 | 4,507 | 20,757 | 91 | 382 | 116 | 12,211 | 47 | 4,630 | 22,262 | 19 | 74 |
|  | 11 | 178 | 19,332 | 42 | 4,574 | 21,335 | 100 | 403 | 106 | 10,502 | 48 | 4,692 | 22,650 | 19 | 76 |
|  | 12 | 176 | 20,012 | 41 | 4,393 | 19,981 | 97 | 357 | 89 | 8,646 | 49 | 4,507 | 21,177 | 17 | 60 |
|  | Total ${ }^{1}$ | 1,557 | 170,886 | 46 | 51,784 | 241,395 | 503 | 2,210 | 1,139 | 116,261 | 49 | 52,972 | 256,859 | 116 | 513 |
| PM | 1 | 78 | 6,781 | 51 | 4,465 | 20,171 | 0 | 2 | 85 | 6,904 | 50 | 4,545 | 21,429 | 1 | 9 |
|  | 2 | 88 | 7,486 | 49 | 4,428 | 19,854 | 4 | 20 | 89 | 6,701 | 49 | 4,553 | 21,113 | 7 | 29 |
|  | 3 | 113 | 9,992 | 47 | 4,572 | 21,238 | 12 | 73 | 108 | 8,479 | 48 | 4,672 | 22,600 | 21 | 127 |
|  | 4 | 137 | 12,609 | 45 | 4,739 | 21,598 | 37 | 183 | 123 | 9,860 | 47 | 4,892 | 23,030 | 50 | 239 |
|  | 5 | 158 | 16,407 | 43 | 4,748 | 21,700 | 67 | 330 | 135 | 11,555 | 46 | 4,870 | 23,210 | 79 | 374 |
|  | 6 | 175 | 17,801 | 42 | 4,724 | 21,355 | 105 | 474 | 146 | 13,453 | 44 | 4,901 | 22,797 | 112 | 499 |
|  | 7 | 198 | 20,597 | 41 | 4,759 | 22,182 | 151 | 717 | 160 | 15,527 | 44 | 4,911 | 23,637 | 153 | 702 |
|  | 8 | 221 | 24,377 | 39 | 4,839 | 22,198 | 217 | 971 | 184 | 19,593 | 42 | 4,985 | 23,932 | 206 | 902 |
|  | 9 | 236 | 26,684 | 38 | 4,797 | 21,984 | 275 | 1,199 | 211 | 23,172 | 40 | 4,912 | 23,441 | 255 | 1,110 |
|  | 10 | 222 | 25,246 | 38 | 4,620 | 20,428 | 316 | 1,282 | 191 | 21,240 | 40 | 4,794 | 21,733 | 293 | 1,190 |
|  | 11 | 176 | 19,134 | 40 | 4,429 | 19,423 | 327 | 1,310 | 144 | 14,620 | 43 | 4,504 | 20,576 | 302 | 1,201 |
|  | 12 | 134 | 13,881 | 43 | 4,152 | 18,122 | 326 | 1,255 | 106 | 9,755 | 46 | 4,199 | 19,142 | 307 | 1,217 |
|  | Total ${ }^{1}$ | 1,936 | 200,995 | 43 | 55,272 | 250,253 | 1,837 | 7,816 | 1,682 | 160,859 | 45 | 56,738 | 266,640 | 1,786 | 7,599 |

A predictive crash analysis was conducted to compare predicted crashes of the No Build and the five Build alternatives. The analysis was conducted for future conditions utilizing the predictive methods set forth in the Highway Safety Manual (HSM) Parts C and D. A summary of the predicted number of annual crashes for the project site (interchange alternatives) is provided in Table 1-3 and for the AOI in Table 1-4. The predicted number of annual crashes for the interchange alternatives range from 96.3 crashes per year for the DDI alternative, the best in regard to safety; to 108.0 crashes per year for the Diamond alternative, ranking the worst. In addition, the project AOI shows a net reduction in total crashes from 321.9 crashes under No Build to 317.2 crashes under Build conditions. It should be noted that compared to No Build, Build Annual Average Daily Traffic (AADT) values are higher; which inherently increases predicted crashes, even when the same scenario is maintained.

Table 1-3: Project Site Predicted 2045 Annual Crashes

| Location | DIAMOND |  |  | SPUI |  |  | ParClo SE |  |  | ParClo NE |  |  | DDI |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total |
| 1-75 (N of US 27 to NW 49 ${ }^{\text {th }}$ Street to $S$ of SR 326) | 19.4 | 48.5 | 67.8 | 19.8 | 49.9 | 69.7 | 17.6 | 44.3 | 61.8 | 18.5 | 46.8 | 65.3 | 19.4 | 48.5 | 67.8 |
| I-75 \& NW 49 ${ }^{\text {th }}$ Street Interchange ${ }^{1}$ | 11.9 | 25.3 | 37.2 | 8.0 | 22.2 | 30.1 | 12.9 | 26.6 | 39.5 | 10.2 | 19.2 | 29.4 | 8.0 | 17.5 | 25.5 |
| NW 49 ${ }^{\text {th }}$ Street, NW 44 ${ }^{\text {th }}$ Avenue to I-75 | 0.1 | 0.2 | 0.3 | 0.1 | 0.3 | 0.4 | 0.1 | 0.2 | 0.3 | 0.1 | 0.2 | 0.3 | 0.1 | 0.2 | 0.3 |
| NW 49 ${ }^{\text {th }}$ Street, East of I-75 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 |
| NW 44 ${ }^{\text {th }}$ Avenue at NW 49 ${ }^{\text {th }}$ Street | 0.7 | 1.3 | 2.0 | 0.7 | 1.3 | 2.0 | 0.7 | 1.3 | 2.0 | 0.6 | 1.3 | 1.9 | 0.7 | 1.3 | 2.0 |
| TOTALS | 32.2 | 75.8 | 108.0 | 28.7 | 74.2 | 102.9 | 31.4 | 72.9 | 104.3 | 29.6 | 68.1 | 97.7 | 28.3 | 68.1 | 96.3 |

${ }^{1}$ Merge/Diverge/Ramps/Ramp Termini

Table 1-4: AOI Cumulative Predicted 2045 Annual Crash Summary

| Location | FI | PDO | NO BUILD | FI | PDO | BUILD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I-75 (S of US 27-N Ramps \& S Ramps-N of SR 326) | 18.5 | 48.1 | 66.6 | 19.4 | 51.0 | 70.3 |
| I-75 \& US 27 Interchange ${ }^{1}$ | 28.2 | 39.9 | 68.0 | 27.1 | 38.4 | 65.5 |
| I-75 \& SR 326 Interchange ${ }^{1}$ | 41.2 | 76.6 | 117.7 | 40.2 | 77.4 | 117.7 |
| US 27 (Arterial \& Intersections) | 13.5 | 28.4 | 41.8 | 12.8 | 27.0 | 39.8 |
| SR 326 (Arterial \& Intersections) | 4.7 | 12.0 | 16.7 | 4.6 | 11.8 | 16.4 |
| NW 44 ${ }^{\text {th }}$ Avenue AOI (N \& S of NW 49 ${ }^{\text {th }}$ St) | 3.0 | 8.0 | 11.0 | 2.0 | 5.4 | 7.4 |
| TOTALS | 109.0 | 212.9 | 321.9 | 106.1 | 211.0 | 317.2 |

${ }^{1}$ Merge/Diverge/Ramps/Ramp Termini

The proposed interchange ramp gores would be located at a minimum of 0.87 miles away from the US 27 ramp gores and a minimum of 0.90 miles away from the SR 326 ramp gores; and do not create weaving segments.
2. The proposed access connects to a public road only and will provide for all traffic movements. Less than "full interchanges" may be considered on a case-by-case basis for applications requiring special access for managed lanes (e.g., transit, HOVs, HOT lanes) or park and ride lots. The proposed access will be designed to meet or exceed current standards (23 CFR 625.2(a), 625.4(a)(2), and 655.603(d)).

The new interchange will be designed to meet or exceed current FDOT Design Standards and will serve all traffic movements. The interchange will connect to the extension of NW $49^{\text {th }}$ Street. This roadway project is currently under design, with funding for construction in 2024/25; it will conform to FDOT Design Standards and will be a public roadway.

Marion County and the City of Ocala have already constructed public roadways that will facilitate access to the proposed interchange. Specifically, the four-laning of NW 35 ${ }^{\text {th }}$ Street from US 441 (North Pine Avenue) to NW $35^{\text {th }}$ Avenue Road and the four-lane construction of NW $35^{\text {th }}$ Avenue Road north from US 27 (NW Blitchton Road) to intersect with the NW 35 ${ }^{\text {th }}$ Street project.

### 1.4 Summary Request

As discussed previously, the recommended DDI alternative meets FHWA's Two Policy Requirements. Based on the analysis presented in this document, approval is requested of a new interchange to be located at I-75 and the planned extension of NW 49 ${ }^{\text {th }}$ Street, as part of a PD\&E Study. The I-75 and NW 49 ${ }^{\text {th }}$ Street interchange is currently listed as the number one (1) priority project on the Ocala/Marion Transportation Planning Organization (TPO) adopted Fiscal Year (FY) 2025 Priority Projects. In addition, the PD\&E Study and Preliminary Design for this project are included in the current FDOT Five Year (2021-2025) Work Program in Years prior to 2020, 2020 and 2023, respectively; presented in more detail in Sections 2 and 9.

The DDI alternative provides the highest performing operations and lowest predicted number of crashes when compared to the other Build alternatives. In terms of environmental, socioeconomic, cost, and other engineering factors, the DDI alternative ranked first in the alternative evaluation matrix. Based on the aforementioned, the DDI alternative is the recommended interchange configuration for I-75 at NW 49 ${ }^{\text {th }}$ Street. Recommended storage lengths are provided in Table 1-5. It should be noted that recommended storage lengths do not include deceleration and taper lengths. Additional storage is also suggested to accommodate the heavy truck traffic that is anticipated at the proposed interchange to support the industrial/commercial Ocala 489 commerce park.

For maximum operational efficiency, it is recommended to integrate the proposed interchange into the surrounding existing and planned Transportation Systems Management \& Operations (TSM\&O) network as identified in the Marion County TSM\&O Master Plan and the FDOT F.R.A.M.E. project (FM Number 440900-1). In addition to inclusion of the recommended interchange into the TSM\&O network, the recommended DDI alternative is also being designed to accommodate future improvements should the need arise. Finally, based on the year of failure analysis, additional I-75 mainline improvements may be required in order for I-75 to meet the LOS D target through design year. As previously mentioned, the District is looking into potential improvements to the I-75 mainline via separate projects or other methods such as the I-75 PD\&E Study (FM Number 443623-1-22-01 \& 443624-1-22-01) to improve overall operations on the I75 mainline. The results and recommendations of this IJR will be shared with the I-75 PD\&E Study team and District Traffic Operations group.

Table 1-5: 2045 Recommended Turn Lane Storage Lengths

| Interchange | Ramps | Movement | Turn Bay Length ${ }^{1}$ (ft) | 95th Percentile Queue Length ${ }^{2}$ ( ft ) |  | Vissim Max Queue Length (ft) |  | Recommended Storage Length, ${ }^{3}$ (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM | PM | AM | PM |  |
| DDI | I-75 NB | WBR | 250 | 40 | 37 | 4 | 0 | 50 |
|  |  | NBL | - | 0 | 0 | 228 | 256 | 275 |
|  | I-75 SB | EBR | 300 | 24 | 13 | 201 | 265 | 275 |
|  |  | SBL | - | 0 | 0 | 166 | 207 | 225 |

[^1]
## 2 Introduction

### 2.1 Background

This IJR follows a previously approved IJR completed on behalf of Marion County. The 2016 IJR documents the need for, and analysis of a new interchange on I-75 at the planned extension of NW 49 ${ }^{\text {th }}$ Street in Marion County, Florida; see Figure 2-1 Project Location.

The 2016 IJR evaluated the No Build and Urban Diamond Interchange alternatives. This new IJR is being developed as part of the I-75 at NW 49 ${ }^{\text {th }}$ Street PD\&E Study which updates the traffic forecasting, using the most recent Central Florida Regional Planning Model (CFRPM) version 6.1; and evaluates additional alternatives.

The greater Ocala area has recently experienced one of the highest growth rates in the country for a city its size, and the Marion County Comprehensive Plan outlines a vision to enhance the livability of its residents and promote economic growth in the region. In this vein, the County has designated approximately 3,000 acres adjacent to I-75 as a future commerce park. This commerce park is composed of a recently constructed FedEx Ground Distribution Hub; Chewy distribution center; an AutoZone distribution center, designated as a CSX Select Site; the Florida Crossroads Logistics Center, a Red Rock Development; and the remaining undeveloped sites. Development in this area will result in traffic volume increases along I-75 and the entire local roadway network; adding a projected $25,000+$ daily trips to the roadway network upon fullbuildout, $12 \%$, or 3,000 vehicles of which are projected to be trucks.

Per request of FDOT, this IJR document is to maintain consistency with the 2016 IJR, when feasible. Therefore, direct excerpts from the 2016 IJR have been incorporated throughout this document for consistency and continuity.


Figure 2-1: Project Location

### 2.2 Project Purpose and Need

### 2.2.1 Purpose

The purpose of a new I-75 interchange at NW $49^{\text {th }} / 35^{\text {th }}$ Street is to provide relief to the congestion and operational deficiencies at both existing contiguous l-75 interchanges, by providing an alternate access to I-75 for the projected increase in truck volumes resulting from the future commerce district.

### 2.2.2 Need

The overall study was initiated with a detailed, comprehensive analysis of existing/projected substandard conditions. In general terms, some of the most critical potential needs include:

### 2.2.2.1 Economic Viability and Job Creation:

The proposed interchange is needed to support the economic viability of the Ocala 489, a 489 acre industrial and commercial development, which is intended to serve as an economic engine for job creation in the region and is envisioned as a strategic central inland hub for freight-related traffic (see Figure 2-2). The Ocala 489 has been established as a Florida Enterprise Zone, a designation which provides numerous tax credits to businesses located within the Commerce Park. In addition, this commerce park includes a site, recently developed by AutoZone, that was designated as a CSX Select Site (the first in Florida). Select Sites are properties identified and vetted as capable locations for future manufacturing


Figure 2-2: Ocala 489 Commerce Park facilities along the CSX rail network. FedEx Ground, Florida Crossroads Logistics Center, and Chewy also completed new facilities within the Ocala 489. Marion County has already made infrastructure improvements within the Park with the extension of NW $35^{\text {th }}$ Street as a divided four lane facility.

It should be noted that the Ocala 489 is zoned $\mathrm{M}-1 / \mathrm{M}-2$ or Light/Heavy Industrial and the businesses that are intended to occupy the commerce park will depend heavily on interstate and regional movement to transport raw materials and finished goods, around the State and beyond. In summary, due to its strategic location and incentives, the Ocala 489 and the commerce district/employment center will provide needed jobs in the area.

### 2.2.2.2 Improve Interstate and Regional Mobility

The proposed interchange will provide a more direct and efficient access to I-75 thus facilitating interstate and regional mobility. As previously stated, I-75 is a vital north-south interstate facility connecting six different states. From a regional perspective (see Figure 2-3) Marion County is


Figure 2-3: Regional Map
approximately midway between Miami and Atlanta and occupies a strategic location due to its relative proximity to other important metropolitan areas such as Jacksonville, Orlando, and Tampa. This strategic location coupled with the presence of a major interstate facility such as I75 makes this area a key potential hub for commercial industry. The proposed interchange is thus needed to support the efficient movements of goods.

### 2.2.2.3 Address Locally Supported Long Term Regional Needs

The proposed project is needed to provide important access to l-75 as part of a locally supported long range vision to provide a future east-west corridor parallel to US 27 and SR 326. This eastwest corridor begins at NE $36^{\text {th }}$ Avenue, east of I-75 and Downtown Ocala and terminates at NW $70^{\text {th }}$ Avenue, west of the proposed I-75 interchange. In conjunction with this new east-west corridor is a connection to US 27 at NW $35^{\text {th }}$ Avenue Road and at NW $60^{\text {th }}$ Avenue.

The proposed I-75 interchange is currently listed as the number one (1) priority project on the Ocala/Marion TPO FY 2025 Priority Projects List. Excerpts from plans published by FDOT, Marion County and the Ocala Marion TPO that reflect corresponding planned and programmed projects are provided in Appendix A. The County has completed a number of improvements in the area in support of the proposed interchange and the Ocala 489 (see Figure 2-4), including extension of NW 35 ${ }^{\text {th }}$ Avenue Road. Phase 2A of the NW $35^{\text {th }}$ Avenue Road extension was recently completed by the County, Phase 2B is a Marion County project currently in Final Design and programmed for construction in 2021, and Phase 2C (see Figure 2-4) is the connection between the proposed interchange and the future NW 35 ${ }^{\text {th }}$ Avenue Road (Phase 2B) that will be completed as part of the proposed interchange.


Figure 2-4: Adjacent Projects

### 2.2.2.4 Accommodate Future Traffic Growth

As previously stated, one of the primary justifications for the new interchange is to accommodate projected future year traffic volumes. Marion County has experienced a significant and sustained growth in population since 1970. This significant growth rate is expected to continue in the future. According to the currently adopted CFRPM socio-economic data for 2010 and 2040, the projected population for Marion County is expected to grow from approximately 325,199 to over 490,204 in population by 2040. As a result of this population growth, traffic volumes are increasing and will continue to increase in the future. As shown on Table 2-1, the proposed interchange will result in a reduction in the design year (2045) traffic volumes on US 27 and SR 326, the two contiguous I-75 interchange locations, as well as NW $35^{\text {th }}$ Avenue Road, generally resulting in reduced delays and improved levels of service.

It should be noted that the existing SR 326 interchange located north of the proposed interchange would be a rather indirect option for trucks serving the Ocala 489 and therefore most of the truck traffic associated with the Commerce Park would likely utilize the US 27 interchange, severely degrading operations and safety at the interchange throughout the day. The need for the new interchange is based on projected traffic volumes in design year 2045 from build-out of not only the Ocala 489 but also the adjacent commerce district/employment center totaling 5,000
+/- acres. It is projected from the CFRPM 6.1 model that build-out in design year 2045 will add 25,000 daily trips to the roadway network with approximately $12 \%$, or 3,000 vehicles, of which are projected to be trucks. As a result of this growth, traffic volumes are increasing and will continue to increase in the future.

Table 2-1: Projected Traffic Effects of the Proposed Interchange (Year 2045)

| LOCATION | \% of Traffic Impact Change (AADT) |  |  |
| :--- | ---: | ---: | ---: |
|  | No Build (2045) | Build (2045) | \% Change |
| US 27 W of I-75 | 51,100 | 49,300 | $-3.52 \%$ |
| US 27 E of I-75 | 55,300 | 53,800 | $-2.71 \%$ |
| I 75 NB Off Ramp at US 27 | 14,600 | 12,800 | $-12.33 \%$ |
| I 75 SB On Ramp at US 27 | 15,200 | 13,500 | $-11.18 \%$ |
| I 75 NB On Ramp at US 27 | 2,700 | 3,600 | $33.33 \%$ |
| I 75 SB Off Ramp at US 27 | 2,900 | 4,300 | $48.28 \%$ |
| NW 35 Ave Rd N of US 27 | 24,700 | 21,600 | $-12.55 \%$ |
| SR 326 W of I-75 | 12,500 | 12,200 | $-2.40 \%$ |
| SR 326 E of I-75 | 38,200 | 37,700 | $-1.31 \%$ |
| NW 49th St East of I-75 | 14,600 | 17,500 | $19.86 \%$ |
| NW 49th St West of I-75 | 14,600 | 21,500 | $47.26 \%$ |

### 2.3 Project Location and Area of Influence

## Location

The proposed interchange would be located along I-75 at the planned extension of NW 49 ${ }^{\text {th }}$ Street in Marion County, Florida. This extension is currently under design by Marion County and is slated for construction in 2024/25. The interchange would be located at Milepost 356, north of US 27 (Milepost 354) and south of SR 326 (Milepost 358). The study interchange is located approximately 2.2 miles north of the I-75 and US 27 interchange and approximately 2.0 miles south of the I-75 and SR 326 interchange.

## Area of Influence

The AOI defines the study area for the IJR. As defined in the FDOT IARUG and as directed by the Department, the AOI includes at a minimum, one interchange on either side of the subject interchange and signalized intersections within one-half mile on the cross streets, see Figure 25.


Figure 2-5: Area of Influence

The following interchanges are included in the AOI:

- I-75 at US 27
- NW 49 ${ }^{\text {th }}$ Street at I-75 northbound ramps (Proposed)
- NW 49 ${ }^{\text {th }}$ Street at I-75 southbound ramps (Proposed)
- I-75 at SR 326

The following existing intersections are within the AOI of the proposed interchange:

- US 27 at NW $44^{\text {th }}$ Avenue
- US 27 at I-75 northbound ramps
- US 27 at I-75 southbound ramps
- US 27 at NW 35 ${ }^{\text {th }}$ Avenue Road
- NW 49 ${ }^{\text {th }}$ Street at NW 44 ${ }^{\text {th }}$ Avenue
- SR 326 at I-75 northbound ramps
- SR 326 at I-75 southbound ramps /NW 44 ${ }^{\text {th }}$ Avenue


### 2.4 Methodology

The methodology for the IJR was developed in accordance with procedures and methods outlined in the 2020 FDOT IARUG and Procedure No. 525-030-160. This procedure requires that the interchange request applicant develops an MLOU for approval by the District Interchange Review Coordinator (DIRC), and the Systems Implementation Office (SIO). The MLOU details the proposed approach to developing the IJR to document the need for, analysis of and impacts associated with the new interchange. The MLOU developed for this project was approved in January 2018.

The original MLOU was updated under an amendment in coordination with the Department and approved in September 2020. The MLOU amendment addresses and documents updates to the methodology such as use of more recent traffic and safety data as well as further operational and forecasting methodology details consistent with this IJR.

The MLOU and MLOU amendment are provided for reference in Appendix B.

### 2.5 Analysis Years

Per the MLOU, the following analysis years were utilized to evaluate interchange operations as part of this IJR:

- Traffic Demand Model Forecasting Years
o Base Year 2015
o Horizon Year 2045
- Traffic Operational Analysis
o Existing Year 2017
o Opening Year 2025
o Interim Year 2035
o Design Year 2045


### 2.6 Existing Condition Analysis

An analysis was conducted of the current operating conditions within the project AOI. This analysis served as the basis for comparison and analysis of the proposed interchange. The existing condition analysis is discussed further in Section 3.

### 2.7 Development of Future Design Traffic

Future traffic volumes were developed using CFRPM version 6.1. Although the CFRPM 6.1 has a 2010 base year, a 2015 network and socioeconomic dataset were developed by the Department with input from the local Metropolitan Planning Organization (MPO), the OcalaMarion TPO, for the area under the Ocala-Marion TPO. The CFRPM 6.1 validation and subarea refinement was performed for the base year 2015. These adjustments were then used as a baseline to develop design traffic volumes for the Opening Year 2025, Interim Year 2035 and Design Year 2045. The development of future year estimates for intersection turning movements is consistent with the procedures outlined in the FDOT Project Traffic Forecasting Handbook, 2019. The future intersection volumes were developed from the existing (2017) turning movement percentage breakdown, corresponding future AADT, $K$ and $D$ factors; in the TMTool worksheets. The future conditions traffic and analyses are further discussed in Sections 5, 6 and 7.

### 2.8 Evaluation of Alternatives

Seven (7) alternatives were considered as part of the IJR: (1) the No Build alternative, (2) the TSM\&O alternative, (3) Diamond Build alternative, (4) SPUI Build alternative, (5) Partial

Cloverleaf (Parclo)-SE Build alternative, (6) Parclo-NE Build alternative and (7) DDI Build alternative. The alternatives are discussed in more detail in Section 4.

### 2.9 Operational Analysis

An operational analysis and evaluation were conducted for both the No Build and the Build Alternatives; under Existing 2017, Opening Year 2025, Interim Year 2035, and Design Year 2045 conditions. The No Build Analysis served as a baseline for comparison of future year conditions. The evaluation involved an assessment of the freeway segments, intersections, ramps, merge and diverge areas.

The operational analysis was accomplished using the most current adopted procedures in the FDOT Traffic Analysis Handbook, March 2014. Software used to perform the operational analysis included the 2010 HCS package 6.8, Synchro 10 and Vissim 2020.00-07. The future operational analysis conducted as part of the IJR is discussed in greater detail in Section 6.

### 2.10 Transportation Plans

Interchange proposals must be consistent with regional and local government adopted transportation plans. This study considered all roadway improvements that are programmed and planned in the area. These capacity improvements are consistent with the following regional transportation plans; presented in greater detail in Section 9.
o FDOT State Transportation Improvement Program (STIP) Five-Year Work Program 20202024
o FDOT Strategic Intermodal Systems (SIS) Plans
o Marion County Transportation Improvement Program (TIP) Fiscal Years 2020/20212024/2025
o Ocala/Marion TPO 2040 Long Range Transportation Plan (LRTP)
o The Marion County Comprehensive Plan 2035
o Ocala/Marion TPO Future Year 2025 Priority Projects

### 2.11 Safety and Crashes

A review of the available crash data between 2013 and 2017 within the AOI was conducted and documented in this report. Crash data was obtained via the FDOT Crash Analysis and Reporting (CAR) Online database and the Signal Four Analytics system. The safety and crash history are discussed in greater detail in Section 3. Future conditions were analyzed using the predictive
methods set forth in the HSM Parts C and D. The analysis is presented in greater detail in Section 7.

### 2.12 Environmental Considerations

No significant impacts are expected as a result of the proposed interchange to the natural, physical, socio-cultural, or economic aspects of the environment. Section 8 provides additional detail regarding each of these environmental factors. Further analysis will be provided in the Preliminary Engineering Report (PER).

### 2.13 Funding Plan

As previously mentioned, the proposed project is listed as the number one (1) priority project by the Ocala/Marion TPO. Funding has been allocated for future phases of the I-75 at NW 49 ${ }^{\text {th }}$ Street interchange project, including the PD\&E study, right of way, design and construction of both the new interchange and the NW 49 ${ }^{\text {th }}$ Street extension; see Table 2-2 for a consolidation of funding source information. The funding plan is presented in greater detail in Section 9.

Table 2-2: Project Location Funding Source and Schedule

| Project | Funding Source | Funding | Phase [1] | Years |
| :---: | :---: | :---: | :---: | :---: |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$10,200,000 | ROW | 2021/22 |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$9,440,914 | CST | 2024/25 |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$8,419,861 | CST | 2024/25 |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$8,522,752 | CST | 2024/25 |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$14,415,217 | CST | 2024/25 |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$114,400 | CST | 2024/25 |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$4,696,516 | CST | 2024/25 |
| I-75 at NW 49 Street Interchange | Ocala/Marion TPO TIP [2] | \$3,407,729 | CST | 2024/25 |
| I-75 at NW 49 Street Interchange | FDOT 5-YEAR WP [3] | \$15,990 | PD\&E | 2021 |
| I-75 at NW 49 Street Interchange | FDOT 5-YEAR WP [3] | \$373,968 | PE | 2021 |
| I-75 at NW 49 Street Interchange | FDOT 5-YEAR WP [3] | \$10,200,000 | ROW | 2022 |
| I-75 at NW 49 Street Interchange | FDOT 5-YEAR WP [3] | \$47,774,814 | CST | 2025 |
| I-75 at NW 49 Street Interchange | FDOT STIP [4] | \$2,716,535 | PD\&E | <2020-2020 |
| I-75 at NW 49 Street Interchange | FDOT STIP [4] | \$2,104,131 | PE | 2022 |
| NW 49 ${ }^{\text {th }} / 35^{\text {th }}$ Street Phase 2C [7] | Marion County TIP [5] | \$5,700,000 | ROW-A | 2020/21 |
| NW 49 ${ }^{\text {th }} / 35^{\text {th }}$ Street Phase 2C [7] | Marion County TIP [5] | \$8,419,862 | CST | 2024/25 |
| NW 49 ${ }^{\text {th }} / 35^{\text {th }}$ Street Phase 3A [8] | Marion County TIP [5] | \$2,000,000 | CST | 2020/21 |

[1] PHASES: ROW Right of Way; CST Construction; PD\&E Project Development \& Environment; PE Preliminary Engineering; DES Design
[2] Ocala/Marion TPO Transportation Improvement Program FY 2020/21-2024/25
[3] FDOT FIVE-YEAR Work Program FY 2021-2025
[4] FDOT State Transportation Improvement Program (STIP) FY 2020-2024
[5] Phase 2B NW 49th $/ 35^{\text {th }}$ Street From: NE 35 th Street To: North End of Limerock Pit
[6] Marion County TIP FY 2020/21-2024/25
[7] Phase 2C NW 49th $/ 35^{\text {th }}$ Street From: NW 44 ${ }^{\text {th }}$ Avenue To: North End of Limerock Pit
[8] Phase 3A NW $49^{\text {th }} / 35^{\text {th }}$ Street From: 1.1 mi W of NW $44^{\text {th }}$ Avenue To: NW $44^{\text {th }}$ Avenue

## 3 Existing Conditions

This section provides an overview of the existing conditions within the IJR AOI. The purpose of the existing conditions analyses is to provide a basis for comparison and to establish a framework for the project need.

As discussed previously, the proposed interchange would be located along I-75 at the planned extension of NW 49 ${ }^{\text {th }}$ Street in Marion County, Florida. The interchange would be located at Milepost 356, north of US 27 (Milepost 354) and south of SR 326 (Milepost 358). The study interchange is located approximately 2.2 miles north of the I-75 and US 27 interchange and approximately 2.0 miles south of the I-75 and SR 326 interchange.

### 3.1 Existing Transportation Network

US 27 and SR 326 are both four-lane divided arterials, with the following 2017 AADTs; vehicles per day (vpd), along each segment obtained from 2017 Florida Traffic Online (FTO) or traffic counts; count data source details provided in Section 3.4.
US 27

- West of NW $44^{\text {th }}$ Avenue $20,700 \mathrm{vpd}$
- East of NW 44 ${ }^{\text {th }}$ Avenue to I-75 31,100 vpd
- I-75 to NW $35^{\text {th }}$ Avenue Road $29,100 \mathrm{vpd}$
- East of NW $35^{\text {th }}$ Avenue Road $25,000 \mathrm{vpd}$


## SR 326

- West of NW $44^{\text {th }}$ Avenue $10,300 \mathrm{vpd}$
- NW $44^{\text {th }}$ Avenue to I-75

18,400 vpd

- East of I-75
$23,400 \mathrm{vpd}$
US 27 connects to US 441/US 301 and SR 40; passes through downtown Ocala and is one of the primary arterial roadways in this region. SR 326 is also an important roadway facility which by-passes Downtown Ocala and allows improved connectivity to I-75, US 301 and SR 40, north of the City of Ocala.

The existing I-75 and US 27 interchange is a diamond interchange with signalized ramp terminal intersections on US 27 and single lane merge and diverge ramp gores on I-75; shown on Figure 3-1, from the FDOT Aerial Photo Lookup System (APLUS). The southbound ramp is a single lane approach with a left turn and channelized right turn onto US 27; the northbound ramp has dual left and dual right turn approach lanes onto US 27. The speed limit is 70 miles per hour (mph) and 45 mph on this section of I-75 and US 27, respectively.


Figure 3-1: I-75 at US 27 Interchange

The I-75 and SR 326 interchange (Figure 3-2) is a modified diamond interchange with a westbound SR 326 to southbound I-75 loop ramp located in the northwest quadrant of the interchange. NW $44^{\text {th }}$ Avenue forms the south leg of the I-75 southbound off-ramp intersection with SR 326. The speed limit is 70 mph and 45 mph on this section of $\mathrm{I}-75$ and SR 326 , respectively.

The following existing signalized and two-way stop controlled (TWSC) intersections are within the AOI of the proposed interchange:

1. US 27 at NW $44^{\text {th }}$ Avenue
2. US 27 at I-75 southbound ramps
3. US 27 at I-75 northbound ramps
4. US 27 at NW $35^{\text {th }}$ Avenue Road
5. NW 49 ${ }^{\text {th }}$ Street at NW $44^{\text {th }}$ Avenue (TWSC)
6. SR 326 at I-75 southbound ramps/NW $44^{\text {th }}$ Avenue
7. SR 326 at I-75 northbound ramps

The AOI is shown on Figure 2-5; and the existing intersection lane configurations on Figure 33.

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Figure 3-2: I-75 at SR 326 Interchange


Figure 3-3: Existing Lane Configuration

### 3.2 Land Use

The area east of I-75 is primarily rural and is mainly comprised of large tracts of undeveloped land. The area west of I-75 contains several residential subdivisions. Commercial development is present along US 27 both to the east and to the west of I-75. Additional subdivisions are present along US 27 as well, though these are located outside the AOI. There are a few commercial parcels along SR 326 in the immediate vicinity of the l-75 interchange. NW $44^{\text {th }}$ Avenue indirectly connects several subdivisions and some industrial parcels with the two existing interchanges at US 27 and SR 326.

The current comprehensive plan is year 2040; Marion County updated the 2035 Comprehensive Plan to establish an area of intense commercial and industrial development to capitalize on and leverage readily available transportation routes. These routes include the surrounding major roadways and freight rail connections (including the " S " Line which runs through Marion County and the City of Ocala and connections to the CSX line which runs between Lakeland and Jacksonville). The 2035 Comprehensive Plan created Ocala 489 and contiguous commerce district/employment center totaling +/- 5000 acres; see Figure 3-4, Marion County Future Land Use Map (FLUM); a layout of Ocala 489 is provided on Figure 3-5. This State established, Florida Enterprise Zone is intended to be an economic engine for job creation in the region and includes a new Chewy Fulfillment Center, AutoZone Distribution Center, FedEx Ground Hub and a recent CSX "Select Site" designation. Select Sites are properties identified and vetted as capable locations for future manufacturing facilities along the CSX rail network. These sites can be developed quickly since standard land use issues and comprehensive due diligence items have already been addressed. This District also includes the proposed I-75 interchange at NW 49 ${ }^{\text {th }}$ Street.

The Phase 1 Freight Feasibility Study conducted to evaluate the viability of an Intermodal Logistic Center (ILC) in Ocala revealed that the area is a particularly competitive location for facilities that transfer freight between transportation modes or large and small vehicles; breaking down large "unit loads" into smaller or mixed loads; storage; manufacturing; and value-added processing. The preferred location of the ILC is adjacent to Ocala 489; as the site has direct access to rail and would be an ideal location for rail-served clients.


Figure 3-4: Future Land Use Map


Figure 3-5: Ocala 489 Layout

### 3.3 Base-Year (2015) Model Validation

Per the MLOU approved by FDOT in January 2018 and MLOU Amendment in September 2020, CFRPM version 6.1 was utilized to develop future traffic volume projections. Although the CFRPM 6.1 has a 2010 base year, a 2015 network and socioeconomic dataset was developed by the Department with input from the local MPO/TPO, for the area under the Ocala-Marion TPO. This model, provided by the Department, was used as a basis for the forecasting effort. The CFRPM 6.1 validation and subarea refinement was performed for the base year 2015. The work effort included identifying the traffic analysis zones (TAZ), and verifying socio-economic data, including population and employment. The roadway network was examined using GIS and Google Earth ${ }^{\text {TM }}$ to replicate the 2015 network with focus on Marion County.

The study area is defined in accordance with the FDOT IARUG as including l-75 from US 27 to SR 326 and extends from NW $44^{\text {th }}$ Avenue to NW $27^{\text {th }}$ Avenue. The CFRPM 6.1 with 2015 base year, also has a corresponding network and socioeconomic dataset for a horizon year of 2045.

A project model validation was performed to ensure the reasonableness of the daily traffic demand forecasts. During the project model validation, one interchange to the north (at SR 326) and one to the south (at US 27) of the proposed NW 49 ${ }^{\text {th }}$ Street interchange were reviewed. Adjustments to the model, such as facility type, speed, and capacity, were made in order to accurately reflect the 2015 roadway network and improve the model performance, while maintaining or improving the validation statistics outside the study area. Consistent with the 2015 FTO Model Output Conversion Factor (MOCF), 0.97 was used for surface streets and 0.96 , for I-75. Comparisons were made for Volume-to-Count (V/C) ratios and Percent Root Mean Square Error (\%RMSE) between the original model validation, obtained from FDOT and the project model validation (refined) prior to using the model for future forecasts.

For the Refined 2015 CFRPM, using the sub-area model validation performed for the 2015 base year, corresponding validity factors were developed. The 2015 FTO AADTs were used for the 2015 "count" values and the 2015 Peak Season Weekly Average Daily Traffic (PSWADT) *MOCF model output for the AADT; 2015 "volume" values. Validity factor (A) = 2015 volumecount difference and validity factor $(B)=2015$ volume/count ratio. Since FTO stations are not placed on all roadway segments, there are a significant number of segments in the CFRPM network without corresponding FTO stations. However, the model outputs for all segments within the study area must also be adjusted. For these segments, the adjustment factors developed for adjacent, segments are applied. For segments that currently do not exist or are not reflected in
the CFRPM roadway network, a roadway segment in close proximity with comparable characteristics is selected. The FTO station locations selected are considered reference stations and are reflected as such. This process is summarized for the analysis segments in Table 3-1. The FDOT Project Traffic Assumption Form and details of the sub-area model validation are provided in Appendix C.

Table 3-1: CFRPM Validity Factors

| Roadway | Segment | FTO Station | 2015 <br> Count | CFRPM <br> Volume | (A) <br> Vol-Count | (B) <br> Vol/Count |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I-75 <br> Mainline | N of SR 326 Interchange <br> $N$ of Proposed Interchange <br> N of US 27 Interchange <br> S of US 27 Interchange | 360437 | 47,500 | 55,100 | 7,600 | 1.16 |
|  |  | 360438 | 65,500 | 62,800 | -2,700 | 0.96 |
|  |  | 360438 |  |  | -2,700 | 0.96 |
|  |  | 360439 | 69,500 | 71,900 | 2,400 | 1.03 |
| I-75 at US 27 Interchange | US 27 W of I-75 US 27 E of I-75 | 360459 |  |  | 2,100 | 1.11 |
|  |  | 360033 |  |  | -200 | 0.99 |
|  | I-75 NB Off-Ramp <br> I-75 NB On-Ramp <br> I-75 SB Off-Ramp <br> I-75 SB On-Ramp | 362012 | 5,900 | 6,600 | 700 | 1.12 |
|  |  | 362013 | 2,000 | 2,000 | 0 | 1.00 |
|  |  | 362014 | 2,100 | 2,100 | 0 | 1.00 |
|  |  | 362015 | 6,300 | 6,700 | 400 | 1.06 |
| US 27 at NW 44 Avenue | NW 44 Avenue N of US 27 NW 44 Avenue S of US 27 US 27 W of NW 44 Avenue US 27 E of NW 44 Avenue | 368029/C-29 | 7,900 | 8,400 | 500 | 1.06 |
|  |  | 368029/C-29 |  |  | 500 | 1.06 |
|  |  | 360459 | 18,700 | 20,800 | 2,100 | 1.11 |
|  |  | 360459 |  |  | 2,100 | 1.11 |
| US 27 at <br> NW 35 Avenue <br> Road | NW 35 Ave Rd N of US 27 NW 35 Ave Rd S of US 27 US 27 W of NW 35 Ave Rd US 27 E of NW 35 Ave Rd | 367008/C-21 | 4,300 | 6,200 | -3,100 | 0.28 |
|  |  |  |  |  |  |  |
|  |  | 360033 |  |  | -200 | 0.99 |
|  |  | 360033 | 22,000 | 21,800 | -200 | 0.99 |
| NW 49 Street at NW 44 Avenue | NW 44 Avenue N of NW 49 Street NW 44 Avenue S of NW 49 Street NW 49 Street W of NW 44 Avenue NW 49 Street E of NW 44 Avenue | 368029/C-29 |  |  | 500 | 1.06 |
|  |  | 368029/C-29 |  |  | 500 | 1.06 |
|  |  | [2] |  |  |  |  |
|  |  | 368039/C-25 |  |  | -2,300 | 0.61 |
| I-75 at <br> NW 49 Street Interchange | NW 49 Street W of I-75 NW 49 Street E of I-75 | 368039/C-25 |  |  | -2,300 | 0.61 |
|  |  | 368039/C-25 |  |  | -2,300 | 0.61 |
|  | I-75 NB Off-Ramp <br> I-75 NB On-Ramp <br> I-75 SB Off-Ramp <br> I-75 SB On-Ramp | [1] |  |  | -1,133 | 0.77 |
|  |  | [1] |  |  | -1,133 | 0.77 |
|  |  | [1] |  |  | -1,133 | 0.77 |
|  |  | [1] |  |  | -1,133 | 0.77 |
| I-75 at <br> SR 326 <br> Interchange | SR 326 W of I-75 SR 326 E of I-75 | MAP A-7 | 6,800 | 2,300 | -4,500 | 0.34 |
|  |  | 360465 | 19,500 | 20,500 | 600 | 1.03 |
|  | I-75 NB Off-Ramp I-75 NB On-Ramp I-75 SB Off-Ramp I-75 SB On-Ramp I-75 SB Loop Ramp | 362016 | 10,000 | 6,800 | -3,200 | 0.68 |
|  |  | 362017 | 4,500 | 2,400 | -2,100 | 0.53 |
|  |  | 362018 | 4,100 | 2,400 | -1,700 | 0.59 |
|  |  | 362019 | 3,400 | 200 | -3,200 | 0.06 |
|  |  | 362024 | 6,600 | 5,500 | -1,100 | 0.83 |
| Reference Station | NW 35 ST/NW 27 Ave NW 27 Ave S of NW 21 ST | 368039/C-25 | 5,900 | 3,600 | -2,300 | 0.61 |
|  |  | 367008/C-21 | 4,300 | 1,200 | -3,100 | 0.28 |

36XXXX - Location references an adjacent or comparable station for factors; [1] AVG OF US 27 \& SR 326 Ramps; [2] No Comparable Road

### 3.4 Existing Year Traffic Count Data

Turning Movement Counts (TMCs) and 72-Hour Classification Counts were collected for the study intersections and roadway systems within the AOI. In addition to collecting traffic counts, data was obtained from the FDOT 2017 FTO and the Ocala/Marion TPO 2013-2017 Traffic Counts \& Trends Manual. The County counts were used for comparison and supplemented FDOT counts as necessary. For locations where count data is not consistent between sources, counts on adjacent segments and historical count data were considered and the most appropriate data source was selected; source details are provided in Appendix D.

Per the approved MLOU, 72-hour bi-directional classification counts were collected between September $26^{\text {th }}$ and September $28^{\text {th }}$, 2017. Count data for the same days at stations along I-75 was obtained from FDOT. Volumes on I-75 range from 75,000 vpd south of US 27 to 56,500 vpd north of SR 326; on US 27 from 20,700 vpd west of NW $44^{\text {th }}$ Avenue, 31,100 vpd and 29,100 vpd adjacent to the interchange and 25,000 vpd east of NW 35 th Avenue Road; and on SR 326 from 10,300 vpd west of NW $44^{\text {th }}$ Avenue to $23,400 \mathrm{vpd}$ east of the interchange. Based on the 72-hour counts, the predominant peak periods fell between the hours of 7:00 AM-9:00 AM and 4:00 PM-6:00 PM; therefore, the TMCs were collected at the following intersections during these times. From the TMCs, global intersection peak hours of 7:15 AM-8:15 AM and 4:30 PM-5:30 PM were selected based on the peak sum of TMCs for surface streets. The raw count data is provided in Appendix D.

- US 27 at I-75 northbound ramps
- US 27 at I-75 southbound ramps
- US 27 at NW 35 ${ }^{\text {th }}$ Avenue Road
- US 27 at NW 44 ${ }^{\text {th }}$ Avenue
- NW 49 ${ }^{\text {th }}$ Street at NW 44 ${ }^{\text {th }}$ Avenue
- SR 326 at I-75 northbound ramps
- SR 326 at I-75 southbound ramps/NW $44^{\text {th }}$ Avenue


### 3.5 Existing Year Traffic

The raw traffic data was adjusted following the procedures set forth in the 2019 FDOT Project Traffic Forecasting Handbook. The classification counts were reviewed including the percent heavy vehicles (\% Truck) and directional (D) split for each location. Based on the results, D was established for surface street segments. An I-75 mainline D-factor was developed using the 5year average (2013-2017) D for the corresponding locations; obtained from the 2017 FDOT

FTO. The daily \%Trucks (\%TDaily) for I-75 mainline was developed the same way. Classification count data was used to establish the $\% \mathrm{~T}_{\text {Daily }}$ for ramps and roadway segments (surface street). Table 3-2 summarizes the existing year (2017) AADT, TDaily and D; detailed breakdown of calculations provided in Appendix E. The Peak Hour Factors (PHF) obtained from the data collection were maintained for Existing Conditions.

Table 3-2: 2017 Existing AADT

| Roadway | Segment | $\begin{gathered} \text { Existing } \\ 2017 \end{gathered}$ | Count Station | Data Source ${ }^{1,2,3}$ | T Daily | D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1-75$ <br> Mainline | N of SR 326 Interchange <br> N of NW 49 Street Interchange (Build) <br> N of US 27 Interchange <br> S of US 27 Interchange | $\begin{aligned} & 56,500 \\ & 76,000 \\ & 76,000 \\ & 75,000 \end{aligned}$ | $\begin{aligned} & 360437 \\ & 360438 \\ & 360438 \\ & 360439 \end{aligned}$ | $\begin{aligned} & \text { FTO } \\ & \text { FTO } \\ & \text { FTO } \\ & \text { FTO } \end{aligned}$ | $\begin{aligned} & 0.191 \\ & 0.233 \\ & 0.233 \\ & 0.223 \end{aligned}$ | $\begin{aligned} & 0.543 \\ & 0.543 \\ & 0.543 \\ & 0.543 \end{aligned}$ |
| I-75 at <br> US 27 Interchange | US 27 W of I-75 US 27 E of I-75 | $\begin{aligned} & 31,100 \\ & 29,100 \end{aligned}$ |  | COUNT COUNT | $\begin{aligned} & 0.147 \\ & 0.363 \end{aligned}$ | $\begin{aligned} & 0.625 \\ & 0.617 \end{aligned}$ |
|  | I-75 NB Off-Ramp <br> I-75 NB On-Ramp <br> I-75 SB Off-Ramp <br> I-75 SB On-Ramp | $\begin{aligned} & 8,100 \\ & 2,200 \\ & 2,800 \\ & 7,500 \end{aligned}$ | $\begin{aligned} & 362012 \\ & 362013 \\ & 362014 \\ & 362015 \end{aligned}$ | COUNT COUNT COUNT COUNT | $\begin{aligned} & 0.218 \\ & 0.300 \\ & 0.140 \\ & 0.160 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.000 \\ & 1.000 \\ & 1.000 \\ & 1.000 \\ & \hline \end{aligned}$ |
| US 27 at NW $44^{\text {th }}$ Avenue | NW 44 Avenue N of US 27 NW 44 Avenue S of US 27 US 27 W of NW 44 Avenue US 27 E of NW 44 Avenue | $\begin{array}{r} 8,900 \\ 400 \\ 20,700 \\ 31,100 \end{array}$ | 368029/C-29 $360459$ | $\begin{gathered} \text { TPO } \\ \text { TMC }^{3} \\ \text { FTO } \\ \text { COUNT } \end{gathered}$ | $\begin{aligned} & 0.056 \\ & 0.379 \\ & 0.102 \\ & 0.940 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.525 \\ & 0.632 \\ & 0.587 \\ & 0.597 \\ & \hline \end{aligned}$ |
| US 27 at <br> NW $35^{\text {th }}$ Avenue <br> Road | NW 35 Ave Rd N of US 27 NW 35 Ave Rd S of US 27 US 27 W of NW 35 Ave Rd US 27 E of NW 35 Ave Rd | $\begin{array}{r} 7,500 \\ 1,400 \\ 29,100 \\ 25,000 \end{array}$ | 360033 | COUNT COUNT COUNT COUNT | $\begin{aligned} & 0.167 \\ & 0.055 \\ & 0.165 \\ & 0.169 \end{aligned}$ | $\begin{aligned} & 0.535 \\ & 0.650 \\ & 0.617 \\ & 0.641 \end{aligned}$ |
| NW 49 ${ }^{\text {th }}$ Street at NW 44 ${ }^{\text {th }}$ Avenue | NW 44 Avenue N of NW 49 Street NW 44 Avenue S of NW 49 Street NW 49 Street W of NW 44 Avenue NW 49 Street E of NW 44 Avenue | $\begin{array}{r} 7,000 \\ 7,100 \\ 150 \end{array}$ | N/A | COUNT COUNT TMC | $\begin{aligned} & 0.040 \\ & 0.078 \\ & 0.000 \end{aligned}$ | $\begin{aligned} & 0.650 \\ & 0.539 \\ & 0.636 \end{aligned}$ |
| Proposed I-75 at NW 49 ${ }^{\text {th }}$ Street Interchange | NW 49 Street W of I-75 NW 49 Street E of I-75 |  |  |  |  |  |
|  | I-75 NB Off-Ramp <br> I-75 NB On-Ramp <br> I-75 SB Off-Ramp <br> I-75 SB On-Ramp |  |  |  |  |  |
| $\begin{aligned} & \text { I-75 at } \\ & \text { SR } 326 \end{aligned}$ <br> Interchange | SR 326 W of I-75 SR 326 E of I-75 | $\begin{aligned} & 10,300 \\ & 23,400 \end{aligned}$ | MAP A-7 | COUNT COUNT | $\begin{aligned} & 0.231 \\ & 0.175 \end{aligned}$ | $\begin{aligned} & 0.621 \\ & 0.548 \end{aligned}$ |
|  | I-75 NB Off-Ramp I-75 NB On-Ramp I-75 SB Off-Ramp I-75 SB On-Ramp I-75 SB Loop Ramp | $\begin{array}{r} 11,000 \\ 3,300 \\ 4,700 \\ 3,400 \\ 5,900 \end{array}$ | $\begin{aligned} & 362016 \\ & 362017 \\ & 362018 \\ & 362019 \\ & 362024 \end{aligned}$ | $\mathrm{FTO}^{2}$ COUNT $\mathrm{FTO}^{2}$ COUNT COUNT | $\begin{aligned} & 0.218 \\ & 0.380 \\ & 0.218 \\ & 0.240 \\ & 0.260 \end{aligned}$ | $\begin{aligned} & 1.000 \\ & 1.000 \\ & 1.000 \\ & 1.000 \\ & 1.000 \end{aligned}$ |

[^2]The I-75 mainline daily peak direction is southbound during the PM peak. Therefore, the D-factor previously established was applied to I-75 northbound direction during the AM peak hour, with corresponding balance applied to the southbound direction. Conversely for the PM peak hour, the D-factor was applied to southbound direction. For the AM and PM peak hours on the surface streets, directional splits were extracted from the classification counts corresponding to the global peak hours (7:15-8:15 AM and 4:30-5:30 PM).

For the I-75 mainline segments, peak hour \%Trucks (\%TPeak) was developed using \%TDaily $/ 2$. For the roadway segment/ intersection approaches, the approach \%T was determined from TMCs. Then, location specific $\% T_{\text {Peak }}$ were established for each roadway and I-75 ramp; for the peak hour analysis. The resulting \% TPeak for each location is summarized in Table 3-3; detailed breakdown of calculations are provided in Appendix E. It should be noted that with availability of 2019 FTO, data corresponding to the study locations were reviewed. Arterial volumes in general, remained the same as the 2017 (existing) data. There was an increase in volumes on the I-75 mainline, south of US 27 and north of SR 326; details provided in Appendix D.

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Table 3-3: Recommended Peak Hour \%Trucks for Analysis

| Segment | Description | Analysis $\%_{\text {Peak }}$ |
| :---: | :---: | :---: |
| I-75 Mainline | North of SR 326 Interchange | 0.10 |
|  | From SR 326 Interchange to NW 49 Street Interchange | 0.12 |
|  | From NW 49 Street Interchange to US 27 Interchange | 0.12 |
|  | South of US 27 Interchange | 0.11 |
| SR 326 | From NW 44 Ave to I-75 SB Ramps From I-75 SB Ramps to I-75 NB Ramps East of I-75 NB Ramps | 0.17 |
| SR 326 <br> Interchange <br> Ramps | I-75 SB Off-Ramp <br> I-75 NB On-Ramp <br> NB Off-Ramp <br> I-75 SB On-Ramp | 0.23 |
| US 27 | From NW 44 Ave to l-75 SB Ramps From I-75 SB Ramps to I-75 NB Ramps From I-75 NB Ramps to NW 35 Ave Rd East of NW 35 Ave Rd | 0.06 |
| US 27 Interchange | I-75 SB Off-Ramp I-75 NB On-Ramp | 0.06 |
| Ramps | NB Off-Ramp I-75 SB On-Ramp | 0.14 |
| NW 49 Street | From NW 44 Ave to l-75 SB Ramps From I-75 SB Ramps to I-75 NB Ramps East of I-75 NB Ramps |  |
| NW 49 Street Interchange Ramps | I-75 SB Off-Ramp I-75 NB On-Ramp NB Off-Ramp I-75 SB On-Ramp |  |
| NW 44 Avenue | South of SR 326 <br> North of NW 49 St <br> South of NW 49 Street | 0.10 |
|  | North of US 27 <br> South of US 27 | 0.02 |
| NW 35 Avenue Road | North of US 27 <br> South of US 27 | 0.10 |

Note: \%TPeak for NW 49 Street \& proposed Interchange discussed in Section 5.
Figure 3-6 illustrates the balanced volumes for intersections within the IJR AOI. The balanced intersection worksheets, are provided in Appendix E.


Figure 3-6: Existing Balanced Intersection Volumes (2017)

### 3.6 Existing Operational Performance

The LOS for the existing conditions was determined using the most current procedures as outlined in the HCM 2010. Per the approved MLOU, the analysis was performed for the peak hours established in Section 3.4 using the methodologies documented in the HCM 2010 as applied using HCS 6.8 and Synchro 10. It should be noted that HCM 2000 was used under certain phasing and lane configuration conditions that are not recognized by HCM 2010 analysis methodologies. Specific analysis techniques utilized in this study included procedures for basic freeway segments, merge/diverge analysis as well as stop controlled and signalized intersection analysis.

### 3.6.1 LOS Targets

Roadways within the AOI were evaluated to determine the operating LOS. The purpose of this evaluation is to identify any deficiency in the existing system. LOS is a qualitative measure of the effect of a number of factors including speed and travel time, traffic interruptions due to traffic signals, freedom to maneuver, safety, driving comfort, convenience, and operating cost. LOS is designated as "A" through "F" and covers the entire range of traffic operation for transportation facilities. LOS " $A$ " represents the best operating condition while LOS " $F$ " represents the worst.

The LOS targets for the study segments are presented in Table 3-4 based upon FDOT District 5 LOS Summary Report, consistent with FDOT Policy 000-525-006c Level of Service for the State Highway System (SHS), and the Transportation Element of the Ocala and Marion County Comprehensive Plans.

Table 3-4: LOS Targets

| Roadway | Location/Segment | LOS Target |
| :--- | :--- | :---: |
| I-75 | North of SR 326 | C |
| I-75 | South of US 27 to south of SR 326 | D |
| US 27 | West of I-75 to east of NE 35 ${ }^{\text {th }}$ Ave | D |
| SR 326 | West of I-75 to east of I-75 | D |

### 3.6.2 Existing LOS Analyses

Figures 3-7 and 3-8 present the existing segmented breakdown of the I-75 mainline and interchange ramps by segment type, segment length and speed, change lane length, peak hour volume, and \%Trucks. The figure also summarizes the HCS analysis results for mainline segment (basic freeway) and merge/diverge (ramp junction) locations; speed, density and LOS. The analyses indicate that the existing I-75 segments and merge/diverge areas are operating within LOS targets. A detailed breakdown of calculations; mainline and ramp volumes; along with HCS Analysis worksheets are provided in Appendix E.

Table 3-5 summarizes the Synchro analysis results for intersection approach, overall intersection delay and LOS. The overall LOS at each intersection meets the LOS D target. However, the southbound approach at the intersection of US 27 and NW 35 ${ }^{\text {th }}$ Avenue Road operates at LOS F during the AM and PM peak hours. In addition, the northbound approaches at the US 27 intersections of NW $35^{\text {th }}$ Avenue Road and NW $44^{\text {th }}$ Avenue operate at LOS E during the PM peak hour. It should be noted that Yield controlled right turn movements at the I75 and SR 326 off-ramps were coded in Synchro as signalized with permitted right turn on red; since HCM2010 methodology omits Yield and Stop controlled movements at signalized intersections. HCM2000 was used for SR 326 at I-75 northbound ramps since HCM2010 generated an unrealistic LOS (over $500 \mathrm{sec} / \mathrm{veh}$ delay for the northbound right turn movement). Synchro Analysis worksheets are provided in Appendix E.

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Figure 3-7: Existing (2017) AM 1-75 Segment \& Merge/Diverge Analysis Summary


Figure 3-8: Existing (2017) PM I-75 Segment \& Merge/Diverge Analysis Summary


Table 3-5: Existing (2017) Intersection Delay and LOS

| Intersection | DIR | AM Peak |  |  |  | PM Peak |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | App. |  | Int. |  | App. |  | Int. |  |
|  |  | Delay ${ }^{1}$ | LOS | Delay ${ }^{1}$ | LOS | Delay ${ }^{1}$ | LOS | Delay ${ }^{1}$ | LOS |
| NW 44 Ave at US 27 | EB | 19.9 | B | 21.5 | C | 13.2 | B | 21.1 | C |
|  | WB | 20.1 | C |  |  |  | C |  |  |
|  | NB | 39.2 | D |  |  | 56.3 | E |  |  |
|  | SB | 26.9 | C |  |  | 34.9 | C |  |  |
| I-75 SB at US 27 | EB |  |  | 15.7 | B | 19.6 | B | 11.7 | B |
|  | WB | 6.1 | A |  |  | 4.6 | A |  |  |
|  | NB |  |  |  |  |  |  |  |  |
|  | SB | 53.3 | D |  |  | 54.6 | D |  |  |
| I-75 NB at US 27 | EB | 1.2 | A | 12.7 | B | 1.1 | A | 14.3 | B |
|  | WB | 13.0 | B |  |  | 13.4 | B |  |  |
|  | NB |  |  |  |  |  | D |  |  |
|  | SB |  |  |  |  |  |  |  |  |
| NW 35 Ave Rd at US 27 | EB | 29.9 | C | 38.9 | D | 37.0 | D | 51.1 | D |
|  | WB | 30.9 | C |  |  | 53.2 | D |  |  |
|  | NB | 54.5 | D |  |  | 56.9 | E |  |  |
|  | SB | 95.4 | F |  |  | 94.0 | F |  |  |
| NW 44 Ave at NW 49 ST (Int. LOS reflective of Stop controlled movement) | EB | 11.7 | B | 11.7 | B |  | A | 9.9 | A |
|  | WB |  |  |  |  |  |  |  |  |
|  | NB | 0.2 | A |  |  | 0.2 | A |  |  |
|  | SB | 0.0 | A |  |  | 0.0 | A |  |  |
| NW 44 Ave/l-75 SB Off at SR 326 | EB | 14.3 | B | 16.1 | B | 15.1 | B | 17.6 | B |
|  | WB | 14.4 | B |  |  | 14.9 | B |  |  |
|  | NB | 26.1 | C |  |  | 25.6 | C |  |  |
|  | SB |  | B |  |  | 19.7 | B |  |  |
| I-75 SB On-Ramp (Loop) at SR 326 | EB | 0.0 | A | 2.5 | A | 0.0 | A | 1.4 | A |
|  | WB | 3.3 | A |  |  | 1.8 | A |  |  |
|  | NB | 10.6 | B |  |  | 10.6 | B |  |  |
| $\begin{gathered} \text { I-75 NB Off/I-75 NB On } \\ \text { at SR } 326^{2} \end{gathered}$ | EB | 7.8 | A | 21.7 | C | 7.7 | A | 21.8 | C |
|  | WB | 20.9 | C |  |  | 20.5 | C |  |  |
|  | NB |  | C |  |  |  | C |  |  |
|  | SB |  |  |  |  |  |  |  |  |

${ }^{1}$ Delay in sec/veh; ${ }^{2}$ LOS results based on HCM 2000 methodology.

### 3.7 Vissim Model Calibration

A network analysis was performed using PTV Vissim software version 20.00-07 to evaluate the entire corridor as a system. The calibration and validation methodologies have been documented per the guidelines set forth in the 2014 FDOT Traffic Analysis Handbook. Documentation includes a summary of the model verification methodology, any assumptions
and modeling issues, and a detailed calibration methodology. Default Vissim Parameters were used during the calibration process. Calibration data includes: Volume, Speed and Queuing/Visualization. Queue lengths measured from Vissim are based on actual queue lengths generated by the simulation, including maximum queue and average queue lengths.

The analysis was conducted for the AM and PM peak period for the existing year (2017). The following Measures of Effectiveness (MOEs) were used:

- Intersections
o Volume (vph)
o Delay (seconds/vehicle)
o Queues (feet)
- Roadway Links
o Average Speed (mph)
o Travel Times (seconds)
- Freeway Links
o Average Speed (mph)
o Density (veh/mi/ln)
o Volume (vph)
- Network
o Total Delay (hrs)
o Total Stops (\# of stops)
o Average Speed (mph)
o Vehicles Arrived
o Vehicle-Miles Traveled (VMT)
o Latent Delay (hrs)
o Latent Demand


### 3.7.1 Base Vissim Model Development

The following sections describe the data inputs and calibration targets used for development of the Vissim model.

### 3.7.1.1 Roadway Geometry

The FDOT APLUS aerials shown on Figures 3-1 and 3-2, were used to develop the roadway geometry. Lane configurations, turn bay storage lengths, and stop bar locations were verified in the field visit during the data collection effort and with 2018 Google Earth ${ }^{\text {TM }}$.

### 3.7.1.2 Vehicle Inputs and Routing Decisions

The AM and PM traffic volume inputs were coded with a 15-minute initialization interval followed by a three-hour period in 15-minute intervals (13 total intervals); with the second hour being the peak hour. Table 3-6 summarizes the peak hour entry link flow rates. The 15-minute interval
flow rates used for the Vissim analysis were calculated by multiplying the peak hour flow rates presented in Table 3-6 by 15 -minute volume ratios. The 15 -minute volume ratios were developed based on total entering volume for each 15-minute divided by the total entering peak hour volume. Detailed calculations are provided in Appendix E. Static Routing (predetermined paths) was used for all routes. Given the number of access points between each major intersection, a few minor streets were coded with estimated turn volumes in order to balance the volumes within the network.

Table 3-6: Entry Link Flow Rates (vph)

| Vehicle Input |  | AM <br> Peak | PM <br> Peak |
| :---: | :---: | :---: | :---: |
| 1 | NB NW 44 ${ }^{\text {th }}$ Avenue from NW 49 ${ }^{\text {th }}$ Street | 145 | 300 |
| 2 | SB NW 44 ${ }^{\text {th }}$ Avenue from NW 49 ${ }^{\text {th }}$ Street | 317 | 249 |
| 3 | EB NW 49 ${ }^{\text {th }}$ Street from NW 44 ${ }^{\text {th }}$ Avenue | 5 | 10 |
| 4 | EB S.R. 326 from I-75 SB | 316 | 281 |
| 5 | WB S.R. 326 from I-75 NB | 845 | 859 |
| 6 | NB NW 35 ${ }^{\text {th }}$ Avenue Road from US 27 | 17 | 28 |
| 7 | SB NW 35 ${ }^{\text {th }}$ Avenue Road from US 27 | 283 | 284 |
| 8 | WB US 27 from NW 35 ${ }^{\text {th }}$ Avenue Road | 672 | 1206 |
| 9 | NB NW 44 ${ }^{\text {th }}$ Avenue from US 27 | 17 | 12 |
| 10 | SB NW 44 ${ }^{\text {th }}$ Avenue from US 27 | 409 | 349 |
| 11 | EB US 27 from NW 44 ${ }^{\text {th }}$ Avenue | 810 | 690 |
| 12 | NB Donut from S.R. 326 | 71 | 40 |
| 13 | NB NW 38 ${ }^{\text {th }}$ Avenue from US 27 | 26 | 26 |
| 14 | SB I-75 North of S.R. 326 | 1165 | 1619 |
| 15 | NB I-75 South of US 27 | 2446 | 2519 |
| 16 | NB NW 44 ${ }^{\text {th }}$ Ave S of SR 326 | 86 | 115 |
| 17 | Dummy Entrance on US 27 | 123 | 114 |

### 3.7.1.3 Speed Distributions

Network links were coded with "Desired Speed Decisions" and "Reduced Speed Areas" to control vehicle speeds in the Vissim models and accurately simulate the vehicle speeds within the study area. The Desired Speed Decisions were defined based on the posted speed limits. Reduced Speed Areas were coded at locations that require vehicles to reduce their speed; typical locations include ramps and turning movements. Table 3-7 summarizes the "Desired Speed Distributions".

Table 3-7: Desired Speed Decisions

| Desired Speed | Minimum (mph) | Maximum (mph) |
| :---: | :---: | :---: |
| 30 mph | 29 | 33 |
| 35 mph | 34 | 38 |
| 40 mph | 39 | 43 |
| 45 mph | 40 | 50 |
| 70 mph | 65 | 90 |
| Right turns | 10 | 13 |
| Left turns | 15 | 18 |
| Channelized Right Turns | 25 | 28 |

### 3.7.1.4 Vehicle Compositions

Vissim is comprised of two main vehicle types, cars (Vehicle Type - Car - 10) and trucks or Heavy Goods Vehicle (Vehicle Type - HGV - 20). In addition, the two main types can be further broken into different model distributions. The standard North American Fleet vehicle class distribution was used for this modeling effort.

### 3.7.1.5 Traffic Control

Stop signs along with signal heads and detectors were coded into the network for traffic control based on the aerial imagery and field observations. The Ring Barrier Controller (RBC) signal timing files were developed using the data obtained from Marion County and the City of Ocala with Synchro 10 software and then imported into Vissim. Conflict areas were also coded and defined based on right-of-way rules and field observations.

### 3.7.1.6 Network Calibration

Calibration of Vissim Models involves adjusting default driver behavior (lane changing and carfollowing) parameters. The network calibration was performed in accordance to the 2014 FDOT Traffic Analysis Handbook which provides calibration parameter guidance and model calibration checklists.

### 3.7.2 Calibration Targets and Results

### 3.7.2.1 Calibration Targets

The calibration process was conducted as a combination of visual examination and evaluation of statistical model outputs. The following calibration targets were used based on the 2014 FDOT Traffic Analysis Handbook:

1) Traffic Volume
a. Simulated and measured link volumes for more than $85 \%$ of links to be:
i. Within 100 vehicles per hour (vph) for volumes less than 700 vph .
ii. Within $15 \%$ for volumes between 700 vph and 2700 vph .
iii. Within 400 vph , for volumes greater than 2700 vph .
b. Simulated and measured link volumes for more than $85 \%$ of links to have a GEH* statistic value of five (5) or lower.
c. Sum of link volumes within calibration area to be within $5 \%$.
d. Sum of link volumes to have a GEH* statistic value of 5 or lower.
2) Speed
a. Modeled average link speeds to be within the $\pm 10 \mathrm{mph}$ of field-measured speeds on at least $85 \%$ of all network links.
3) Queue Length
a. Difference between simulated and observed queue lengths to be within $20 \%$.
4) Visualization
a. Check consistency with field conditions for driver behavior, speed-flow relationship, queue lengths, lane utilization, congested links, bottlenecks; etc.
*GEH is an empirical formula expressed as $\sqrt{2 *(M-C)^{2} /(M+C)}$ where $M$ is the simulation model volume and $C$ is the field counted volume.

### 3.7.2.2 Calibration Results

Tables 3-8, 3-9, and 3-10 summarize the AM and PM peak hour calibration of the traffic volume, speed, and queue lengths. It should be noted that additional data was collected for the calibration of the Vissim model including speed data and queue length observations. Speed data was obtained from classification count data for which the road tube installations allow for this data extraction. In addition, queue lengths were extracted for one or more approaches per intersection utilizing video from turning movement count data collection. Summary of this additional data is provided in Appendix D. Speed data shows that the eastbound SR 326 segment east of I-75 does not meet the calibration target with the field speed data 19.9 mph lower than simulated. Although there is a significant difference in speed on the subject segment, it is likely due to vehicles slowing down to access nearby properties while in Vissim this segment is an exit link and therefore does not quantify the effects of nearby driveways. No eastbound SR 326 congestion was observed east of I-75 on SR 326 during data collection that would impact the operational integrity of the Vissim model. All results are based on 10 simulation runs, the use of 10 simulation runs is considered adequate per the 2014 FDOT Traffic Analysis Handbook. Visualization of the model simulation is consistent with the field conditions.

Queue length calibration results presented in Table 3-10 show that 20 out of 32 observed queues meet the $20 \%$ threshold of which three (3) simulated queue lengths are within $21 \%$ of the observed queue lengths. Although 12 observed queue lengths are outside the $20 \%$ threshold, the difference in observed and simulated queue length is generally 3 passenger cars or less.

Table 3-8: Simulated versus Measured Link Volumes (vph)

| Input <br> Link | Location | AM Peak |  |  |  |  |  |  | PM Peak |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Field | Sim. | GEH | Diff. | \% Diff | MeetsTarget (Y/N) |  | Field | Sim. | GEH | Diff | \%Diff | Meets Target (Y/N) |  |
|  |  |  |  |  |  |  | GEH | $\begin{aligned} & \hline \text { Vol } \\ & \text { Diff } \end{aligned}$ |  |  |  |  |  | GEH | $\begin{aligned} & \hline \text { Vol } \\ & \text { Diff } \end{aligned}$ |
| 1 | I-75 SB Off-Ramp to SR 326 | 127 | 129 | 0.18 | -2 | -1.6\% | Y | Y | 288 | 288 | 0.00 | 0 | 0.0\% | Y | Y |
| 2 | I-75 NB Off-Ramp to SR 326 | 555 | 533 | 0.94 | 22 | 4.0\% | Y | Y | 618 | 595 | 0.93 | 23 | 3.7\% | Y | Y |
| 3 | I-75 SB On-Ramp from SR 326 | 143 | 142 | 0.08 | 1 | 0.7\% | Y | Y | 136 | 135 | 0.09 | 1 | 0.7\% | Y | Y |
| 4 | I-75 NB On-Ramp from SR 326 | 259 | 246 | 0.82 | 13 | 5.0\% | Y | Y | 173 | 161 | 0.93 | 12 | 6.9\% | Y | Y |
| 51 | I-75 SB from SR 326 (Loop) | 286 | 280 | 0.36 | 6 | 2.1\% | Y | Y | 389 | 387 | 0.10 | 2 | 0.5\% | Y | Y |
| 6 | I-75 SB Off-Ramp to US 27 | 162 | 155 | 0.56 | 7 | 4.3\% | $Y$ | Y | 162 | 155 | 0.56 | 7 | 4.3\% | Y | Y |
| 71 | I-75 NB On-Ramp from US 27 | 166 | 164 | 0.16 | 2 | 1.2\% | $Y$ | $Y$ | 182 | 176 | 0.45 | 6 | 3.3\% | Y | Y |
| 8 I | I-75 SB On-Ramp from US 27 | 545 | 539 | 0.26 | 6 | 1.1\% | Y | Y | 583 | 573 | 0.42 | 10 | 1.7\% | Y | Y |
| 9, 11 | I-75 NB Off-Ramp to US 27 | 539 | 536 | 0.13 | 3 | 0.6\% | Y | Y | 552 | 544 | 0.34 | 8 | 1.4\% | Y | Y |
| 21 | I-75 NB S of US 27 | 2446 | 2403 | 0.87 | 43 | 1.8\% | $Y$ | $Y$ | 2519 | 2469 | 1.00 | 50 | 2.0\% | Y | $Y$ |
| 25 | I-75 SB S of US 27 | 1850 | 1840 | 0.23 | 10 | 0.5\% | $Y$ | $Y$ | 2277 | 2259 | 0.38 | 18 | 0.8\% | Y | $Y$ |
| 29 | I-75 NB N of US 27 | 2073 | 2031 | 0.93 | 42 | 2.0\% | Y | Y | 2149 | 2100 | 1.06 | 49 | 2.3\% | Y | Y |
| 331 | I-75 SB N of US 27 | 1467 | 1458 | 0.24 | 9 | 0.6\% | $Y$ | $Y$ | 1856 | 1844 | 0.28 | 12 | 0.6\% | Y | $Y$ |
| 41 | I-75 NB S of SR 326 | 2073 | 2028 | 0.99 | 45 | 2.2\% | $Y$ | $Y$ | 2149 | 2088 | 1.33 | 61 | 2.8\% | Y | Y |
| 45 | I-75 SB S of SR 326 | 1467 | 1456 | 0.29 | 11 | 0.7\% | Y | Y | 1856 | 1850 | 0.14 | 6 | 0.3\% | Y | Y |
| 491 | I-75 NB N of SR 326 | 1777 | 1740 | 0.88 | 37 | 2.1\% | Y | Y | 1704 | 1653 | 1.24 | 51 | 3.0\% | Y | Y |
| 52 | I-75 SB N of SR326 | 1165 | 1159 | 0.18 | 6 | 0.5\% | Y | Y | 1619 | 1618 | 0.02 | 1 | 0.1\% | Y | Y |
| 61 | SR 326 EB W of I-75 | 316 | 309 | 0.40 | 7 | 2.2\% | Y | Y | 281 | 274 | 0.42 | 7 | 2.5\% | Y | Y |
| 64 | SR 326 WB W of I-75 | 300 | 301 | 0.06 | -1 | -0.3\% | Y | Y | 437 | 437 | 0.00 | 0 | 0.0\% | Y | Y |
| 65 | NW 44 Ave NB S of SR 326 | 86 | 78 | 0.88 | 8 | 9.3\% | Y | Y | 115 | 109 | 0.57 | 6 | 5.2\% | Y | Y |
| 67 | NW 44 Ave SB S of SR 326 | 80 | 82 | 0.22 | -2 | -2.5\% | Y | $Y$ | 68 | 65 | 0.37 | 3 | 4.4\% | Y | $Y$ |
| 69 | SR 326 EB E of I-75 | 834 | 803 | 1.08 | 31 | 3.7\% | Y | Y | 957 | 933 | 0.78 | 24 | 2.5\% | Y | Y |
| 71 | SR 326 WB E of I-75 | 845 | 837 | 0.28 | 8 | 0.9\% | Y | Y | 862 | 850 | 0.41 | 12 | 1.4\% | Y | Y |
| 73 | US 27 EB W of I-75 | 1198 | 1269 | 2.02 | -71 | -5.9\% | $Y$ | Y | 982 | 1044 | 1.95 | -62 | -6.3\% | Y | $Y$ |
| 75 | US 27 WB W of I-75 | 695 | 740 | 1.68 | -45 | -6.5\% | $Y$ | $Y$ | 1250 | 1304 | 1.51 | -54 | -4.3\% | Y | $Y$ |
| 77 | US 27 EB E of I-75 | 1400 | 1407 | 0.19 | -7 | -0.5\% | Y | Y | 1090 | 1090 | 0.00 | 0 | 0.0\% | Y | Y |
| 79 | US 27 WB E of I-75 | 903 | 898 | 0.17 | 5 | 0.6\% | Y | Y | 1455 | 1418 | 0.98 | 37 | 2.5\% | Y | Y |
| 81 | US 27 EB E of NW 35 Ave Rd | 1198 | 1145 | 1.55 | 53 | 4.4\% | Y | Y | 982 | 873 | 3.58 | 109 | 11.1\% | Y | Y |
| 83 | US 27 WB E of NW 35 Ave Rd | 695 | 661 | 1.31 | 34 | 4.9\% | Y | Y | 1250 | 1167 | 2.39 | 83 | 6.6\% | Y | Y |
| 91 | NW 44 Av NB S of NW 49 St | 145 | 143 | 0.17 | 2 | 1.4\% | Y | Y | 300 | 284 | 0.94 | 16 | 5.3\% | Y | Y |
| 93 | NW 44 Av SB S of NW 49 St | 318 | 310 | 0.45 | 8 | 2.5\% | Y | $Y$ | 256 | 246 | 0.63 | 10 | 3.9\% | Y | Y |
| 95 | NW 44 Av NB N of NW 49 St | 148 | 144 | 0.33 | 4 | 2.7\% | Y | Y | 293 | 278 | 0.89 | 15 | 5.1\% | Y | Y |
| 97 | NW 44 Av SB N of NW 49 St | 317 | 309 | 0.45 | 8 | 2.5\% | Y | Y | 249 | 238 | 0.70 | 11 | 4.4\% | Y | Y |
| Sum of | Link Volumes | 26578 | 26275 | 1.86 | 303 | 1.1\% |  |  | 30039 | 29505 | 3.12 | 534 | 1.8\% | 30039 |  |
| Meeting Threshold |  |  |  |  |  |  | 100\% | 100\% |  |  |  |  |  | 100\% | 100\% |

Table 3-9: Simulated versus Measured Average Speeds (mph)

| Segment | AM Peak |  |  |  | PM Peak |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Field | Sim. | Diff. | Meets <br> Target <br> (Y/N) | Field | Sim. | Diff. | Meets <br> Target <br> (Y/N) |
| I-75 SB Off to SR 326 | 45.6 | 44.3 | 1.3 | Y | 51.3 | 43.9 | 7.4 | Y |
| I-75 NB Off to SR 326 | 36.4 | 38.8 | 2.4 | Y | 35.2 | 39.1 | 3.9 | Y |
| I-75 SB Off to US 27 | 37.5 | 37.2 | 0.3 | Y | 38.4 | 37.2 | 1.2 | Y |
| I-75 NB Off to US 27 | 45.2 | 37.9 | 7.3 | Y | 50.6 | 38.3 | 12.3 | N |
| W of I-75 on SR 326 EB | 36.4 | 42.3 | 5.9 | Y | 35.2 | 42.3 | 7.1 | Y |
| W of I-75 on SR 326 WB | 24.4 | 34.4 | 10.0 | Y | 29.6 | 35.4 | 5.8 | Y |
| S of SR 326 NB | 20.5 | 21.2 | 0.7 | Y | 17.7 | 20.9 | 3.2 | Y |
| S of SR 326 SB | 21.0 | 28.0 | 7.0 | Y | 22.5 | 28.2 | 5.7 | Y |
| E of I-75 on SR 326 EB | 24.4 | 44.3 | 19.9 | N | 42.4 | 44.3 | 1.9 | Y |
| E of I-75 on SR 326 WB | 41.8 | 44.2 | 2.4 | Y | 42.4 | 44.1 | 1.7 | Y |
| W of I-75 on US 27 EB | 26.7 | 41.5 | 14.8 | N | 30.0 | 42.2 | 12.2 | N |
| W of I-75 on US 27 WB | 45.6 | 40.4 | 5.2 | Y | 38.8 | 37.7 | 1.1 | Y |
| E of I-75 on US 27 EB | 34.7 | 41.1 | 6.4 | Y | 33.5 | 41.7 | 8.2 | Y |
| E of I-75 on US 27 WB | 39.3 | 42.1 | 2.8 | Y | 33.3 | 39.1 | 5.8 | Y |
| E of NW $35^{\text {th }} \mathrm{Av}$ on US 27 EB | 45.8 | 43.2 | 2.6 | Y | 45.5 | 43.5 | 2.0 | Y |
| E of NW $35^{\text {th }} \mathrm{Av}$ on US 27 WB | 36.1 | 44.0 | 7.9 | Y | 36.2 | 42.7 | 6.5 | Y |
| S of NW $49^{\text {th }}$ ST on NW $44^{\text {th }}$ Av NB | 43.6 | 45.2 | 1.6 | Y | 36.4 | 45.1 | 8.7 | Y |
| S of NW $49^{\text {th }}$ ST on NW $44^{\text {th }}$ Av SB | 50.4 | 45.0 | 5.4 | $Y$ | 49.2 | 45.0 | 4.2 | Y |
| N of NW 49 ${ }^{\text {th }}$ ST on NW 44 ${ }^{\text {th }}$ Av NB | 45.8 | 45.1 | 0.7 | Y | 39.3 | 45.0 | 5.7 | Y |
| N of NW $49^{\text {th }}$ ST on NW $44^{\text {th }}$ Av SB | 33.5 | 45.1 | 11.6 | N | 36.2 | 45.1 | 8.9 | Y |
| \%MEETING THRESHOLD |  |  |  | 85.0\% |  |  |  | 85.0\% |

Table 3-10: Simulated versus Observed Queue Lengths (feet)

| Intersection | Peak Hour | Movement or Approach | Field | Simulated | \% Difference | Difference in passenger car equivalent ${ }^{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { SR } 326 \text { at I-75 NB } \\ \text { Ramp } \end{gathered}$ | AM | WB | 317 | 251 | 20\% | 2.64 |
|  |  | NB | 97 | 124 | 21\% | 1.08 |
|  | PM | WB | 327 | 243 | 25\% | 3.36 |
|  |  | NB | 102 | 181 | 43\% | 3.16 |
| SR 326 at NW 44 Ave | AM | EB | 156 | 148 | 5\% | 0.32 |
|  |  | SBL | 84 | 106 | 20\% | 0.88 |
|  | PM | EB | 176 | 146 | 17\% | 1.20 |
|  |  | SBL | 159 | 164 | 3\% | 0.20 |
| US 27 at I-75 NB Ramp | AM | WBL | 106 | 172 | 38\% | 2.64 |
|  |  | WBT | 169 | 143 | 15\% | 1.04 |
|  |  | NBL | 99 | 121 | 18\% | 0.88 |
|  |  | NBR | 98 | 142 | 30\% | 1.76 |
|  | PM | WBL | 143 | 234 | 38\% | 3.64 |
|  |  | WBT | 365 | 286 | 21\% | 3.16 |
|  |  | NBL | 137 | 149 | 8\% | 0.48 |
|  |  | NBR | 114 | 117 | 2\% | 0.12 |
| US 27 at I-75 SB Ramp | AM | SBL | 95 | 149 | 36\% | 2.16 |
|  |  | EBT | 381 | 302 | 20\% | 3.16 |
|  |  | EBR | 129 | 150 | 14\% | 0.84 |
|  | PM | SBL | 106 | 117 | 9\% | 0.44 |
|  |  | EBT | 223 | 242 | 7\% | 0.76 |
|  |  | EBR | 81 | 167 | 51\% | 3.44 |
| US 27 at NW 35 Ave Rd | AM | SBL | 42 | 48 | 12\% | 0.24 |
|  |  | SBR | 96 | 176 | 45\% | 3.20 |
|  |  | EBL | 99 | 126 | 21\% | 1.08 |
|  |  | EBT | 324 | 295 | 8\% | 1.16 |
|  | PM | SBL | 44 | 53 | 16\% | 0.36 |
|  |  | SBR | 138 | 170 | 18\% | 1.28 |
|  |  | EBL | 171 | 145 | 15\% | 1.04 |
|  |  | EBT | 158 | 197 | 19\% | 1.56 |
| US 27 at NW 44 Ave | AM | WBT | 131 | 164 | 20\% | 1.32 |
|  | PM | WBT | 199 | 298 | 33\% | 3.96 |

[^3]
## Validation Results

Table 3-11 summarizes travel times for the arterial segments. Table 3-12 summarizes the Vissim overall intersection delay (seconds/vehicle) and queue (feet) for the existing condition peak hours. This analysis is performed for network/system performance; the estimated LOS based on HCM thresholds along with Vissim delays are provided for informational purposes only. It should be noted that the sink/source intersection of US 27 at NW 38 Avenue was included in the Table 3-11 summary since it was modeled in Vissim.

In comparison to the intersection Synchro results, a difference in delay is observed for the intersections of US 27 at NW $35^{\text {th }}$ Avenue and SR 326 at I- 75 northbound off-ramp. In general, Synchro reported higer delays for the eastbound and westbound approaches at the two subject intersections resulting in a higher overall intersection LOS when compared to Vissim results. Difference in LOS results is likely due to the difference in HCM 2010 right-turn-on-red (RTOR) volume estimation calculations and the Vissim simulated RTOR which directly impacts green time distribution and ultimately approach delay. Results from the Vissim analysis were determined to be acceptable based on the observed queue lengths.
$\mathrm{I}-75$ volume (veh/hour), speed (mph) and density (veh/n/mi) 15 -minute results are summarized in Figures 3-9 thru 3-12. In general, volume and speed results show that optimal speeds are maintained throughout the analysis period and demand volumes are processed. During the AM and PM peak hours (time periods 5 through 8), I-75 northbound densities range from 6.8 $\mathrm{veh} / \mathrm{mi} / \mathrm{ln}$ to $12.2 \mathrm{veh} / \mathrm{mi} / \mathrm{ln}$ and from $7.0 \mathrm{veh} / \mathrm{mi} / \mathrm{ln}$ to $12.3 \mathrm{veh} / \mathrm{mi} / \mathrm{ln}$, respectively. During the AM and PM peak hours, I-75 southbbound densities range from $4.3 \mathrm{veh} / \mathrm{mi} / \mathrm{ln}$ to $9.7 \mathrm{veh} / \mathrm{mi} / \mathrm{ln}$ and from $6.2 \mathrm{veh} / \mathrm{mi} / \mathrm{ln}$ to $11.7 \mathrm{veh} / \mathrm{mi} / \mathrm{ln}$, respectively. Similar to the HCS results, densities are generally increase toward the south closer to the US 27 interchange. In comparison to the HCS results, Vissim is observed to generate slightly lower densities. Density calculation methodologies are significantly different between the two evaluation methods; however, relative density result trends along I-75 are similar.

The network performance summary is provided in Table 3-13. Detailed three hour analysis period results in 15 -minute intervals are provided in Appendix $\mathbf{E}$.

Table 3-11: Travel Time Summary (sec)

| Peak | Segment |  | Time Period |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Period |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | PK HR |
| AM | US 27 | US 27 EB from W of NW 44 Ave to I-75 | 121 | 124 | 124 | 125 | 129 | 131 | 129 | 127 | 127 | 124 | 126 | 126 | 129 |
|  |  | US 27 EB from I-75 to NW 35 Ave Rd | 17 | 18 | 17 | 19 | 19 | 20 | 19 | 18 | 18 | 19 | 19 | 18 | 19 |
|  |  | US 27 EB from NW 35 Ave Rd to E of NW 35 Ave Rd | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 |
|  |  | US 27 WB from E of NW 35 Ave Rd to NW 35 Ave Rd | 46 | 47 | 46 | 47 | 49 | 49 | 49 | 48 | 48 | 49 | 49 | 47 | 49 |
|  |  | US 27 WB from NW 35 Ave Rd to I-75 | 15 | 17 | 17 | 17 | 19 | 18 | 18 | 18 | 17 | 17 | 18 | 17 | 18 |
|  |  | US 27 WB from I-75 to W of NW 44 Ave | 85 | 86 | 87 | 85 | 88 | 88 | 87 | 87 | 87 | 86 | 87 | 86 | 88 |
|  | SR 326 | SR 326 EB from W of I-75 to I-75 | 35 | 37 | 38 | 38 | 41 | 41 | 41 | 39 | 39 | 39 | 39 | 38 | 41 |
|  |  | SR 326 EB from I-75 to E of I-75 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 |
|  |  | SR 326 WB from E of I-75 to I-75 | 33 | 33 | 33 | 34 | 34 | 34 | 34 | 34 | 33 | 33 | 33 | 33 | 34 |
|  |  | SR 326 WB from I-75 to W of I-75 | 6 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
|  | NW 44 Ave | NW 44 Ave NB from S of NW 49 St to NW 49 St | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 |
|  |  | NW 44 Ave NB from NW 49 St to N of NW 49 St | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
|  |  | NW 44 Ave SB from N of NW 49 St to NW 49 St | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  |  | NW 44 Ave SB from NW 49 St to S of NW 49 St | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 |
| PM | US 27 | US 27 EB from W of NW 44 Ave to I-75 | 122 | 123 | 124 | 123 | 123 | 124 | 125 | 124 | 123 | 121 | 121 | 121 | 124 |
|  |  | US 27 EB from I-75 to NW 35 Ave Rd | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 19 | 19 | 18 | 18 | 17 | 18 |
|  |  | US 27 EB from NW 35 Ave Rd to E of NW 35 Ave Rd | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 | 23 |
|  |  | US 27 WB from E of NW 35 Ave Rd to NW 35 Ave Rd | 51 | 50 | 51 | 51 | 52 | 52 | 51 | 53 | 53 | 51 | 50 | 49 | 52 |
|  |  | US 27 WB from NW 35 Ave Rd to I-75 | 20 | 21 | 22 | 21 | 22 | 24 | 23 | 24 | 25 | 25 | 20 | 19 | 23 |
|  |  | US 27 WB from I-75 to W of NW 44 Ave | 88 | 88 | 90 | 90 | 90 | 89 | 91 | 89 | 91 | 89 | 88 | 88 | 90 |
|  | SR 326 | SR 326 EB from W of I-75 to I-75 | 42 | 43 | 43 | 43 | 44 | 43 | 43 | 44 | 44 | 42 | 43 | 41 | 44 |
|  |  | SR 326 EB from I-75 to E of I-75 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 | 21 |
|  |  | SR 326 WB from E of I-75 to I-75 | 34 | 33 | 34 | 34 | 33 | 34 | 34 | 34 | 33 | 33 | 33 | 33 | 34 |
|  |  | SR 326 WB from I-75 to W of I-75 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
|  | NW 44 Ave | NW 44 Ave NB from S of NW 49 St to NW 49 St | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 | 17 |
|  |  | NW 44 Ave NB from NW 49 St to N of NW 49 St | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
|  |  | NW 44 Ave SB from N of NW 49 St to NW 49 St | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
|  |  | NW 44 Ave SB from NW 49 St to S of NW 49 St | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 | 18 |

Table 3-12: Intersection Delay \& Queue Summary

| Intersection | Control | MVMT | $\mathrm{AM}^{1}$ |  |  |  |  | PM ${ }^{1}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Vol | Delay | LOS | Avg Q | Max Q | Vol | Delay | LOS | Avg Q | Max Q |
| NW 49 St at NW 44 Ave | U | NBL | 1 | 0.5 | A | 0 | 0 | 8 | 0.5 | A | 0 | 0 |
|  |  | NBT | 142 | 0.0 | A | 0 | 0 | 277 | 0.0 | A | 0 | 0 |
|  |  | SBT | 309 | 0.0 | A | 0 | 0 | 237 | 0.0 | A | 0 | 0 |
|  |  | SBR | 0 | 0.0 | A | 0 | 0 | 2 | 0.7 | A | 0 | 0 |
|  |  | EBL | 4 | 5.6 | A | 0 | 35 | 1 | 5.5 | A | 0 | 19 |
|  |  | EBR | 2 | 4.8 | A | 0 | 0 | 8 | 4.7 | A | 0 | 0 |
|  |  | Overall |  | 0.1 | A |  |  |  | 0.1 | A |  |  |
| SR 326 at NW 44 Ave | S | NBL | 15 | 20.5 | C | 3 | 70 | 32 | 21.9 | C | 6 | 96 |
|  |  | NBR | 63 | 20.9 | C | 8 | 77 | 78 | 22.7 | C | 11 | 91 |
|  |  | SBL | 78 | 18.3 | B | 9 | 106 | 165 | 20.0 | B | 21 | 164 |
|  |  | SBT | 7 | 19.7 | B | 9 | 106 | 6 | 20.0 | B | 21 | 164 |
|  |  | SBR | 42 | 1.0 | A | 0 | 9 | 117 | 1.3 | A | 0 | 28 |
|  |  | EBT | 290 | 11.6 | B | 14 | 148 | 258 | 15.3 | B | 17 | 146 |
|  |  | EBR | 19 | 6.4 | A | 1 | 51 | 18 | 7.6 | A | 1 | 45 |
|  |  | WBL | 57 | 13.9 | B | 3 | 72 | 41 | 17.7 | B | 3 | 56 |
|  |  | WBT | 244 | 11.5 | B | 12 | 133 | 287 | 16.2 | B | 20 | 150 |
|  |  | Overall |  | 12.6 | B |  |  |  | 15.5 | B |  |  |
| SR 326 at I-75 NB | S | NBL | 62 | 3.0 | A | 2 | 124 | 513 | 3.9 | A | 5 | 181 |
|  |  | NBR | 472 | 19.6 | B | 7 | 92 | 82 | 18.5 | B | 9 | 94 |
|  |  | EBL | 85 | 6.3 | A | 2 | 66 | 37 | 6.7 | A | 1 | 39 |
|  |  | EBT | 331 | 4.3 | A | 4 | 80 | 421 | 5.6 | A | 6 | 99 |
|  |  | WBT | 672 | 8.0 | A | 20 | 251 | 726 | 7.4 | A | 21 | 243 |
|  |  | WBR | 163 | 3.7 | A | 0 | 54 | 124 | 3.6 | A | 0 | 23 |
|  |  | Overall |  | 5.9 | A |  |  |  | 6.3 | A |  |  |
| US 27 at l-75 SB | S | SBL | 118 | 40.1 | D | 28 | 149 | 93 | 37.9 | D | 21 | 117 |
|  |  | SBR | 36 | 1.2 | A | 0 | 0 | 63 | 1.3 | A | 0 | 0 |
|  |  | EBT | 986 | 15.2 | B | 45 | 302 | 780 | 14.1 | B | 33 | 242 |
|  |  | EBR | 285 | 7.4 | A | 5 | 150 | 259 | 8.5 | A | 7 | 167 |
|  |  | WBL | 256 | 11.1 | B | 15 | 212 | 314 | 10.3 | B | 19 | 254 |
|  |  | WBT | 718 | 5.1 | A | 9 | 156 | 1252 | 5.0 | A | 20 | 295 |
|  |  | Overall |  | 11.9 | B |  |  |  | 9.5 | A |  |  |
| US 27 at I-75 NB | S | NBL | 181 | 25.8 | C | 24 | 121 | 279 | 26.8 | C | 36 | 149 |
|  |  | NBR | 354 | 19.1 | B | 35 | 142 | 261 | 18.6 | B | 27 | 117 |
|  |  | EBL | 54 | 7.4 | A | 1 | 46 | 51 | 9.9 | A | 1 | 49 |
|  |  | EBT | 1052 | 7.6 | A | 26 | 309 | 826 | 7.9 | A | 19 | 257 |
|  |  | WBT | 535 | 9.5 | A | 14 | 143 | 973 | 13.6 | B | 34 | 286 |
|  |  | WBT>L | 256 | 10.9 | B | 12 | 172 | 313 | 14.6 | B | 20 | 234 |
|  |  | WBR | 110 | 4.2 | A | 0 | 27 | 126 | 5.9 | A | 0 | 21 |
|  |  | Overall |  | 11.0 | B |  |  |  | 13.4 | B |  |  |
| US 27 at NW 35 Ave Rd | S | NBL | 12 | 51.4 | D | 5 | 44 | 21 | 49.9 | D | 7 | 60 |
|  |  | NBT | 4 | 45.1 | D | 5 | 44 | 2 | 55.5 | E | 7 | 60 |
|  |  | NBR | 0 | 13.7 | B | 7 | 57 | 4 | 12.4 | B | 10 | 75 |
|  |  | SBL | 18 | 54.1 | D | 6 | 48 | 23 | 51.4 | D | 7 | 53 |
|  |  | SBT | 3 | 52.6 | D | 0 | 10 | 1 | 60.0 | E | 0 | 9 |
|  |  | SBR | 268 | 9.9 | A | 26 | 176 | 267 | 12.9 | B | 30 | 170 |
|  |  | EBL | 242 | 10.0 | A | 7 | 126 | 219 | 16.1 | B | 12 | 145 |
|  |  | EBT | 1127 | 6.4 | A | 19 | 295 | 845 | 5.3 | A | 11 | 197 |
|  |  | Ebr | 37 | 4.9 | A | 1 | 51 | 24 | 2.8 | A | 0 | 32 |
|  |  | WBL | 17 | 9.6 | A | 0 | 19 | 13 | 7.7 | A | 0 | 15 |
|  |  | WBT | 620 | 9.6 | A | 18 | 164 | 1131 | 11.6 | B | 41 | 335 |
|  |  | WBR | 25 | 2.5 | A | 0 | 0 | 21 | 2.9 | A | 0 | 13 |
|  |  | Overall |  | 8.7 | A |  |  |  | 10.6 | B |  |  |
| US 27 at NW 44 Ave | S | NBL | 4 | 34.2 | C | 1 | 17 | 4 | 35.5 | D | 1 | 11 |
|  |  | NBT | 0 | 39.8 | D | 0 | 5 | 0 | 0.0 | A | 0 | 0 |
|  |  | NBR | 14 | 3.3 | A | 0 | 16 | 11 | 2.3 | A | 0 | 10 |
|  |  | SBL | 341 | 21.5 | C | 30 | 139 | 273 | 24.1 | C | 28 | 129 |
|  |  | SBT | 1 | 24.6 | C | 30 | 139 | 0 | 0.0 | A | 28 | 129 |
|  |  | SBR | 65 | 6.0 | A | 38 | 154 | 66 | 7.4 | A | 36 | 143 |
|  |  | EBL | 43 | 11.2 | B | 2 | 55 | 51 | 12.7 | B | 3 | 54 |
|  |  | EBT | 781 | 11.7 | B | 26 | 220 | 647 | 9.1 | A | 16 | 157 |
|  |  | EBR | 0 | 13.5 | B | 0 | 0 | 0 | 6.8 | A | 0 | 0 |
|  |  | WBL | 10 | 10.7 | B | 0 | 21 | 6 | 11.2 | B | 0 | 13 |
|  |  | WBT | 489 | 12.2 | B | 18 | 164 | 930 | 13.0 | B | 36 | 298 |
|  |  | WBR | 166 | 5.4 | A | 7 | 140 | 252 | 6.1 | A | 10 | 151 |
|  |  | Overall |  | 12.9 | B |  |  |  | 12.2 | B |  |  |
| SR 326 at I-75 SB | U | NBR | 47 | 7.9 | A | 3 | 77 | 27 | 7.8 | A | 2 | 65 |
|  |  | EBT | 290 | 0.9 | A | 0 | 2 | 381 | 0.6 | A | 0 | 0 |
|  |  | EBR | 40 | 0.9 | A | 0 | 2 | 18 | 0.8 | A | 0 | 0 |
|  |  | WBL | 52 | 3.3 | A | 1 | 75 | 22 | 3.6 | A | 0 | 41 |
|  |  | WBT | 301 | 0.5 | A | 0 | 0 | 329 | 0.4 | A | 0 | 0 |
|  |  | WBR | 280 | 0.9 | A | 0 | 0 | 386 | 0.9 | A | 0 | 0 |
|  |  | WBU | 76 | 3.8 | A | 1 | 64 | 51 | 3.8 | A | 1 | 42 |
|  |  | Overall |  | 1.5 | A |  |  |  | 1.1 | A |  |  |
| US 27 at NW 38 Ave | U | NBL | 741 | 7.5 | A | 0 | 26 | 1295 | 10.8 | B | 1 | 48 |
|  |  | NBR | 21 | 10.7 | B | 2 | 66 | 18 | 8.7 | A | 1 | 61 |
|  |  | EBT | 1250 | 0.5 | A | 0 | 0 | 1025 | 0.3 | A | 0 | 0 |
|  |  | EBR | 4 | 0.9 | A | 0 | 0 | 14 | 0.8 | A | 0 | 0 |
|  |  | WBL | 13 | 5.8 | A | 0 | 25 | 20 | 4.2 | A | 0 | 27 |
|  |  | WBT | 2 | 0.2 | A | 0 | 0 | 5 | 0.3 | A | 0 | 0 |
|  |  | Overall |  | 0.5 | A |  |  |  | 0.5 | A |  |  |

[^4]NORTHBOUND I-75 - TIME PLOT

| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 2066 | 2066 | 1650 | 1790 | 1798 | 1812 | 1335 | 1550 | 1556 |
|  | Demand | 2036 | 2036 | 1588 | 1726 | 1726 | 1726 | 1264 | 1479 | 1479 |
|  | Diff. | 30 | 30 | 62 | 64 | 72 | 86 | 71 | 71 | 77 |
| 11 | Processed | 2281 | 2271 | 1783 | 1941 | 1928 | 1921 | 1405 | 1638 | 1634 |
|  | Demand | 2266 | 2266 | 1767 | 1921 | 1921 | 1921 | 1406 | 1646 | 1646 |
|  | Diff. | 15 | 5 | 16 | 20 | 7 | 0 | -1 | -8 | -12 |
| 10 | Processed | 2219 | 2211 | 1755 | 1918 | 1922 | 1927 | 1384 | 1603 | 1610 |
|  | Demand | 2201 | 2201 | 1716 | 1865 | 1865 | 1865 | 1366 | 1599 | 1599 |
|  | Diff. | 18 | 10 | 39 | 53 | 57 | 62 | 18 | 4 | 11 |
| 9 | Processed | 2211 | 2204 | 1736 | 1888 | 1883 | 1869 | 1363 | 1566 | 1565 |
|  | Demand | 2204 | 2204 | 1718 | 1868 | 1868 | 1868 | 1368 | 1601 | 1601 |
|  | Diff. | 7 | 0 | 18 | 20 | 15 | 1 | -5 | -35 | -36 |
| 8 | Processed | 2145 | 2141 | 1682 | 1852 | 1874 | 1901 | 1406 | 1637 | 1649 |
|  | Demand | 2153 | 2153 | 1679 | 1825 | 1825 | 1825 | 1336 | 1564 | 1564 |
|  | Diff. | -8 | -12 | 3 | 27 | 49 | 76 | 70 | 73 | 85 |
| 7 | Processed | 2487 | 2478 | 1929 | 2091 | 2106 | 2117 | 1558 | 1819 | 1813 |
|  | Demand | 2552 | 2552 | 1990 | 2163 | 2163 | 2163 | 1584 | 1854 | 1854 |
|  | Diff. | -65 | -74 | -61 | -72 | -57 | -46 | -26 | -35 | -41 |
| 6 | Processed | 2479 | 2466 | 1931 | 2108 | 2099 | 2087 | 1532 | 1781 | 1790 |
|  | Demand | 2567 | 2567 | 2001 | 2175 | 2175 | 2175 | 1593 | 1865 | 1865 |
|  | Diff. | -88 | -101 | -70 | -67 | -76 | -88 | -61 | -84 | -75 |
| 5 | Processed | 2415 | 2407 | 1897 | 2065 | 2029 | 2007 | 1471 | 1711 | 1705 |
|  | Demand | 2512 | 2512 | 1958 | 2129 | 2129 | 2129 | 1559 | 1825 | 1825 |
|  | Diff. | -97 | -105 | -61 | -64 | -100 | -122 | -88 | -114 | -120 |
| 4 | Processed | 2123 | 2105 | 1646 | 1781 | 1768 | 1752 | 1267 | 1502 | 1504 |
|  | Demand | 2167 | 2167 | 1690 | 1837 | 1837 | 1837 | 1345 | 1575 | 1575 |
|  | Diff. | -44 | -62 | -44 | -56 | -69 | -85 | -78 | -73 | -71 |
| 3 | Processed | 2017 | 2007 | 1568 | 1720 | 1701 | 1687 | 1201 | 1401 | 1397 |
|  | Demand | 2070 | 2070 | 1614 | 1755 | 1755 | 1755 | 1285 | 1504 | 1504 |
|  | Diff. | -53 | -63 | -46 | -35 | -54 | -68 | -84 | -103 | -107 |
| 2 | Processed | 1848 | 1832 | 1434 | 1546 | 1518 | 1503 | 1099 | 1285 | 1279 |
|  | Demand | 1902 | 1902 | 1483 | 1612 | 1612 | 1612 | 1180 | 1382 | 1382 |
|  | Diff. | -54 | -70 | -49 | -66 | -94 | -109 | -81 | -97 | -103 |
| 1 | Processed | 1464 | 1450 | 1142 | 1231 | 1215 | 1182 | 865 | 1007 | 1009 |
|  | Demand | 1498 | 1498 | 1168 | 1269 | 1269 | 1269 | 929 | 1088 | 1088 |
|  | Diff. | -34 | -48 | -26 | -38 | -54 | -87 | -64 | -81 | -79 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | I-75 | US 27 Interchange |  |  | I-75 | SR 326 Interchange |  |  | I-75 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > |

SOUTHBOUND I-75-TIME PLOT

| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 966 | 951 | 856 | 1103 | 1102 | 1215 | 1215 | 1232 | 1102 | 1582 | 1589 |
|  | Demand | 970 | 970 | 864 | 1102 | 1102 | 1221 | 1221 | 1221 | 1086 | 1540 | 1540 |
|  | Diff. | -4 | -19 | -8 | 1 | 0 | -6 | -6 | 11 | 16 | 42 | 49 |
| 11 | Processed | 1068 | 1052 | 957 | 1204 | 1201 | 1323 | 1317 | 1317 | 1177 | 1710 | 1702 |
|  | Demand | 1079 | 1079 | 962 | 1227 | 1227 | 1359 | 1359 | 1359 | 1209 | 1714 | 1714 |
|  | Diff. | -11 | -27 | -5 | -23 | -26 | -36 | -42 | -42 | -32 | -4 | -12 |
| 10 | Processed | 1036 | 1021 | 917 | 1146 | 1146 | 1277 | 1277 | 1274 | 1145 | 1624 | 1627 |
|  | Demand | 1048 | 1048 | 934 | 1191 | 1191 | 1320 | 1320 | 1320 | 1174 | 1664 | 1664 |
|  | Diff. | -12 | -27 | -17 | -45 | -45 | -43 | -43 | -46 | -29 | -40 | -37 |
| 9 | Processed | 1029 | 1018 | 920 | 1155 | 1156 | 1283 | 1278 | 1275 | 1141 | 1635 | 1639 |
|  | Demand | 1050 | 1050 | 935 | 1193 | 1193 | 1322 | 1322 | 1322 | 1176 | 1667 | 1667 |
|  | Diff. | -21 | -32 | -15 | -38 | -37 | -39 | -44 | -47 | -35 | -32 | -28 |
| 8 | Processed | 1017 | 1001 | 901 | 1171 | 1172 | 1299 | 1321 | 1338 | 1203 | 1702 | 1716 |
|  | Demand | 1026 | 1026 | 914 | 1166 | 1166 | 1291 | 1291 | 1291 | 1149 | 1629 | 1629 |
|  | Diff. | -9 | -25 | -13 | 5 | 6 | 8 | 30 | 47 | 54 | 73 | 87 |
| 7 | Processed | 1210 | 1192 | 1085 | 1376 | 1378 | 1524 | 1519 | 1519 | 1368 | 1938 | 1938 |
|  | Demand | 1215 | 1215 | 1083 | 1381 | 1381 | 1530 | 1530 | 1530 | 1361 | 1930 | 1930 |
|  | Diff. | -5 | -23 | 2 | -5 | -3 | -6 | -11 | -11 | 7 | 8 | 8 |
| 6 | Processed | 1215 | 1199 | 1079 | 1373 | 1373 | 1520 | 1510 | 1510 | 1347 | 1910 | 1904 |
|  | Demand | 1223 | 1223 | 1089 | 1389 | 1389 | 1539 | 1539 | 1539 | 1369 | 1941 | 1941 |
|  | Diff. | -8 | -24 | -10 | -16 | -16 | -19 | -29 | -29 | -22 | -31 | -37 |
| 5 | Processed | 1199 | 1180 | 1066 | 1325 | 1320 | 1478 | 1458 | 1434 | 1286 | 1805 | 1800 |
|  | Demand | 1196 | 1196 | 1066 | 1360 | 1360 | 1507 | 1507 | 1507 | 1340 | 1900 | 1900 |
|  | Diff. | 3 | -16 | 0 | -35 | -40 | -29 | -49 | -73 | -54 | -95 | -100 |
| 4 | Processed | 1037 | 1017 | 919 | 1174 | 1174 | 1287 | 1274 | 1264 | 1122 | 1574 | 1569 |
|  | Demand | 1032 | 1032 | 920 | 1173 | 1173 | 1300 | 1300 | 1300 | 1156 | 1639 | 1639 |
|  | Diff. | 5 | -15 | -1 | 1 | 1 | -13 | -26 | -36 | -34 | -65 | -70 |
| 3 | Processed | 979 | 966 | 880 | 1083 | 1078 | 1198 | 1192 | 1183 | 1052 | 1489 | 1495 |
|  | Demand | 986 | 986 | 879 | 1121 | 1121 | 1242 | 1242 | 1242 | 1105 | 1566 | 1566 |
|  | Diff. | -7 | -20 | 1 | -38 | -43 | -44 | -50 | -59 | -53 | -77 | -71 |
| 2 | Processed | 895 | 874 | 780 | 982 | 981 | 1073 | 1042 | 1018 | 899 | 1286 | 1281 |
|  | Demand | 906 | 906 | 807 | 1029 | 1029 | 1141 | 1141 | 1141 | 1015 | 1438 | 1438 |
|  | Diff. | -11 | -32 | -27 | -47 | -48 | -68 | -99 | -123 | -116 | -152 | -157 |
| 1 | Processed | 690 | 682 | 617 | 789 | 788 | 870 | 859 | 851 | 755 | 1068 | 1065 |
|  | Demand | 713 | 713 | 636 | 811 | 811 | 898 | 898 | 898 | 799 | 1133 | 1133 |
|  | Diff. | -23 | -31 | -19 | -22 | -23 | -28 | -39 | -47 | -44 | -65 | -68 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | 1-75 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > |

Volume (vph): XXXX Difference greater than 400vph (Based on FDOT Traffic Analysis Handbook Calibration Volume> 2,700 vph)

NORTHBOUND I-75 - TIME PLOT

| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 1952 | 1946 | 1534 | 1675 | 1685 | 1701 | 1215 | 1360 | 1366 |
|  | Demand | 1919 | 1919 | 1499 | 1638 | 1638 | 1638 | 1167 | 1298 | 1298 |
|  | Diff. | 33 | 27 | 35 | 37 | 47 | 63 | 48 | 62 | 68 |
| 11 | Processed | 2112 | 2104 | 1678 | 1831 | 1833 | 1842 | 1298 | 1448 | 1455 |
|  | Demand | 2087 | 2087 | 1630 | 1781 | 1781 | 1781 | 1269 | 1412 | 1412 |
|  | Diff. | 25 | 17 | 48 | 50 | 52 | 61 | 29 | 36 | 43 |
| 10 | Processed | 2224 | 2223 | 1757 | 1928 | 1953 | 1974 | 1416 | 1567 | 1563 |
|  | Demand | 2200 | 2200 | 1718 | 1877 | 1877 | 1877 | 1337 | 1488 | 1488 |
|  | Diff. | 24 | 23 | 39 | 51 | 76 | 97 | 79 | 79 | 75 |
| 9 | Processed | 2498 | 2489 | 1959 | 2148 | 2159 | 2175 | 1524 | 1680 | 1691 |
|  | Demand | 2513 | 2513 | 1963 | 2144 | 2144 | 2144 | 1527 | 1700 | 1700 |
|  | Diff. | -15 | -24 | -4 | 4 | 15 | 31 | -3 | -20 | -9 |
| 8 | Processed | 2526 | 2514 | 2003 | 2194 | 2181 | 2174 | 1549 | 1697 | 1698 |
|  | Demand | 2553 | 2553 | 1993 | 2178 | 2178 | 2178 | 1551 | 1727 | 1727 |
|  | Diff. | -27 | -39 | 10 | 16 | 3 | -4 | -2 | -30 | -29 |
| 7 | Processed | 2524 | 2508 | 1961 | 2135 | 2122 | 2096 | 1499 | 1671 | 1668 |
|  | Demand | 2593 | 2593 | 2025 | 2213 | 2213 | 2213 | 1576 | 1754 | 1754 |
|  | Diff. | -69 | -85 | -64 | -78 | -91 | -117 | -77 | -83 | -86 |
| 6 | Processed | 2347 | 2341 | 1833 | 2012 | 2020 | 2031 | 1457 | 1610 | 1610 |
|  | Demand | 2429 | 2429 | 1896 | 2072 | 2072 | 2072 | 1476 | 1643 | 1643 |
|  | Diff. | -82 | -88 | -63 | -60 | -52 | -41 | -19 | -33 | -33 |
| 5 | Processed | 2407 | 2392 | 1880 | 2055 | 2052 | 2054 | 1472 | 1625 | 1627 |
|  | Demand | 2501 | 2501 | 1953 | 2134 | 2134 | 2134 | 1520 | 1692 | 1692 |
|  | Diff. | -94 | -109 | -73 | -79 | -82 | -80 | -48 | -67 | -65 |
| 4 | Processed | 2384 | 2375 | 1880 | 2050 | 2047 | 2053 | 1459 | 1626 | 1628 |
|  | Demand | 2454 | 2454 | 1916 | 2093 | 2093 | 2093 | 1491 | 1660 | 1660 |
|  | Diff. | -70 | -79 | -36 | -43 | -46 | -40 | -32 | -34 | -32 |
| 3 | Processed | 2399 | 2391 | 1875 | 2043 | 2019 | 1987 | 1395 | 1552 | 1552 |
|  | Demand | 2478 | 2478 | 1935 | 2114 | 2114 | 2114 | 1506 | 1676 | 1676 |
|  | Diff. | -79 | -87 | -60 | -71 | -95 | -127 | -111 | -124 | -124 |
| 2 | Processed | 2153 | 2143 | 1678 | 1848 | 1850 | 1865 | 1313 | 1454 | 1461 |
|  | Demand | 2210 | 2210 | 1726 | 1885 | 1885 | 1885 | 1343 | 1495 | 1495 |
|  | Diff. | -57 | -67 | -48 | -37 | -35 | -20 | -30 | -41 | -34 |
| 1 | Processed | 2212 | 2206 | 1744 | 1919 | 1917 | 1907 | 1352 | 1503 | 1498 |
|  | Demand | 2290 | 2290 | 1788 | 1953 | 1953 | 1953 | 1392 | 1549 | 1549 |
|  | Diff. | -78 | -84 | -44 | -34 | -36 | -46 | -40 | -46 | -51 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | I-75 | US 27 Interchange |  |  | I-75 | SR 326 Interchange |  |  | 1-75 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > |


| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 1228 | 1200 | 1008 | 1295 | 1297 | 1409 | 1420 | 1437 | 1314 | 1764 | 1775 |
|  | Demand | 1234 | 1234 | 1014 | 1311 | 1311 | 1209 | 1414 | 1414 | 1291 | 1735 | 1735 |
|  | Diff. | -6 | -34 | -6 | -16 | -14 | 200 | 6 | 23 | 23 | 29 | 40 |
| 11 | Processed | 1334 | 1306 | 1086 | 1391 | 1392 | 1506 | 1516 | 1519 | 1413 | 1921 | 1915 |
|  | Demand | 1342 | 1342 | 1103 | 1425 | 1425 | 1314 | 1538 | 1538 | 1404 | 1887 | 1887 |
|  | Diff. | -8 | -36 | -17 | -34 | -33 | 192 | -22 | -19 | 9 | 34 | 28 |
| 10 | Processed | 1407 | 1376 | 1155 | 1484 | 1485 | 1610 | 1627 | 1653 | 1528 | 2065 | 2078 |
|  | Demand | 1414 | 1414 | 1162 | 1502 | 1502 | 1385 | 1621 | 1621 | 1479 | 1988 | 1988 |
|  | Diff. | -7 | -38 | -7 | -18 | -17 | 225 | 6 | 32 | 49 | 77 | 90 |
| 9 | Processed | 1601 | 1568 | 1321 | 1689 | 1688 | 1827 | 1825 | 1832 | 1675 | 2253 | 2253 |
|  | Demand | 1615 | 1615 | 1328 | 1716 | 1716 | 1582 | 1852 | 1852 | 1690 | 2272 | 2272 |
|  | Diff. | -14 | -47 | -7 | -27 | -28 | 245 | -27 | -20 | -15 | -19 | -19 |
| 8 | Processed | 1642 | 1610 | 1353 | 1734 | 1733 | 1874 | 1875 | 1879 | 1724 | 2328 | 2338 |
|  | Demand | 1641 | 1641 | 1349 | 1743 | 1743 | 1607 | 1881 | 1881 | 1717 | 2307 | 2307 |
|  | Diff. | 1 | -31 | 4 | -9 | -10 | 267 | -6 | -2 | 7 | 21 | 31 |
| 7 | Processed | 1668 | 1626 | 1359 | 1760 | 1760 | 1892 | 1862 | 1843 | 1691 | 2261 | 2262 |
|  | Demand | 1667 | 1667 | 1370 | 1771 | 1771 | 1633 | 1911 | 1911 | 1744 | 2344 | 2344 |
|  | Diff. | 1 | -41 | -11 | -11 | -11 | 259 | -49 | -68 | -53 | -83 | -82 |
| 6 | Processed | 1562 | 1519 | 1283 | 1660 | 1655 | 1788 | 1808 | 1814 | 1666 | 2207 | 2209 |
|  | Demand | 1561 | 1561 | 1283 | 1658 | 1658 | 1529 | 1789 | 1789 | 1633 | 2195 | 2195 |
|  | Diff. | 1 | -42 | 0 | 2 | -3 | 259 | 19 | 25 | 33 | 12 | 14 |
| 5 | Processed | 1598 | 1570 | 1323 | 1697 | 1702 | 1842 | 1817 | 1809 | 1666 | 2234 | 2231 |
|  | Demand | 1608 | 1608 | 1322 | 1708 | 1708 | 1575 | 1843 | 1843 | 1682 | 2261 | 2261 |
|  | Diff. | -10 | -38 | 1 | -11 | -6 | 267 | -26 | -34 | -16 | -27 | -30 |
| 4 | Processed | 1572 | 1536 | 1292 | 1648 | 1645 | 1778 | 1778 | 1781 | 1641 | 2192 | 2197 |
|  | Demand | 1577 | 1577 | 1297 | 1675 | 1675 | 1545 | 1808 | 1808 | 1650 | 2218 | 2218 |
|  | Diff. | -5 | -41 | -5 | -27 | -30 | 233 | -30 | -27 | -9 | -26 | -21 |
| 3 | Processed | 1585 | 1549 | 1289 | 1659 | 1657 | 1791 | 1767 | 1741 | 1585 | 2114 | 2110 |
|  | Demand | 1593 | 1593 | 1310 | 1692 | 1692 | 1560 | 1826 | 1826 | 1667 | 2240 | 2240 |
|  | Diff. | -8 | -44 | -21 | -33 | -35 | 231 | -59 | -85 | -82 | -126 | -130 |
| 2 | Processed | 1422 | 1387 | 1167 | 1484 | 1480 | 1599 | 1611 | 1625 | 1484 | 1964 | 1970 |
|  | Demand | 1420 | 1420 | 1168 | 1509 | 1509 | 1391 | 1628 | 1628 | 1486 | 1998 | 1998 |
|  | Diff. | 2 | -33 | -1 | -25 | -29 | 208 | -17 | -3 | -2 | -34 | -28 |
| 1 | Processed | 1467 | 1435 | 1213 | 1567 | 1571 | 1689 | 1674 | 1657 | 1516 | 2033 | 2033 |
|  | Demand | 1472 | 1472 | 1210 | 1563 | 1563 | 1442 | 1687 | 1687 | 1540 | 2070 | 2070 |
|  | Diff. | -5 | -37 | 3 | 4 | 8 | 247 | -13 | -30 | -24 | -37 | -37 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | 1-75 |
| Direction | f Travel | > | > | > | > | > | > | > | > | > | $>$ | > |

Volume (vph): XXXX Difference greater than 400vph (Based on FDOT Traffic Analysis Handbook Calibration Volume> 2,700 vph)

1-75 NORTHBOUND

| Time <br> Period | Average Speed (mph)- AM Peak |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 69.4 | 68.3 | 69.2 | 68.8 | 68.8 | 67.7 | 69.2 | 68.4 | 68.9 |  |
| 11 | 69.3 | 68.1 | 69.2 | 68.6 | 68.8 | 67.5 | 69.1 | 68.3 | 68.8 |  |
| 10 | 69.2 | 68.1 | 69.1 | 68.6 | 68.7 | 67.4 | 69.1 | 68.4 | 68.9 |  |
| 9 | 69.3 | 68.2 | 69.1 | 68.7 | 68.8 | 67.6 | 69.2 | 68.3 | 68.9 |  |
| 8 | 69.3 | 68.3 | 69.2 | 68.7 | 68.8 | 67.8 | 69.0 | 68.0 | 68.7 |  |
| 7 | 69.2 | 67.9 | 68.9 | 68.5 | 68.5 | 67.3 | 68.9 | 68.0 | 68.7 |  |
| 6 | 69.1 | 68.0 | 69.0 | 68.5 | 68.6 | 67.5 | 69.1 | 68.3 | 68.9 |  |
| 5 | 69.1 | 68.1 | 69.0 | 68.5 | 68.7 | 67.3 | 69.0 | 68.3 | 68.9 |  |
| 4 | 69.3 | 68.4 | 69.1 | 68.6 | 68.8 | 67.7 | 69.1 | 68.3 | 68.9 |  |
| 3 | 69.3 | 68.2 | 69.1 | 68.7 | 68.9 | 67.9 | 69.2 | 68.5 | 68.9 |  |
| 2 | 69.4 | 68.5 | 69.3 | 68.9 | 69.0 | 68.1 | 69.5 | 68.8 | 69.2 |  |
| 1 | 69.7 | 68.9 | 69.6 | 69.3 | 69.3 | 68.5 | 69.6 | 68.9 | 69.3 |  |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |  |
| Int. | $1-75$ | US 27 | Interchange | I-75 | SR 326 Interchange | $1-75$ |  |  |  |  |
| Length (ft) | 2,702 | 1,479 | 3,134 | 1,500 | 16,309 | 1,500 | 3,094 | 1,495 | 3,759 |  |
| Direction of Travel | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ |  |  |


| Time <br> Period | Average Speed (mph)- PM Peak |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 69.5 | 68.4 | 69.4 | 68.8 | 68.9 | 67.6 | 69.3 | 68.6 | 69.0 |  |
| 11 | 69.3 | 68.4 | 69.2 | 68.7 | 68.8 | 67.5 | 69.0 | 68.5 | 68.9 |  |
| 10 | 69.2 | 68.1 | 69.1 | 68.6 | 68.7 | 67.4 | 69.1 | 68.5 | 68.9 |  |
| 9 | 69.1 | 67.8 | 68.9 | 68.4 | 68.5 | 67.1 | 69.0 | 68.5 | 68.8 |  |
| 8 | 69.1 | 67.7 | 68.9 | 68.3 | 68.6 | 67.2 | 69.0 | 68.5 | 68.8 |  |
| 7 | 69.1 | 67.8 | 69.0 | 68.4 | 68.6 | 67.5 | 69.1 | 68.5 | 68.9 |  |
| 6 | 69.2 | 68.1 | 69.1 | 68.2 | 68.6 | 67.2 | 69.0 | 68.6 | 68.9 |  |
| 5 | 69.1 | 67.9 | 69.0 | 68.5 | 68.6 | 67.5 | 69.1 | 68.5 | 68.9 |  |
| 4 | 69.1 | 68.0 | 68.9 | 68.5 | 68.6 | 67.3 | 69.1 | 68.6 | 68.9 |  |
| 3 | 69.1 | 68.2 | 69.0 | 68.5 | 68.7 | 67.2 | 69.1 | 68.7 | 69.0 |  |
| 2 | 69.2 | 68.2 | 69.1 | 68.7 | 68.8 | 67.7 | 69.1 | 68.6 | 69.0 |  |
| 1 | 69.3 | 68.3 | 69.1 | 68.6 | 68.7 | 67.5 | 69.0 | 68.6 | 68.9 |  |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |  |
| Int. | I-75 | US 27 Interchange | I-75 | SR 326 Interchange | $1-75$ |  |  |  |  |  |
| Length (ft) | 2,702 | 1,479 | 3,134 | 1,500 | 16,309 | 1,500 | 3,094 | 1,495 | 3,759 |  |
| Direction of Travel | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ |  |  |

## I-75 SOUTHBOUND

| Time | Average Speed (mph)- AM Peak |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 69.9 | 69.7 | 69.8 | 68.0 | 68.9 | 68.4 | 69.2 | 68.9 | 69.2 | 67.4 | 68.7 |
| 11 | 69.8 | 69.6 | 69.6 | 68.0 | 68.7 | 68.4 | 69.1 | 68.8 | 69.2 | 67.0 | 68.7 |
| 10 | 69.8 | 69.6 | 69.7 | 68.2 | 68.9 | 68.5 | 69.2 | 68.9 | 69.2 | 67.7 | 68.8 |
| 9 | 69.8 | 69.6 | 69.6 | 68.0 | 68.9 | 68.5 | 69.2 | 68.8 | 69.2 | 67.1 | 68.6 |
| 8 | 69.8 | 69.6 | 69.7 | 68.0 | 68.8 | 68.4 | 69.1 | 68.7 | 69.1 | 67.5 | 68.7 |
| 7 | 69.8 | 69.5 | 69.6 | 68.0 | 68.7 | 68.3 | 69.1 | 68.7 | 69.1 | 66.8 | 68.6 |
| 6 | 69.9 | 69.6 | 69.6 | 68.0 | 68.8 | 68.3 | 69.0 | 68.6 | 69.1 | 67.1 | 68.6 |
| 5 | 69.9 | 69.6 | 69.5 | 68.1 | 68.8 | 68.3 | 69.1 | 68.7 | 69.2 | 67.4 | 68.7 |
| 4 | 69.9 | 69.7 | 69.7 | 68.2 | 68.9 | 68.6 | 69.2 | 68.8 | 69.3 | 67.5 | 68.9 |
| 3 | 70.0 | 69.8 | 69.8 | 68.3 | 69.0 | 68.7 | 69.3 | 69.0 | 69.4 | 67.8 | 68.9 |
| 2 | 70.1 | 69.9 | 69.9 | 68.3 | 69.0 | 68.9 | 69.5 | 69.1 | 69.5 | 67.8 | 69.0 |
| 1 | 70.1 | 69.9 | 70.0 | 68.3 | 69.1 | 69.1 | 69.5 | 69.2 | 69.6 | 68.1 | 69.2 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,464 | 1,461 | 2,429 |
| Direction of | avel | > | > | > | > | > | > | > | > | > |  |


| Time Period | Average Speed (mph)- PM Peak |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 69.8 | 69.5 | 69.7 | 68.1 | 68.8 | 68.6 | 69.1 | 68.9 | 69.2 | 67.5 | 68.7 |
| 11 | 69.8 | 69.4 | 69.6 | 68.1 | 68.8 | 68.5 | 69.1 | 68.9 | 69.1 | 67.2 | 68.6 |
| 10 | 69.7 | 69.3 | 69.5 | 67.7 | 68.5 | 68.2 | 68.8 | 68.4 | 68.9 | 66.7 | 68.4 |
| 9 | 69.6 | 69.0 | 69.3 | 67.6 | 68.5 | 68.1 | 68.7 | 68.5 | 68.8 | 66.7 | 68.3 |
| 8 | 69.6 | 69.1 | 69.4 | 67.4 | 68.3 | 68.0 | 68.7 | 68.4 | 68.8 | 66.2 | 68.2 |
| 7 | 69.7 | 69.1 | 69.4 | 67.7 | 68.5 | 68.2 | 68.8 | 68.5 | 68.8 | 66.6 | 68.3 |
| 6 | 69.7 | 69.2 | 69.5 | 67.6 | 68.4 | 68.3 | 68.8 | 68.5 | 68.8 | 66.8 | 68.3 |
| 5 | 69.7 | 69.2 | 69.5 | 67.7 | 68.5 | 68.2 | 68.8 | 68.5 | 68.8 | 66.8 | 68.4 |
| 4 | 69.7 | 69.3 | 69.5 | 67.7 | 68.4 | 68.2 | 68.8 | 68.6 | 68.8 | 66.7 | 68.4 |
| 3 | 69.7 | 69.2 | 69.5 | 67.8 | 68.6 | 68.3 | 69.0 | 68.6 | 69.0 | 67.1 | 68.5 |
| 2 | 69.8 | 69.4 | 69.7 | 68.1 | 68.8 | 68.7 | 69.1 | 68.8 | 69.1 | 67.5 | 68.7 |
| 1 | 69.8 | 69.4 | 69.6 | 67.6 | 68.5 | 68.4 | 69.0 | 68.7 | 69.0 | 67.3 | 68.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,464 | 1,461 | 2,429 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > |

## AVERAGE SPEED DIFFERENCE (mph)

| Diff: | 5 mph | 10 mph | 15 mph | 20 mph | 25 mph | 30 mph |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Upper: | 70 | $<65$ | $<60$ | $<55$ | $<50$ | $<45$ |
| Lower: | 65 | 60 | 55 | 50 | 45 | 0 |

(Posted Speed-Avg. Speed)

## Figure 3-12: I-75 Density Contour Plots

I-75 NORTHBOUND

| Time | Average Density (veh/mi/ln) - AM Peak |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 9.9 | 10.1 | 7.9 | 8.7 | 8.7 | 8.9 | 6.4 | 7.6 | 7.5 |
| 11 | 11.0 | 11.1 | 8.6 | 9.4 | 9.4 | 9.5 | 6.8 | 8.0 | 7.9 |
| 10 | 10.7 | 10.8 | 8.5 | 9.3 | 9.3 | 9.5 | 6.7 | 7.8 | 7.8 |
| 9 | 10.6 | 10.8 | 8.4 | 9.1 | 9.1 | 9.2 | 6.6 | 7.6 | 7.6 |
| 8 | 10.3 | 10.5 | 8.1 | 9.0 | 9.1 | 9.4 | 6.8 | 8.0 | 8.0 |
| 7 | 12.0 | 12.2 | 9.3 | 10.2 | 10.2 | 10.5 | 7.5 | 8.9 | 8.8 |
| 6 | 12.0 | 12.1 | 9.3 | 10.3 | 10.2 | 10.3 | 7.4 | 8.7 | 8.7 |
| 5 | 11.6 | 11.8 | 9.2 | 10.0 | 9.9 | 9.9 | 7.1 | 8.3 | 8.3 |
| 4 | 10.2 | 10.3 | 7.9 | 8.6 | 8.6 | 8.7 | 6.1 | 7.3 | 7.3 |
| 3 | 9.7 | 9.8 | 7.6 | 8.3 | 8.2 | 8.3 | 5.8 | 6.8 | 6.8 |
| 2 | 8.9 | 8.9 | 6.9 | 7.5 | 7.4 | 7.4 | 5.3 | 6.2 | 6.2 |
| 1 | 7.0 | 7.0 | 5.5 | 5.9 | 5.8 | 5.7 | 4.1 | 4.9 | 4.8 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 2,702 | 1,479 | 3,134 | 1,500 | 16,309 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | > | > | $>$ | > | > | > | > |


| Time <br> Period | Average Density (veh/mi/ln) - AM Peak |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 9.4 | 9.5 | 7.4 | 8.1 | 8.1 | 8.4 | 5.8 | 6.6 | 6.6 |  |
| 11 | 10.2 | 10.3 | 8.1 | 8.9 | 8.9 | 9.1 | 6.3 | 7.0 | 7.0 |  |
| 10 | 10.7 | 10.9 | 8.5 | 9.4 | 9.5 | 9.8 | 6.8 | 7.6 | 7.6 |  |
| 9 | 12.0 | 12.2 | 9.5 | 10.5 | 10.5 | 10.8 | 7.4 | 8.2 | 8.2 |  |
| 8 | 12.2 | 12.3 | 9.7 | 10.7 | 10.6 | 10.8 | 7.5 | 8.3 | 8.2 |  |
| 7 | 12.2 | 12.3 | 9.5 | 10.4 | 10.3 | 10.4 | 7.2 | 8.1 | 8.1 |  |
| 6 | 11.3 | 11.5 | 8.8 | 9.8 | 9.8 | 10.1 | 7.0 | 7.8 | 7.8 |  |
| 5 | 11.6 | 11.7 | 9.1 | 10.0 | 10.0 | 10.2 | 7.1 | 7.9 | 7.9 |  |
| 4 | 11.5 | 11.6 | 9.1 | 10.0 | 9.9 | 10.2 | 7.0 | 7.9 | 7.9 |  |
| 3 | 11.6 | 11.7 | 9.1 | 9.9 | 9.8 | 9.9 | 6.7 | 7.5 | 7.5 |  |
| 2 | 10.4 | 10.5 | 8.1 | 9.0 | 8.9 | 9.2 | 6.3 | 7.1 | 7.1 |  |
| 1 | 10.6 | 10.8 | 8.4 | 9.3 | 9.3 | 9.4 | 6.5 | 7.3 | 7.3 |  |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |  |
| Int. | I-75 | US 27 Interchange |  | I-75 | SR 326 Interchange | $1-75$ |  |  |  |  |
| Length (ft) | 2,702 | 1,479 | 3,134 | 1,500 | 16,309 | 1,500 | 3,094 | 1,495 | 3,759 |  |
| Direction of Travel | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ |  |  |

I-75 SOUTHBOUND

| Time Period | Average Density (veh/mi/ln) - AM Peak |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 4.6 | 4.6 | 4.1 | 5.4 | 5.3 | 5.9 | 5.8 | 5.9 | 5.3 | 7.8 | 7.7 |
| 11 | 5.1 | 5.0 | 4.6 | 5.9 | 5.8 | 6.4 | 6.4 | 6.4 | 5.7 | 8.5 | 8.3 |
| 10 | 4.9 | 4.9 | 4.4 | 5.6 | 5.5 | 6.2 | 6.2 | 6.1 | 5.5 | 8.0 | 7.9 |
| 9 | 4.9 | 4.9 | 4.4 | 5.7 | 5.6 | 6.2 | 6.2 | 6.2 | 5.5 | 8.1 | 8.0 |
| 8 | 4.9 | 4.8 | 4.3 | 5.8 | 5.7 | 6.3 | 6.4 | 6.5 | 5.8 | 8.4 | 8.3 |
| 7 | 5.8 | 5.7 | 5.2 | 6.8 | 6.7 | 7.4 | 7.4 | 7.3 | 6.6 | 9.7 | 9.4 |
| 6 | 5.8 | 5.7 | 5.2 | 6.8 | 6.7 | 7.4 | 7.3 | 7.3 | 6.5 | 9.5 | 9.3 |
| 5 | 5.7 | 5.7 | 5.1 | 6.5 | 6.4 | 7.2 | 7.0 | 6.9 | 6.2 | 8.9 | 8.7 |
| 4 | 4.9 | 4.9 | 4.4 | 5.8 | 5.7 | 6.2 | 6.2 | 6.1 | 5.4 | 7.8 | 7.6 |
| 3 | 4.7 | 4.6 | 4.2 | 5.3 | 5.2 | 5.8 | 5.7 | 5.7 | 5.1 | 7.3 | 7.2 |
| 2 | 4.3 | 4.2 | 3.7 | 4.8 | 4.7 | 5.2 | 5.0 | 4.9 | 4.3 | 6.3 | 6.2 |
| 1 | 3.3 | 3.3 | 2.9 | 3.9 | 3.8 | 4.2 | 4.1 | 4.1 | 3.6 | 5.2 | 5.1 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3,001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,464 | 1,461 | 2,429 |
| Direction of | Travel | > | > | > | $>$ | > | > | > | > | > | > |


| Time | Average Density (veh/mi/ln) - AM Peak |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 5.9 | 5.8 | 4.8 | 6.4 | 6.3 | 6.8 | 6.9 | 6.9 | 6.3 | 8.7 | 8.6 |
| 11 | 6.4 | 6.3 | 5.2 | 6.8 | 6.7 | 7.3 | 7.3 | 7.3 | 6.8 | 9.6 | 9.3 |
| 10 | 6.7 | 6.6 | 5.5 | 7.3 | 7.2 | 7.8 | 7.9 | 8.0 | 7.4 | 10.3 | 10.1 |
| 9 | 7.7 | 7.6 | 6.4 | 8.3 | 8.2 | 8.9 | 8.9 | 8.9 | 8.1 | 11.3 | 11.0 |
| 8 | 7.9 | 7.8 | 6.5 | 8.6 | 8.5 | 9.1 | 9.1 | 9.2 | 8.4 | 11.7 | 11.4 |
| 7 | 8.0 | 7.8 | 6.5 | 8.7 | 8.6 | 9.2 | 9.0 | 9.0 | 8.2 | 11.3 | 11.0 |
| 6 | 7.5 | 7.3 | 6.2 | 8.2 | 8.1 | 8.7 | 8.8 | 8.8 | 8.1 | 11.0 | 10.8 |
| 5 | 7.6 | 7.6 | 6.3 | 8.4 | 8.3 | 9.0 | 8.8 | 8.8 | 8.1 | 11.2 | 10.9 |
| 4 | 7.5 | 7.4 | 6.2 | 8.1 | 8.0 | 8.7 | 8.6 | 8.6 | 7.9 | 11.0 | 10.7 |
| 3 | 7.6 | 7.5 | 6.2 | 8.2 | 8.1 | 8.7 | 8.5 | 8.4 | 7.7 | 10.5 | 10.3 |
| 2 | 6.8 | 6.7 | 5.6 | 7.3 | 7.2 | 7.7 | 7.8 | 7.9 | 7.2 | 9.7 | 9.6 |
| 1 | 7.0 | 6.9 | 5.8 | 7.7 | 7.7 | 8.2 | 8.1 | 8.0 | 7.3 | 10.1 | 9.9 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3,001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,464 | 1,461 | 2,429 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > |

LOS THRESHOLDS (Density in veh $/ \mathrm{mi} / \mathrm{In}$ )
LOS: LOSA LOSB LOSC LOSD LOSE LOSF Lower: $\begin{array}{lllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$ Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0>$ Using HCM 2010 thresholds for informational purposes

Table 3-13: Network Performance Summary

| Peak <br> Hour | 15-min Period | Total Delay (Hours) | Total <br> Stops | Average Speed (mph) | Vehicles <br> Arrived (Vehicles) | Vehicle- <br> Miles Traveled | Latent Delay <br> (Hours) | Latent Demand (Vehicles) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM | P1 | 5 | 615 | 58 | 1118 | 4325 | 0 | 0 |
|  | P2 | 7 | 883 | 57 | 1394 | 5391 | 0 | 0 |
|  | P3 | 8 | 952 | 57 | 1565 | 6016 | 0 | 0 |
|  | P4 | 8 | 1045 | 57 | 1660 | 6358 | 0 | 0 |
|  | P5 | 11 | 1323 | 56 | 1888 | 7287 | 0 | 0 |
|  | P6 | 12 | 1434 | 56 | 1986 | 7556 | 0 | 0 |
|  | P7 | 12 | 1392 | 56 | 2004 | 7588 | 0 | 0 |
|  | P8 | 9 | 1138 | 57 | 1776 | 6648 | 0 | 0 |
|  | P9 | 9 | 1137 | 57 | 1718 | 6575 | 0 | 0 |
|  | P10 | 9 | 1095 | 57 | 1748 | 6650 | 0 | 0 |
|  | P11 | 10 | 1180 | 57 | 1776 | 6786 | 0 | 0 |
|  | P12 | 8 | 1025 | 57 | 1675 | 6286 | 0 | 0 |
|  | PK Hour | 108 | 13,219 | 57 | 20,308 | 77,466 | 0 | 0 |
| PM | P1 | 11 | 1249 | 57 | 1908 | 7431 | 0 | 0 |
|  | P2 | 10 | 1226 | 57 | 1898 | 7199 | 0 | 0 |
|  | P3 | 12 | 1423 | 56 | 2011 | 7861 | 0 | 0 |
|  | P4 | 12 | 1399 | 56 | 2084 | 7963 | 0 | 0 |
|  | P5 | 13 | 1465 | 56 | 2090 | 8064 | 0 | 0 |
|  | P6 | 13 | 1469 | 56 | 2080 | 7950 | 0 | 0 |
|  | P7 | 13 | 1566 | 56 | 2161 | 8341 | 0 | 0 |
|  | P8 | 13 | 1565 | 56 | 2191 | 8417 | 0 | 0 |
|  | P9 | 14 | 1586 | 56 | 2152 | 8273 | 0 | 0 |
|  | P10 | 11 | 1276 | 56 | 1972 | 7433 | 0 | 0 |
|  | P11 | 10 | 1131 | 57 | 1825 | 6966 | 0 | 0 |
|  | P12 | 9 | 1047 | 57 | 1705 | 6460 | 0 | 0 |
|  | PK Hour | 141 | 16,402 | 56 | 24,077 | 92,358 | 0 | 0 |

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### 3.8 Safety Analysis

In accordance with the approved MLOU, a safety analysis was conducted for existing conditions utilizing crash data recorded within the IJR AOI between years 2013 and 2017. The AOI encompasses the I-75 mainline between US 27 and SR 326, the I-75 interchanges with US 27 and with SR 326, as well as the following adjacent segments and intersections:

- Intersection of US 27 at NW $44^{\text {th }}$ Avenue
- Intersection of US 27 at NW $35^{\text {th }}$ Avenue Road
- Segment of US 27 from NW $44^{\text {th }}$ Avenue to I-75 southbound ramps
- Segment of US 27 from I-75 northbound ramps to NW 35 th Avenue Road
- Segment of SR 326 from one-half mile west to I-75 southbound off-ramp
- Segment of SR 326 from I-75 northbound ramps to one-half mile east
- Segment of NW $44^{\text {th }}$ Avenue from US 27 to NW 49 ${ }^{\text {th }}$ Street
- Segment of NW 44 ${ }^{\text {th }}$ Avenue from NW 49 ${ }^{\text {th }}$ Street to SR 326

Crash data was obtained for a five-year period from January 1, 2013 through December 31, 2017. The crash data was obtained from the FDOT CAR Online database; the Signal Four Analytics application was used to obtain off system crash data, as well as a check against the CAR Online data. The following sections summarize the recorded crash data. Section 3.8.1 includes a summary of intersections within the AOI, and Sections 3.8.2 and 3.8.3 provide a summary of the crashes recorded on ramps and segments within the AOI, respectively. Police crash reports were reviewed for identified crash clusters/patterns. Figure 3-13 depicts the locations detailed in the following sections.

Each of the following sections will provide a comparison of the 5-year average actual crash rate for each facility against the statewide 5-year average crash rate on a similar facility, based on characteristics such as number of lanes, divided/undivided, number of legs at an intersection, freeway, arterial, collector, etc.

The equation for actual crash rates of an intersection is:

$$
R=\frac{1,000,000 \times \mathrm{C}}{365 \times \mathrm{N} \mathrm{xV}}
$$

Where:
$R=$ Crash rate for the intersection expressed as crashes per million entering vehicles (MEV).
$C=$ Total number of intersection crashes in the study period.
$N=$ Number of years of data.
$V=$ Traffic volumes entering the intersection daily (source: FTO 5-year Historical AADT Reports).


Figure 3-13: Existing Crash Analysis Location Legend

The equation for actual crash rates of a segment or on a ramp is:

$$
R=\frac{1,000,000 \times \mathrm{x}}{365 \times \mathrm{N} \mathrm{x} \mathrm{~V} \mathrm{x}}
$$

Where:
$R=$ Crash rate for the road segment expressed as crashes per million vehicle-miles of travel (MVMT).
$C=$ Total number of crashes in the study period.
$N=$ Number of years of data.
$V=$ Number of vehicles per day (both directions); obtained from FTO 5-year Historical AADT Reports.
$L=$ Length of the roadway segment in miles.
Crash rate calculation worksheets are provided in Appendix E.
District 5 intersection and segment High Crash Locations for the period from 2013 to 2017 were also obtained from the FDOT CAR Online database. The data was filtered to only include locations within Marion County; and then to only include intersections and segments corresponding to roadway section numbers going thru the study area. It should be noted that although the High Crash Locations are districtwide, actual crash rates are compared to statewide average crash rates per MEV or MVMT, for corresponding similar facilities. The resultant locations are further discussed in this section; detailed data is provided in Appendix $\mathbf{E}$.

### 3.8.1 Intersections

Six intersections were included in the existing conditions analysis, including two at each existing interchange ramp within the AOI. The crash severity and type recorded for each of the six intersections within the AOI during the five-year period, are summarized in Table 3-14 and crash rates provided in Table 3-15; 2013-2017 statewide average crash rate data is provided in Appendix E.

Table 3-14: Intersection Crash Summaries

| Location | Crash Severity \& Type |  |  |  | Year |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2013 | 2014 | 2015 | 2016 | 2017 | Total |
|  |  | Overall | 9 | 9 | 11 | 7 | 10 | 46 |
|  | Severity | Injury | 6 | 5 | 3 | 4 | 6 | 24 |
|  | Severity | Property Damage Only | 3 | 4 | 8 | 3 | 4 | 22 |
|  | Crash Type | Rear End | 3 | 5 | 6 | 5 | 7 | 26 |
|  |  | Left Turn | 2 | 2 | 1 | 2 | 2 | 9 |
|  |  | Angle | 0 | 2 | 1 | 0 | 0 | 3 |
|  |  | Off Road | 1 | 0 | 1 | 0 | 0 | 2 |
|  |  | Other | 3 | 0 | 2 | 0 | 1 | 6 |
|  | Overall |  | 2 | 3 | 5 | 6 | 11 | 27 |
|  | Severity | Injury | 1 | 1 | 4 | 1 | 4 | 11 |
|  |  | Property Damage Only | 1 | 2 | 1 | 5 | 7 | 16 |
|  | Crash Type | Rear End | 1 | 2 | 1 | 2 | 6 | 12 |
|  |  | Left Turn | 1 | 1 | 4 | 1 | 4 | 11 |
|  |  | Other | 0 | 0 | 0 | 3 | 1 | 4 |
|  |  | Overall | 6 | 6 | 10 | 4 | 4 | 30 |
|  | Severity | Injury | 3 | 4 | 5 | 0 | 2 | 14 |
|  | Severity | Property Damage Only | 3 | 2 | 5 | 4 | 2 | 16 |
|  | Crash Type | Rear End | 2 | 2 | 4 | 2 | 1 | 11 |
|  |  | Left Turn | 1 | 1 | 2 | 0 | 1 | 5 |
|  |  | Other | 3 | 3 | 4 | 2 | 2 | 14 |
|  | Overall |  | 3 | 4 | 10 | 7 | 14 | 38 |
|  |  | Injury | 0 | 2 | 2 | 3 | 9 | 16 |
|  | Severity | Property Damage Only | 3 | 2 | 8 | 4 | 5 | 22 |
|  | Crash Type | Rear End | 1 | 2 | 5 | 4 | 8 | 20 |
|  |  | Left Turn | 0 | 1 | 2 | 0 | 2 | 5 |
|  |  | Other | 2 | 1 | 3 | 3 | 4 | 13 |
|  |  | Overall | 6 | 4 | 7 | 2 | 12 | 31 |
|  |  | Injury | 2 | 0 | 2 | 1 | 4 | 9 |
|  | Severity | Property Damage Only | 4 | 4 | 5 | 1 | 8 | 22 |
|  | Crash Type | Rear End | 3 | 1 | 4 | 1 | 9 | 18 |
|  |  | Left Turn | 2 | 2 | 1 | 1 | 1 | 7 |
|  |  | Sideswipe | 1 | 0 | 2 | 0 | 0 | 3 |
|  |  | Other | 0 | 1 | 0 | 0 | 2 | 3 |
|  |  | Overall | 21 | 15 | 14 | 5 | 7 | 62 |
|  |  | Injury | 7 | 3 | 5 | 1 | 4 | 20 |
|  | Severity | Property Damage Only | 14 | 12 | 9 | 4 | 3 | 42 |
|  | Crash Type | Rear End | 10 | 13 | 8 | 0 | 0 | 31 |
|  |  | Sideswipe | 3 | 0 | 2 | 1 | 1 | 7 |
|  |  | Left Turn | 5 | 1 | 1 | 2 | 2 | 11 |
|  |  | Other | 3 | 1 | 3 | 2 | 4 | 13 |
|  |  | Overall | 0 | 1 | 0 | 1 | 1 | 3 |
|  | Severity | Injury | 0 | 1 | 0 | 1 | 1 | 3 |
|  | Severity | Property Damage Only | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Crash Type | Head On | 0 | 1 | 0 | 0 | 0 | 1 |
|  |  | Right Turn | 0 | 0 | 0 | 1 | 0 | 1 |
|  |  | Other | 0 | 0 | 0 | 0 | 1 | 1 |

Table 3-15: 5-Year (2013-2017) Intersection Crash Rates

| Intersection |  | Total Crashes | 5-Year AADT ${ }^{1}$ | Annual Crash Frequency | Crash Rate (per MEV) ${ }^{2}$ | Statewide 5YR Avg Crash Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| US 27 | NW 44 ${ }^{\text {th }}$ Avenue | 46 | 131,200 | 9.2 | 0.96 | 0.533 |
|  | I-75 SB ramps | 27 | 106,300 | 5.4 | 0.70 | 0.623 |
|  | I-75 NB ramps | 30 | 136,400 | 6.0 | 0.60 | 0.623 |
|  | NW 35 ${ }^{\text {th }}$ Avenue Road | 38 | 123,900 | 7.6 | 0.84 | 0.623 |
| SR 326 | I-75 SB off-ramp/NW 44 ${ }^{\text {th }}$ Avenue | 31 | 139,200 | 6.2 | 0.61 | 0.623 |
|  | I-75 NB ramps | 62 | 150,100 | 12.4 | 1.13 | 0.623 |
| NW 44 ${ }^{\text {th }}$ Ave | NW 49 ${ }^{\text {th }}$ Street | 3 | 36,800 | 0.6 | 0.22 | 0.419 |

${ }^{1}$ AADT entering intersection
${ }^{2}$ Corresponding AADTs obtained from 2017 FTO Historical AADT Reports

## US 27 at NW 44 ${ }^{\text {th }}$ Avenue

A total of 46 crashes were recorded at the intersection of US 27 at NW $44^{\text {th }}$ Avenue during the five-year period. Based on the AADT on US 27 and NW $44^{\text {th }}$ Avenue during the five-year period, 9.2 crashes per year represents a rate of approximately 0.96 crashes per MEV. The 2017 fiveyear average crash rate per MEV for similar Urban 4-5 Lane 2-Way Divided Paved intersections was approximately 0.533 ; showing that actual crashes for this location were substantially higher than average. US 27 at NW $44^{\text {th }}$ Avenue is reflected as a districtwide high crash intersection location.

Of the 24 injury crashes recorded at the intersection of US 27 and NW $44^{\text {th }}$ Avenue, 12 were rear end crashes, eight were left turn crashes, and three were angle crashes. According to crash data, four of the left turn crashes were between a through vehicle and a vehicle turning left during the permitted phase at the traffic signal.

## US 27 at I-75 Southbound Ramps

A total of 27 crashes were recorded at the intersection of US 27 and the I-75 southbound ramps during the five-year period. Based on the AADT on US 27 and on the I-75 southbound off-ramp during the five-year period, 5.4 crashes per year represents a rate of approximately 0.70 crashes per MEV. The 2017 five-year average crash rate per MEV for similar Urban 4-5 Lane 2-Way Divided Raised intersections was approximately 0.623 , showing that actual crashes for this location were higher than average. US 27 at the I-75 southbound ramps is reflected as a districtwide high crash intersection location.

Of the 11 injury crashes recorded at the intersection of US 27 and the I-75 southbound ramps, six were left turn crashes. Five of the left turn crashes were between an eastbound through vehicle and a westbound vehicle turning left during the permitted phase at the traffic signal.

## US 27 at I-75 Northbound Ramps

A total of 30 crashes were recorded at the intersection of US 27 and the I-75 northbound ramps during the five-year period. Based on the AADT of US 27 and the I-75 northbound off-ramp during the five-year period, 6.0 crashes per year represents a rate of approximately 0.60 crashes per MEV. The 2017 five-year average crash rate per MEV for similar Urban 4-5 Lane 2-Way Divided Raised intersections was approximately 0.623 ; showing that actual crashes for this location were slightly lower than average. However, US 27 at the I-75 northbound ramps is reflected as a districtwide high crash intersection location.

Of the 30 crashes recorded at the intersection of US 27 and the I-75 northbound ramps, 14 resulted in at least one injury. Eight of the injury crashes were rear end crashes and two were left turn crashes. Among the crash types classified as 'Other' at this location are two angle crashes, three off road crashes, one right turn crash, one sideswipe crash, and one pedestrian crash.

## US 27 at NW $35^{\text {th }}$ Avenue Road

A total of 38 crashes were recorded at the intersection of US 27 and NW $35^{\text {th }}$ Avenue Road during the five-year period. Based on the AADT of US 27 and NW $35^{\text {th }}$ Avenue Road during the five-year period, 7.6 crashes per year represents a rate of approximately 0.84 crashes per MEV. The 2017 five-year average crash rate per MEV for similar Urban 4-5 Lane 2-Way Divided Raised intersections was approximately 0.623 ; showing that actual crashes for this location were higher than average. However, it is not reflected as a districtwide high crash intersection location; possibly due to the reconfiguration of the intersection occurring within the 2013 - 2017 period.

Of the 38 crashes recorded at the intersection of US 27 and NW $35^{\text {th }}$ Avenue Road, 16 resulted in at least one injury. Nine of the injury crashes were rear end crashes and two were left turn crashes.

## SR 326 at I-75 Southbound Off-Ramp/NW 44 ${ }^{\text {th }}$ Avenue

A total of 31 crashes were recorded at the intersection of SR 326 and the I-75 southbound offramp/NW $44^{\text {th }}$ Avenue during the five-year period. Based on the AADT of SR 326, the I-75
southbound off-ramp, and NW $44^{\text {th }}$ Avenue, 6.2 crashes per year represents a rate of approximately 0.61 crashes per MEV. The 2017 five-year average crash rate per MEV for similar Urban 4-5 Lane 2-Way Divided Raised intersections was approximately 0.623 ; showing that actual crashes for this location were slightly lower than average. However, this intersection is reflected as a districtwide high crash location.

Nine of the 26 crashes at the intersection of SR 326 and the I- 75 southbound off-ramp/NW $44^{\text {th }}$ Avenue resulted in at least one injury. Seven of the nine injury crashes recorded at the intersection of SR 326 and the I-75 southbound off-ramp/NW $44^{\text {th }}$ Avenue were rear end crashes and one was a left turn crash. Six of the 17 total rear end crashes were in the westbound direction.

## SR 326 at I-75 Northbound Ramps

A total of 62 crashes were recorded at the intersection of SR 326 and the I-75 northbound ramps during the five-year period. Based on the AADT of SR 326 and the I-75 northbound off-ramp, 12.4 crashes per year represents a rate of approximately 1.13 crashes per MEV. The 2017 fiveyear average crash rate per MEV for similar Urban 4-5 Lane 2-Way Divided Raised intersections was approximately 0.623 . With this intersection having a crash rate significantly higher than that of similar intersections; it should be noted that in 2016, an auxiliary lane was added to the northbound off-ramp; showing that actual crashes for this location were significantly higher than average. SR 326 at the l-75 northbound ramps is reflected as a districtwide high crash intersection location.

Approximately 90 percent ( 27 crashes) of the rear end crashes recorded at the intersection of SR 326 and the I-75 northbound ramp involved two northbound vehicles on the I-75 off-ramp. This crash type represents almost half of the recorded injury crashes. Among the crash types classified as 'Other' at this location are four right turn crashes, one angle crash, and three off road crashes.

## NW 44 ${ }^{\text {th }}$ Avenue at NW 49 ${ }^{\text {th }}$ Street

A total of 3 crashes were recorded at the intersection of NW $44^{\text {th }}$ Avenue and NW $49^{\text {th }}$ Street during the five-year period. Based on the AADT of NW $44^{\text {th }}$ Avenue and NW $49^{\text {th }}$ Street during the five-year period, 0.6 crashes per year represents a rate of approximately 0.22 crashes per MEV. The 2017 five-year average crash rate per MEV for similar Urban 4-5 Lane 2-Way Raised
intersections was approximately 0.419 ; showing that actual crashes for this location were significantly lower than average.

All three (3) of the crashes recorded resulted in injury. One (1) of the crashes was head on and one (1) of the crashes was a right turn.

### 3.8.2 Interchange Ramps

The I-75 at US 27 interchange is a standard diamond interchange, featuring four ramps. The I75 and SR 326 interchange is a modified diamond interchange with a single "cloverleaf" ramp for westbound SR 326 traffic entering I-75 southbound. The crash severity and type recorded for the interchange ramp during the five-year period are summarized in Table 3-16 with crash rates provided in Table 3-17.

Table 3-16: Interchange Ramp Crash Summaries

| Location | Crash Severity \& Type |  |  |  | Year |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2013 | 2014 | 2015 | 2016 | 2017 | Total |
| $\begin{aligned} & \text { I-75 at US } 27 \text { Interchange } \\ & \text { ramps } \end{aligned}$ |  | Overall | 2 | 1 | 3 | 3 | 5 | 14 |
|  | Severity | Fatality | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Injury | 2 | 0 | 0 | 2 | 2 | 6 |
|  |  | Property Damage Only | 0 | 1 | 3 | 1 | 3 | 8 |
|  | Crash <br> Type | Rollover | 2 | 0 | 0 | 0 | 0 | 2 |
|  |  | Sideswipe | 0 | 0 | 1 | 1 | 0 | 2 |
|  |  | Rear End | 0 | 0 | 1 | 2 | 2 | 5 |
|  |  | Other | 0 | 1 | 1 | 0 | 3 | 5 |
| I-75 at SR 326 Interchange ramps |  | Overall | 5 | 6 | 4 | 12 | 19 | 46 |
|  | Severity | Fatality | 0 | 0 | 0 | 0 | 1 | 1 |
|  |  | Injury | 3 | 2 | 1 | 4 | 6 | 16 |
|  |  | Property Damage Only | 2 | 4 | 3 | 8 | 12 | 29 |
|  | Crash <br> Type | Rollover | 3 | 3 | 3 | 0 | 0 | 9 |
|  |  | Sideswipe | 0 | 0 | 0 | 3 | 3 | 6 |
|  |  | Right Turn | 0 | 1 | 0 | 0 | 1 | 2 |
|  |  | Off Road | 1 | 1 | 0 | 3 | 1 | 6 |
|  |  | Other | 1 | 1 | 1 | 6 | 14 | 23 |

Table 3-17: 5-Year (2013-2017) Individual Ramp Crash Rates

| Location | Length (mi) | Total <br> Crashes | 5-Year <br> AADT | Annual Crash <br> Frequency | Crash Rate <br> (per MVMT) ${ }^{\mathbf{2}}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| I-75 NB to US 27 | 0.26 | 4 | 31,500 | 0.8 | 1.34 |
| I-75 NB from US 27 | 0.31 | 2 | 10,350 | 0.4 | 1.71 |
| I-75 SB to US 27 | 0.30 | 6 | 11,900 | 1.2 | 4.60 |
| I-75 SB from US 27 | 0.30 | 2 | 33,100 | 0.4 | 0.55 |
| I-75 SB to SR 326 | 0.44 | 12 | 21,200 | 2.4 | 3.52 |
| I-75 NB to SR 326 | 0.25 | 25 | 50,500 | 5.0 | 5.43 |
| I-75 NB from SR 326 | 0.28 | $0^{3}$ | 19,200 | 0.0 | 0.00 |
| I-75 SB from SR 326 EB | 0.46 | 3 | 17,400 | 0.6 | 1.03 |
| I-75 SB from SR 326 WB | 0.29 | 6 | 32,100 | 1.2 | 1.77 |

${ }^{1}$ No statewide 5-year average crash rate for ramps provided in CAR Online
${ }^{2}$ Corresponding AADTs obtained from 2017 FTO Historical AADT Reports
${ }^{3}$ Zero crashes verified

## I-75 at US 27 Interchange

A total of 14 crashes were recorded on the ramps and merge/diverge areas at the I-75 at US 27 interchange during the five-year period (not including the intersections at ramp termini). There were six injury crashes. Two were rollovers by northbound vehicles on the northbound I-75 onramp and one involving a bicyclist being struck while crossing the northbound on-ramp. Based on the AADT reported for the ramps, the calculated crash rates for the northbound off/on ramps were 1.34 and 1.71 crashes per MVMT; with 4.60 and 0.55 for the southbound off/on ramps, respectively, during the five-year period. Calculation details are provided in Appendix E.

## I-75 at SR 326 Interchange

A total of 46 crashes were recorded on the ramps and merge/diverge areas at the I-75 at SR 326 interchange during the five-year period (not including the intersections at ramp termini).

The I-75 southbound off-ramp to SR 326 had 12 recorded crashes during the five-year period ( 3.52 crashes per MVMT), eight of which were rollover crashes. Five of the rollover crashes resulted in injuries to one or more persons involved in the crash. Five of the rollover crashes occurred under dark conditions and two occurred on a wet road surface. Detailed analysis of the adjacent interchanges is beyond the scope of this IJR; therefore, further study by the Department for possible causes and potential mitigation of the rollover crashes is recommended.

The I-75 southbound on-ramp from SR 326 eastbound had three recorded crashes during the five-year period, zero resulting in injury ( 1.03 crashes per MVMT). Two of the crashes were related to vehicles exiting the driveway immediately adjacent to the on-ramp diverge on SR 326.

The I-75 southbound on-ramp from SR 326 westbound had six recorded crashes during the fiveyear period, two resulting in injury ( 1.77 crashes per MVMT). Four of the crashes involved a same direction sideswipe and one was a rear end crash at the merge onto I-75.

The I-75 northbound off-ramp to SR 326 had 25 recorded crashes during the five-year period ( 5.43 crashes per MVMT), One being a rollover crash that resulted in an injury. These crashes are in addition to those recorded at the signalized intersection with SR 326.

Although crashes occurred at the ramp terminal, there were no recorded crashes during the fiveyear period for the I-75 northbound on-ramp from SR 326.

### 3.8.3 Segments

The segments evaluated for the existing conditions analysis include the segments of I-75 between ramps at each study interchange, the 3.7 -mile segment of I-75 between the two interchanges, the segment of US 27 and SR 326 from the l-75 ramps to the nearest signalized intersection in either direction (or a half-mile segment, if no signalized intersection is within the AOI), and two segments of NW $44^{\text {th }}$ Avenue. The crash severity and type recorded for the segments during the five-year period are summarized in Table 3-18 with crash rates provided in Table 3-19; 2013-2017 statewide average crash rate data is provided in Appendix $\mathbf{E}$.

Table 3-18: Segment Crash Summaries

| Location | Crash Severity \& Type |  | Year |  |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2013 | 2014 | 2015 | 2016 | 2017 |  |
|  |  | Overall | 15 | 26 | 11 | 11 | 6 | 69 |
|  | Severity | Injury | 4 | 4 | 4 | 3 | 2 | 17 |
|  |  | Property Damage Only | 11 | 22 | 7 | 8 | 4 | 52 |
|  | Crash Type | Rear End | 4 | 14 | 8 | 6 | 3 | 35 |
|  |  | Off Road | 7 | 6 | 3 | 2 | 1 | 19 |
|  |  | Sideswipe | 3 | 3 | 0 | 2 | 0 | 8 |
|  |  | Other | 1 | 3 | 0 | 1 | 2 | 7 |
|  |  | Overall | 55 | 81 | 111 | 82 | 82 | 411 |
|  | Severity | Fatal | 0 | 0 | 0 | 1 | 0 | 1 |
|  |  | Injury | 9 | 21 | 29 | 20 | 23 | 102 |
|  |  | Property Damage Only | 46 | 60 | 82 | 61 | 59 | 308 |
|  | Crash Type | Rear End | 22 | 40 | 45 | 28 | 40 | 175 |
|  |  | Off Road | 12 | 16 | 18 | 20 | 17 | 83 |
|  |  | Sideswipe | 10 | 14 | 23 | 15 | 14 | 76 |
|  |  | Rollover | 3 | 3 | 6 | 6 | 3 | 21 |
|  |  | Other | 8 | 8 | 19 | 13 | 8 | 56 |
|  |  | Overall | 11 | 19 | 22 | 24 | 33 | 109 |
|  | Severity | Injury | 2 | 5 | 5 | 7 | 11 | 30 |
|  |  | Property Damage Only | 9 | 14 | 17 | 17 | 22 | 79 |
|  | Crash Type | Rear End | 2 | 6 | 11 | 11 | 16 | 46 |
|  |  | Sideswipe | 4 | 5 | 2 | 10 | 6 | 27 |
|  |  | Off Road | 3 | 4 | 4 | 1 | 3 | 15 |
|  |  | Rollover | 2 | 0 | 2 | 0 | 0 | 4 |
|  |  | Other | 0 | 4 | 3 | 2 | 8 | 17 |
|  |  | Overall | 14 | 14 | 25 | 11 | 9 | 73 |
|  |  | Fatal | 0 | 0 | 0 | 1 | 0 | 1 |
|  | Severity | Injury | 6 | 3 | 7 | 4 | 3 | 23 |
|  |  | Property Damage Only | 8 | 11 | 18 | 6 | 6 | 49 |
|  | Crash Type | Rear End | 5 | 4 | 11 | 2 | 5 | 27 |
|  |  | Left Turn | 3 | 4 | 4 | 4 | 1 | 16 |
|  |  | Sideswipe | 1 | 1 | 3 | 2 | 1 | 8 |
|  |  | Angle | 2 | 2 | 3 | 0 | 1 | 8 |
|  |  | Other | 3 | 3 | 4 | 3 | 1 | 14 |
|  |  | Overall | 4 | 4 | 1 | 1 | 0 | 10 |
|  | Severity | Injury | 1 | 0 | 1 | 1 | 0 | 3 |
|  |  | Property Damage Only | 3 | 4 | 0 | 0 | 0 | 7 |
|  | Crash Types | Rear End | 1 | 0 | 0 | 0 | 0 | 1 |
|  |  | Sideswipe | 0 | 2 | 0 | 0 | 0 | 2 |
|  |  | Other | 3 | 2 | 1 | 1 | 0 | 7 |

Table 3-18: Segment Crash Summaries (continued)

| Location | Crash Severity \& Type |  | Year |  |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2013 | 2014 | 2015 | 2016 | 2017 |  |
| $\begin{aligned} & \stackrel{n}{1} \\ & \stackrel{1}{0} \\ & 3 \\ & \mathbf{N} \\ & \underset{\sim}{N} \\ & \underset{\sim}{n} \end{aligned}$ |  | Overall | 3 | 2 | 2 | 1 | 6 | 14 |
|  | Severity | Injury <br> Property Damage Only | $\begin{aligned} & 0 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ | $0$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $3$ | $5$ |
|  | Crash Type | Rear End Left Turn Other | $\begin{aligned} & \hline 1 \\ & 1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1 \\ & 1 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1 \\ & 0 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 2 \\ & 4 \\ & 0 \end{aligned}$ | $\begin{aligned} & 5 \\ & 7 \\ & 2 \\ & \hline \end{aligned}$ |
|  |  | Overall | 11 | 23 | 35 | 35 | 28 | 132 |
|  | Severity | Fatality <br> Injury <br> Property Damage Only | $\begin{aligned} & 0 \\ & 3 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{gathered} 1 \\ 4 \\ 18 \end{gathered}$ | $\begin{gathered} 0 \\ 7 \\ 28 \end{gathered}$ | $\begin{gathered} 0 \\ 9 \\ 26 \end{gathered}$ | $\begin{gathered} 0 \\ 12 \\ 16 \end{gathered}$ | $\begin{gathered} 1 \\ 35 \\ 96 \\ \hline \end{gathered}$ |
|  | Crash Type | Rear End <br> Off Road <br> Sideswipe <br> Rollover <br> Other | $\begin{aligned} & 3 \\ & 1 \\ & 4 \\ & 0 \\ & 3 \end{aligned}$ | $\begin{gathered} 3 \\ 0 \\ 9 \\ 0 \\ 11 \end{gathered}$ | $\begin{gathered} 2 \\ 0 \\ 10 \\ 1 \\ 22 \end{gathered}$ | $\begin{gathered} 7 \\ 0 \\ 5 \\ 0 \\ 23 \end{gathered}$ | $\begin{gathered} 8 \\ 1 \\ 5 \\ 0 \\ 14 \end{gathered}$ | $\begin{gathered} 23 \\ 2 \\ 33 \\ 1 \\ 73 \\ \hline \end{gathered}$ |
|  |  | Overall | 7 | 3 | 8 | 6 | 5 | 29 |
|  | Severity | Injury <br> Property Damage Only | $\begin{array}{r} 2 \\ 5 \\ \hline \end{array}$ | $\begin{aligned} & 1 \\ & 2 \\ & \hline \end{aligned}$ | $3$ | $\begin{aligned} & 1 \\ & 5 \end{aligned}$ | $3$ | $\begin{aligned} & 10 \\ & 19 \end{aligned}$ |
|  | Crash <br> Type | Off Road <br> Rear End Left Turn Angle Other | $\begin{aligned} & 3 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2 \\ & 0 \\ & 0 \\ & 0 \\ & 1 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \\ & 0 \\ & 3 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2 \\ & 0 \\ & 1 \\ & 0 \\ & 3 \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 0 \\ & 2 \\ & 2 \end{aligned}$ | $\begin{aligned} & 9 \\ & 3 \\ & 2 \\ & 6 \\ & 9 \\ & \hline \end{aligned}$ |
|  |  | Overall | 4 | 3 | 1 | 2 | 4 | 14 |
|  | Severity | Injury <br> Property Damage Only | $\begin{aligned} & 1 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1 \\ & 2 \\ & \hline \end{aligned}$ | $0$ | $\begin{aligned} & 1 \\ & 1 \\ & \hline \end{aligned}$ |  |  |
|  | Crash Type | Off Road Rear End Left Turn Other | $\begin{aligned} & 2 \\ & 0 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & \hline 0 \\ & 2 \\ & 0 \\ & 1 \end{aligned}$ | $\begin{aligned} & \hline 1 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \hline 0 \\ & 0 \\ & 0 \\ & 2 \end{aligned}$ | 2 1 1 0 | 5 3 2 4 |

Table 3-19: 5-Year (2013-2017) Segment Crash Rates

| Roadway | Segment Limits | Length (mi) | Total Crashes | 5-Year AADT | Annual Crash Frequency | Crash Rate $\left(\right.$ per MVMT) ${ }^{1}$ | Statewide 5YR Avg Crash Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-75 | between US 27 ramps | 0.70 | 69 | 170,800 | 13.8 | 1.58 | 0.976 |
|  | US 27 to SR 326 | 3.70 | 411 | 333,500 | 82.2 | 0.91 | 0.976 |
|  | between SR 326 ramps | 0.70 | 109 | 129,500 | 21.8 | 3.29 | 0.976 |
| US 27 | NW 44 ${ }^{\text {th }}$ Avenue to l-75 SB ramps | 0.57 | 73 | 94,400 | 14.6 | 3.72 | 5.884 |
|  | I-75 NB ramps to NW 35 ${ }^{\text {th }}$ Ave Rd | 0.25 | 10 | 104,900 | 2.0 | 1.04 | 3.364 |
| SR 326 | 1/2 mile west of SB ramps | 0.50 | 14 | 99,600 | 2.8 | 0.77 | 3.364 |
|  | NB ramps to $1 / 2$ mile east | 0.68 | 132 | 99,600 | 26.4 | 5.34 | 5.884 |
| NW 44 ${ }^{\text {th }}$ | US 27 to NW 49 ${ }^{\text {th }}$ Street | 1.85 | 29 | 36,800 | 5.8 | 1.17 | 3.364 |
| Avenue | NW 49 ${ }^{\text {th }}$ Street to SR 326 | 2.13 | 14 | 36,800 | 2.8 | 0.49 | 3.654 |

${ }^{1}$ Corresponding AADTs obtained from 2017 FTO Historical AADT Reports

## I-75 between US 27 Ramps

A total of 69 crashes were recorded on the 0.70 -mile segment of I-75 between the US 27 interchange ramps during the five-year period. Based on the AADT of I-75 during this period, 13.8 crashes per year represents a rate of approximately 1.58 crashes per MVMT. The average crash rate for urban interstate segments in 2017 was approximately 0.976 crashes per MVMT; showing that actual crashes for this location were significantly higher than average. I-75 between the US 27 interchange ramps is reflected as a districtwide high crash segment location.

Rear end crashes accounted for 11 of the 17 injury crashes on this segment. Approximately twothirds ( 22 crashes) of the 35 total rear end crashes were between southbound vehicles. More than half (43 crashes) of the recorded crashes on this segment occurred between 1:00 and 6:00 PM.

## I-75 from US 27 to SR 326

A total of 411 crashes were recorded on the 3.70-mile segment of I-75 between US 27 and SR 326 during the five-year period. Based on the AADT of I-75 during the five-year period, 82.2 crashes per year represents a rate of approximately 0.91 crashes per MVMT. The average crash rate for urban interstate segments in 2017 was approximately 0.976 crashes per MVMT; showing that actual crashes for this location were slightly lower than average. However, I-75 between the US 27 and SR 326 is reflected as a districtwide high crash segment location.

Of the injury crashes, 45 percent were rear end crashes. Forty-three percent of total crashes were rear end and 15 percent were sideswipe crashes. The directionality of crashes included 55 percent occurring on the northbound lanes and 45 percent on the southbound lanes.

Approximately 35 percent of crashes occurred under dark conditions (including dawn and dusk) and 24 percent of crashes occurred with wet surface conditions. Of the 56 crashes classified as 'Other' at this location, 50 percent ( 23 crashes) involved a vehicle striking debris or lost cargo on the interstate.

## I-75 between SR 326 Ramps

A total of 109 crashes were recorded on the 0.70 -mile segment of I-75 between the SR 326 interchange ramps during the five-year period. Based on the AADT of I-75 during this period, 21.8 crashes per year represents a rate of approximately 3.29 crashes per MVMT. The average crash rate for urban interstate segments in 2017 was approximately 0.976 crashes per MVMT; showing that actual crashes for this location were significantly higher than average. I-75 between the SR 326 interchange ramps is reflected as a districtwide high crash segment location.

The highest crash type recorded on this segment of I-75 between SR 326 ramps was rear end with 46 crashes, 26 sideswipe and 15 off-road crashes. Approximately two-thirds of the recorded crashes occurred in the southbound lanes during the five-year period.

## US 27 from NW 44 ${ }^{\text {th }}$ Avenue to I-75 Southbound Ramps

A total of 72 crashes were recorded on the 0.57 -mile segment of US 27 between NW $44^{\text {th }}$ Avenue and the I-75 southbound ramps during the five-year period. Based on the AADT of US 27 during this period, 14.6 crashes per year represents a rate of approximately 3.72 crashes per MVMT. The average crash rate in 2017 for an urban four-lane arterial with raised median was approximately 5.884 crashes per MVMT; showing that actual crashes for this location were lower than average. However, US 27 between NW $44^{\text {th }}$ Avenue and the I-75 southbound ramps is reflected as a districtwide high crash segment location.

Ten of the injury crashes were rear end and six were left turn. Approximately 41 percent of the recorded crashes during the five-year period occurred under dark conditions (including dawn and dusk) and 25 percent occurred with wet surface conditions.

## US 27 from I-75 Northbound Ramps to NW 35 th Avenue Road

A total of 10 crashes were recorded on the 0.25 -mile segment of US 27 between the I-75 northbound ramps and NW $35^{\text {th }}$ Avenue Road during the five-year period. Based on the AADT of US 27 during the five-year period, two crashes per year represents a rate of approximately 1.04 crashes per MVMT. The average crash rate in 2017 for an urban four-lane arterial with
raised median was approximately 3.364 crashes per MVMT; showing that actual crashes for this location were lower than average.

Five of the ten crashes were recorded on Short Forms by the Ocala Police Department, with limited information. The other five crashes included two sideswipe crashes, one rear end crash, and one angle crash.

## SR 326 one-half mile west of I-75

A total of 14 crashes were recorded on SR 326 on the half-mile segment west of the I-75 southbound off-ramp. Based on the AADT of SR 326 during the five-year period, 2.8 crashes per year represent a rate of approximately 0.77 crashes per MVMT. The average crash rate in 2017 for an urban four-lane arterial with raised median was approximately 3.364 crashes per MVMT and for an urban two-lane undivided arterial was approximately 3.1 crashes per MVMT; showing that actual crashes for this location were slightly higher than average.

## SR 326 from I-75 Northbound Ramps to one-half mile East

A total of 132 crashes were recorded on the 0.68 -mile segment of SR 326 from the $\mathrm{I}-75$ northbound ramps to one-half mile east. Based on the AADT of SR 326 during the five-year period, 26.4 crashes per year represent a rate of approximately 5.34 crashes per MVMT. The average crash rate in 2017 for an urban four-lane arterial with paved median was approximately 5.884 crashes per MVMT; showing that actual crashes for this location were lower than average.

The only fatal crash within the AOI occurred on this segment of SR 326, when a westbound vehicle struck an intoxicated pedestrian who was improperly walking in the roadway.

Fourteen of the 35 injury crashes were left turn crashes and 12 were rear end crashes. Approximately 15 percent of crashes occurred under dark conditions (including dawn and dusk) and approximately 14 percent of the crashes occurred with wet surface conditions.

## NW 44 ${ }^{\text {th }}$ Avenue from US 27 to NW 49 ${ }^{\text {th }}$ Street

A total of 29 crashes were recorded on the 1.85 -mile segment of NW $44^{\text {th }}$ Avenue between US 27 and NW 49 ${ }^{\text {th }}$ Street. Based on the AADT of NW $44^{\text {th }}$ Avenue during the five-year period, 5.8 crashes per year represent a rate of approximately 1.17 crashes per MVMT. The average crash rate in 2017 for an urban four-lane collector with raised median was approximately 3.364 crashes per MVMT; showing that actual crashes for this location were lower than average.

Approximately 31 percent of the recorded crashes occurred under dark conditions and 14 percent occurred with wet surface conditions.

## NW 44 ${ }^{\text {th }}$ Avenue from NW 49 ${ }^{\text {th }}$ Street to SR 326

A total of 17 crashes were recorded on the 2.13 -mile segment of NW $44^{\text {th }}$ Avenue between NW $49^{\text {th }}$ Street and SR 326. Based on the AADT of NW $44^{\text {th }}$ Avenue during the five-year period, 2.8 crashes per year represent a rate of approximately 0.49 crashes per MVMT. The average crash rate in 2017 for an urban four-lane collector with raised median was approximately 3.654 crashes per MVMT; showing that actual crashes for this location were significantly lower than average.

Approximately 35 percent of the recorded crashes occurred under dark conditions (including dawn and dusk) and 12 percent occurred with wet surface conditions.

### 3.8.4 Overall Summary

Overall, 1,157 crashes were recorded within the AOI during the five-year period. Figures 3-14 through 3-16 summarize the crash severity, crash types, and various crash conditions of the cumulative data recorded within the AOI. There was a noticeable increase in annual crashes in years 2014 and 2015; however, there was not a proportionate change in AADTs to suggest these increases were directly correlated to increased exposure. The findings from this safety analysis will be shared with the District Safety Office. Corresponding crash data tables for the five-year evaluation period are provided in Appendix E.


Figure 3-14: Crash Severity by Year


Figure 3-15: Crash Type Summary (2013-2017)


Figure 3-16: Crash Conditions (2013-2017)

## 4 Alternatives Discussion

This section of the report discusses the interchange alternatives considered as part of the IJR process. The general alternatives considered for the project are No Build, TSM\&O and Build alternatives. Each of the alternatives are discussed in greater detail in the following sections.

### 4.1 No Build Alternative

The No Build alternative assumes that a new interchange facility will not be constructed within the AOI and that existing conditions will remain. The purpose of the No Build condition analysis is to identify the need for improvements and to compare it to the future Build condition analysis. For this study, the No Build alternative includes all other planned and programmed roadway improvements (financially feasible) expected to be open to traffic as specified in the 2040 Ocala/Marion TPO LRTP. The No Build alternative includes projects such as Phases 2B and 2C of the NW 49 ${ }^{\text {th }}$ Street Extension.

### 4.2 Transportation Systems Management \& Operations Alternative

TSM\&O Improvements typically involve the utilization of comparatively lower cost traffic management strategies to serve the projected traffic demand in lieu of implementing/constructing the proposed project. Examples of TSM\&O improvements include adding turn lanes at existing intersections, improving the operation of the existing signals and widening existing roadways. The intent of the TSM\&O alternative is to determine whether there is a more cost-effective alternative to constructing a new interchange.

As discussed in Section 2 regarding the purpose and need for the project, one of the primary intents of the proposed interchange at I-75 and NW 49 ${ }^{\text {th }}$ Street is to provide a direct connection to I-75 to serve traffic; including significant truck traffic associated with Ocala 489 and the contiguous employment center and commercial district. Consequently, a standalone TSM\&O alternative does not meet this need; therefore, was not further considered as part of this IJR. Although a TSM\&O alternative does not meet the purpose and need for the project as a standalone alternative; it is recommended to integrate the proposed interchange into the surrounding existing and planned TSM\&O network as identified in the Marion County TSM\&O Master Plan and the FDOT F.R.A.M.E. project (FM Number 440900-1). As part of the F.R.A.M.E. project, roadside units are being deployed along I-75 as well as the adjacent interchanges of US 27 and SR 326. Figure 4-1 illustrates the surrounding existing and planned TSM\&O network as well as recommended elements for the proposed interchange.


### 4.3 Build Alternatives

Eight (8) build interchange alternatives were initially considered. Five (5) of the alternatives involved different variations of diamond interchanges, while other options included Parclo, SPUI, roundabout and bowtie configurations. A preliminary evaluation was conducted using a numerical/descriptive matrix approach; to identify which configurations were inferior. This initial evaluation included 13 engineering, environmental, socio-economic and cost factors (see Appendix F for excerpt from the PER). Based on the results, five (5) build alternative interchange layouts will be further considered: Diamond Interchange, SPUI, Parclo-SE, ParcloNE and DDI.

It should be noted, an Intersection Control Evaluation (ICE) CAP-X analysis was not performed for the proposed I-75 interchange at NW 49th Street; based on coordination with Traffic Engineering and Operations in Central Office. The current version of ICE published by FDOT is intended to be used only for at grade intersections.

### 4.3.1 Access Management

The preferred alternative of NW $49^{\text {th }}$ Street from NW 44 ${ }^{\text {th }}$ Avenue to Marion County's future NW $35^{\text {th }}$ Street extension (currently in final design). NW 49 ${ }^{\text {th }}$ Street (shown on Figure 4-2) will be signalized at NW $44^{\text {th }}$ Avenue and the I-75 ramp terminals; there will be no traffic signals within one-half mile, east of the interchange. NW 49 ${ }^{\text {th }}$ Street will feature four 12 -foot travel lanes with 7 -foot bicycle lanes, a 28 -foot raised median, and 6 -foot sidewalk. The proposed right-of-way for NW 49 ${ }^{\text {th }}$ Street is 120 feet. NW 49 ${ }^{\text {th }}$ Street will curve towards the south east of I-75 to connect to Marion County's future NW 35 ${ }^{\text {th }}$ Street extension through Magnum Materials Mine.


Figure 4-2: NW 49 ${ }^{\text {th }}$ Street Preferred Typical Section

A Context Classification Assignment Evaluation was performed for NW 49 ${ }^{\text {th }}$ Street and is included as part of the PER. Results of this effort show that NW 49 ${ }^{\text {th }}$ Street should be classified as "C3C-Suburban Commercial". A summary of the primary measurements for the evaluation is shown in Table 4-1. The C3C-Suburban Commercial context classification falls under FDOT Roadway Class 3, per Chapter 14-97, F.A.C. State Highway System Access Control Classification System and Access Management Standards; see Table 4-2. The detailed Context Classification Assignment Evaluation is presented in the PER.

Table 4-1: NW 49 ${ }^{\text {th }}$ Street Context Classification

| Primary Measures | NW 49 ${ }^{\text {th }}$ Street from NW 44 ${ }^{\text {th }}$ Avenue to west of NW $35^{\text {th }}$ Street |
| :---: | :---: |
| Land Use Building Height Building Placement Fronting Uses Location of On-Street Parking Intersection Density Block Perimeter Block Length Proposed Context Classification | Commerce District w/ abutting low/medium residential to the west 1-2 Floors Serving Commercial and Offices $\begin{gathered} \text { Large (> 75') Setbacks } \\ \text { N/A } \\ \text { N/A } \\ 4 \text { Intersections Per Square Mile } \\ 9,744 \text { Feet } \\ 2,335 \text { Feet } \\ \text { Suburban (C3C) } \\ \hline \end{gathered}$ |

Table 4-2: NW 49 ${ }^{\text {th }}$ Street Roadway Access Class

| Roadway Access Class | FDOT Context Classification | Median Type | Connection Spacing (feet) |  | Median Opening Spacing (feet) |  | Minimum Signal Spacing (feet) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | <45mph Posted | $>45 \mathrm{mph}$ Posted | Directional | Full |  |
| 3 | C3C Suburban Commercial | Restrictive | 440 | 660 | 1,320 | 2,640 | 2,640 |

Source: 2019 FDOT Access Management Guidebook

### 4.3.2 Diamond Interchange Build Alternative

The Diamond interchange is a common interchange type characterized by diverge ramps in advance of the interchange and merge ramps beyond the interchange. Both the merge and diverge ramps connect to the grade separated intersecting roadway. Viewed from above, the Diamond interchange resembles a diamond shape. Advantages of this interchange are a smaller footprint and the fact that a wide range of drivers are familiar with this interchange form. Another advantage of this interchange is that longer on and off ramps could be provided to facilitate truck acceleration, deceleration and storage.

This Diamond alternative is a hybrid of a Tight Diamond and Typical Diamond interchange; while the previous (May 2016) IJR considered a Typical Diamond interchange. The smaller footprint of this interchange is advantageous given that the NW $44^{\text {th }}$ Avenue intersection is located only approximately 1,100 feet west of I-75. Therefore, the southbound ramps are designed as a Tight Diamond interchange, which increases the distance to NW $44^{\text {th }}$ Avenue. The northbound ramps are designed as a typical Diamond interchange. A Preliminary Conceptual Plan of the Diamond interchange is provided in Figures 4-3 and 4-4.

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Figure 4-3: Preliminary Concept Diamond


Figure 4-4: Preliminary Concept Diamond

### 4.3.3 Single Point Urban Interchange Build Alternative

A SPUI is a type of Diamond interchange that compresses the movements associated with the ramps to the interstate/major roadway as a single signalized intersection with the interstate/major roadway through lanes accommodated via an underpass or overpass. One potential operational advantage of the single intersection is it allows opposing left turns to proceed simultaneously by compressing the two intersections of a diamond interchange. On the other hand, potential disadvantages include its higher bridge cost, availability of sufficient right of way, and Maintenance of Traffic (MOT) considerations on the interstate. A Preliminary Conceptual Plan of the SPUI interchange is provided in Figures 4-5 and 4-6.

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Figure 4-5: Preliminary Concept SPUI


Figure 4-6: Preliminary Concept SPUI

### 4.3.4 Partial Cloverleaf Interchange Build Alternatives

A Cloverleaf interchange has left turns which are handled by loop ramps and right turns which are handled by slip ramps. Typically, to go left vehicles first continue beyond the intersecting road, then exit right onto a one-way loop ramp and merge onto the intersecting road. Similarly, typically to go right, vehicles diverge prior to the loop ramp and come to an intersection on the intersecting road. Viewed from above the Cloverleaf interchange resembles a four-leaf clover. A full Cloverleaf interchange has loop and slip ramps in all four quadrants whereas a Parclo has at least one quadrant without a loop ramp. Typically loop ramps are implemented where there is a heavy left turn movement, which is accommodated on the directional/free-flow loop ramp.

The large right-of-way footprint required for loop ramps for the westbound to southbound on ramp and southbound to eastbound off ramp (loop ramps on the southwest and northwest quadrants) would potentially impact the operations at the NW $44^{\text {th }}$ Avenue intersection located approximately 1,100 feet to the west of I-75 by creating an undesirably short weave section between the interchange and this intersection. Therefore, loop ramps were only considered for the southeast and northeast quadrants; where sufficient right-of-way is available without conflict. Two Parclo alternatives were developed and evaluated; the Parclo-SE provides a loop ramp for the eastbound to northbound movement and Parclo-NE provides a loop ramp for the northbound to westbound movement. The remaining movements are served by diamond ramps. The southbound on/off ramps reflect a tight diamond design to minimize impacts at NW $44^{\text {th }}$ Avenue. Preliminary Conceptual Plans of the Parclo-SE and Parclo-NE interchanges are provided in Figures 4-7 and 4-8, and Figures 4-9 and 4-10, respectively.

[^5]

Figure 4-7: Preliminary Concept Parclo-SE


Figure 4-8: Preliminary Concept Parclo-SE


Figure 4-9: Preliminary Concept Parclo-NE


Figure 4-10: Preliminary Concept Parclo-NE

### 4.3.5 Diverging Diamond Interchange Build Alternative

The DDI is an alternative to the conventional diamond interchange. The primary difference between a DDI and a conventional diamond interchange is the design of directional crossovers on either side of the interchange. This eliminates the need for left-turning vehicles to cross the paths of approaching through vehicles. By shifting cross street traffic to the left side of the street between the signalized crossover intersections, vehicles on the crossroad making a left turn on to or off of ramps do not conflict with vehicles approaching from other directions. This allows for a simple two-phase operation at the two signalized intersections within the interchange (no left turns), thus improving efficiency.

The DDI alternative for the proposed project consists of an east-west crossover over I-75. Critical design and operational components that are considered when evaluating a DDI include:

## Operational:

- Signal operations favor either cross-street traffic or off-ramps traffic.
- Signal progression; only obtainable in one direction.
- Lane configuration and utilization; use of shared through/left turn lanes may result in blocking of the on-ramps if storage is inadequate between the on-ramp and the crossover leaving the DDI.
- Proximity to adjacent intersections which may create weaving conflicts and queue spillbacks into the DDI. NW $44^{\text {th }}$ Avenue intersection located less than 700 feet to the west of the potential west side crossover intersection.
- Pedestrian paths, inside versus outside the DDI. Facilities on the inside minimize conflicts with left-turning vehicles.


## Design:

- Design speed that affects the reverse curve radii though the intersection crossover; typical range is 25 mph to 35 mph .
- Avoid abrupt curvature and design for a "Natural Path" providing tangents between reverse curves and performing a direct path test to eliminate wrong-way driving and same direction path overlaps. Minimum recommended crossing angle is 30 degrees.
- "Sum of the Parts" that should be considered collectively; crossing angle, length of tangent, setback distance, "eyebrow" design, and pass through test.

A Preliminary Conceptual Plan of the DDI interchange is provided in Figures 4-11 and 4-12.


Figure 4-11: Preliminary Concept DDI


Figure 4-12: Preliminary Concept DDI

### 4.4 Right-of-Way

The proposed project is anticipated to require one business relocation and will impact 26 parcels with a total of 86 acres. Additionally, 13 outdoor advertising signs are anticipated to be impacted. During final design, existing billboards should be preserved where feasible.

The relocation of one business, Barracuda Boat and RV Storage, is anticipated under the preferred alternative. There would be no residential relocations under the preferred alternative. Nearby replacement commercial sites are available. Relocation advisory services and assistance will be provided in accordance with the Uniform Relocation Assistance and Real Property Acquisition Policies Act of 1970, as amended (Uniform Act).

### 4.5 Design Variation

I-75/SR 93 at NW 49 Street in Marion County is a limited access state road facility where a new I-75 interchange at NW 49 Street and an extension from NW 44 Avenue to NW 35 Avenue is planned. The project location is in a C3C - Suburban Commercial environment due to the agricultural and industrial land uses, with nearby commercial and low-density residential land uses.

Although the project strives to meet the standards as set by FDOT, it's not feasible to provide the minimum requirements of the border width due to the impact to the public. Therefore, a design variation is required for border width. The proposed conditions meet standards with the exception of STA $593+80.00$ to STA $636+09.37$ along the I-75 Southbound off-ramp.

## 5 Future Year Traffic

This section summarizes the methodology used to develop the future year traffic volumes and provides a summary of the results. Future year traffic volumes were developed for both the No Build and the Build scenarios for the Opening Year (2025), Interim Year (2035), and Design Year (2045) as specified in the MLOU.

### 5.1 Travel Demand Modeling

The following provides a brief synopsis of the travel demand modeling efforts conducted in support of forecasting future traffic. The refined 2015 CFRPM presented in Section 3 of this document was utilized to develop future traffic volume projections. Consistent with the 2045 CFRPM 6.1 MOCF, 0.97 was used for surface streets and 0.98 , for I-75. Criteria used for refinement of the base year model was carried thru to the 2045 CFRPM provided by the Department, to develop the year 2045 travel demand models for the No Build and Build alternatives.

### 5.2 Future Traffic Development

The CFRPM 2045 PSWADT*MOCF output (AADT) was adjusted by the 2015 validity factors established in Section 3, using the equation: Adjusted 2045 AADT $=(2045$ AADT $-A+2045$ AADT / B) / 2; where (A) is the 2015 volume-count difference and $(B)$ is the 2015 volume/count ratio; resulting in the validity factors (A) and (B). The validity factors, 2015 Adjusted AADTs, No Build and Build 2045 Adjusted AADTs are summarized in Table 5-1. Detailed calculations are provided in Appendix G.

## Table 5-1: CFRPM Adjusted AADTs

| Roadway | Segment | FTO Station | 2015 |  |  |  | 2045 | 2045 No Build |  |  | 2045 Build |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | CFRPM <br> AADT | (A) <br> Vol-Count | (B) Vol/Count | Adjusted AADT | CFRPM <br> MOCF | PSWADT | AADT | Adjusted AADT | PSWADT AADT AADT ${ }^{\text {Adjusted }}$ A |  |  |
| I-75Mainline | N of SR 326 Interchange | 360437 | 55,100 | 7,600 | 1.16 | 47,500 | 0.98 | 84,003 | 82,323 | 72,800 | 83,900 | 82,222 | 72,800 |
|  | $N$ of Proposed Interchange | 360438 | 62,800 | -2,700 | 0.96 | 65,500 | 0.98 | 93,195 | 91,331 | 94,600 | 95,226 | 93,321 | 96,700 |
|  | $N$ of US 27 Interchange | 360438 | 62,800 | -2,700 | 0.96 | 65,500 | 0.98 | 93,195 | 91,331 | 94,600 | 103,773 | 101,698 | 105,200 |
|  | S of US 27 Interchange | 360439 | 71,900 | 2,400 | 1.03 | 69,500 | 0.98 | 119,782 | 117,386 | 114,200 | 124,156 | 121,673 | 118,400 |
| $1-75 \text { at }$ $\text { US } 27$ <br> Interchange | US 27 W of I-75 | 360459 | 28,500 | 2,100 | 1.11 | 26,000 | 0.97 | 56,671 | 54,971 | 51,100 | 54,703 | 53,062 | 49,300 |
|  | US 27 E of $\mathrm{l}-75$ | 360033 | 26,200 | -200 | 0.99 | 26,500 | 0.97 | 56,638 | 54,939 | 55,300 | 55,141 | 53,487 | 53,800 |
|  | I-75 NB Off-Ramp | 362012 | 6,600 | 700 | 1.12 | 5,900 | 0.98 | 16,077 | 15,755 | 14,600 | 14,138 | 13,855 | 12,800 |
|  | 1-75 NB On-Ramp | 362013 | 2,000 | 0 | 1.00 | 2,000 | 0.98 | 2,765 | 2,710 | 2,700 | 3,712 | 3,638 | 3,600 |
|  | I-75 SB Off-Ramp | 362014 | 2,100 | 0 | 1.00 | 2,100 | 0.98 | 2,948 | 2,889 | 2,900 | 4,413 | 4,325 | 4,300 |
|  | I-75 SB On-Ramp | 362015 | 6,700 | 400 | 1.06 | 6,300 | 0.98 | 16,223 | 15,899 | 15,200 | 14,371 | 14,084 | 13,500 |
| US 27 at NW 44 Avenue | NW 44 Avenue N of US 27 | 368029/C-29 | 8,400 | 500 | 1.06 | 7,900 | 0.97 | 16,266 | 15,778 | 15,100 | 12,966 | 12,577 | 12,000 |
|  | NW 44 Avenue S of US 27 | 368029/C-29 |  | 500 | 1.06 |  | 0.97 | 4,572 | 4,435 | 4,100 | 2,969 | 2,880 | 2,500 |
|  | US 27 W of NW 44 Avenue | 360459 | 20,800 | 2,100 | 1.11 | 18,700 | 0.97 | 46,811 | 45,407 | 42,100 | 46,664 | 45,264 | 41,900 |
|  | US 27 E of NW 44 Avenue | 360459 | 27,400 | 2,100 | 1.11 | 24,900 | 0.97 | 53,516 | 51,911 | 48,200 | 51,003 | 49,473 | 45,900 |
| $\begin{aligned} & \text { US } 27 \text { at } \\ & \text { NW } 35 \\ & \text { Avenue } \end{aligned}$ | NW 35 Ave Rd N of US 27 | $367008 / \mathrm{C}-21^{(3]}$ | 6,200 | -3,100 | $0.28{ }^{[4]}$ | 15,700 | 0.97 | 22,224 | 21,557 | 24,700 | 19,041 | 18,470 | 21,600 |
|  | NW 35 Ave Rd S of US 27 | [2] |  |  |  |  |  |  |  |  |  |  |  |
|  | US 27 W of NW 35 Ave Rd | 360033 | 26,200 | -200 | 0.99 | 26,400 | 0.97 | 56,647 | 54,948 | 55,300 | 55,134 | 53,480 | 53,800 |
|  | US 27 E of NW 35 Ave Rd | 360033 | 21,800 | -200 | 0.99 | 22,000 | 0.97 | 45,599 | 44,231 | 44,500 | 46,152 | 44,767 | 45,100 |
| NW 49 Street at NW 44 Avenue | NW 44 Ave N of NW 49 St | 368029/C-29 | 6,200 | 500 | 1.06 | 5,700 | 0.97 | 16,411 | 15,919 | 15,200 | 13,873 | 13,457 | 12,800 |
|  | NW 44 Ave S of NW 49 St | 368029/C-29 | 6,200 | 500 | 1.06 | 5,700 | 0.97 | 14,895 | 14,448 | 13,800 | 10,544 | 10,228 | 9,700 |
|  | NW 49 St W of NW 44 Ave |  |  |  |  |  |  |  |  |  |  |  |  |
|  | NW 49 St E of NW 44 Ave | 368039/C-25 ${ }^{(3)}$ |  | -2,300 | $0.61{ }^{14]}$ |  | 0.97 | 12,720 | 12,338 | 14,600 | 19,786 | 19,192 | 21,500 |
| I-75 at NW 49 Street Interchange | NW 49 Street W of I-75 | 368039/C-25 ${ }^{[3]}$ |  | -2,300 | $0.611^{[4]}$ |  | 0.97 | 12,720 | 12,338 | 14,600 | 19,786 | 19,192 | 21,500 |
|  | NW 49 Street E of I-75 | 368039/C-25 ${ }^{[3]}$ |  | -2,300 | $0.61^{[4]}$ |  | 0.97 | 12,720 | 12,338 | 14,600 | 15,662 | 15,192 | 17,500 |
|  | I-75 NB Off-Ramp | [1] |  | -1,133 | 0.77 |  | 0.98 |  |  |  | 7,642 | 7,489 | 9,200 |
|  | 1-75 NB On-Ramp | [1] |  | -1,133 | 0.77 |  | 0.98 |  |  |  | 3,331 | 3,264 | 4,300 |
|  | I-75 SB Off-Ramp | [1] |  | -1,133 | 0.77 |  | 0.98 |  |  |  | 3,195 | 3,131 | 4,200 |
|  | I-75 SB On-Ramp | [1] |  | -1,133 | 0.77 |  | 0.98 |  |  |  | 7,432 | 7,283 | 8,900 |
| $\mathrm{I}-75 \text { at }$ $\text { SR } 326$ <br> Interchange | SR 326 W of I-75 | MAP A-7 | 2,300 | -4,500 | $0.34{ }^{[4]}$ | 6,700 | 0.97 | 8,220 | 7,973 | 12,500 | 7,971 | 7,732 | 12,200 |
|  | SR 326 E of I-75 | 360465 | $20,500$ | 600 | 1.03 | 19,900 | 0.97 | 40,243 | 39,036 | 38,200 | 39,749 | 38,557 | 37,700 |
|  | I-75 NB Off-Ramp | 362016 | 6,800 | -3,200 | 0.68 | 10,000 | 0.98 | 11,743 | 11,508 | 15,800 | 12,148 | 11,905 | 16,300 |
|  | 1-75 NB On-Ramp | 362017 | 2,400 | -2,100 | $0.53{ }^{[4]}$ | 4,500 | 0.98 | 7,145 | 7,002 | 9,100 | 6,617 | 6,485 | 8,600 |
|  | I-75 SB Off-Ramp | 362018 | 2,400 | -1,700 | 0.59 | 4,000 | 0.98 | 5,957 | 5,838 | 8,800 | 5,087 | 4,985 | 7,600 |
|  | I-75 SB On-Ramp | 362019 | 200 | -3,200 | $0.06{ }^{[4]}$ | 3,400 | 0.98 | 1,201 | 1,177 | 4,400 | 798 | 782 | 4,000 |
|  | I-75 SB Loop Ramp | 362024 | 5,500 | -1,100 | 0.83 | 6,600 | 0.98 | 9,351 | 9,164 | 10,600 | 10,085 | 9,883 | 11,400 |

$36 X X X X$ - Location references an adjacent or comparable station for factors; [1] Average of US 27 \& SR 326 Ramps; [2] No Comparable Road in CFRPM; [3] Reference Station located adjacent to project AOI, see Table 3-1 Adjusted 2045 AADT $=(2045$ AADT - A + 2045 AADT / B) / 2, rounding variances may occur, Adjusted AADTs calculated including A and B calculations, see Appendix G,
[4] Validity Ratio Factor, B, omitted from Adjustment equation, consistent with NCHRP 255

### 5.2.1 Trends Analysis

Historical traffic count growth was evaluated with trends analysis for AADTs from FDOT count sites, using the FDOT Traffic Trends V03a spreadsheet with the 2045 Florida Standard Urban Transportation Model Structure (FSUTMS) CFRPM forecasts for both No Build and Build scenarios.

The Trends Analysis $R^{2}$ results for the scenarios are summarized in Table 5-2. Per the 2019 FDOT Traffic Forecasting Handbook, only growth with an $\mathrm{R}^{2}$ value greater than or equal to $75 \%$ should be considered when determining growth factors with trends. The FDOT Traffic Trends Worksheets are provided in Appendix G.

From the trends analysis, based on the low $\mathrm{R}^{2}$ for Historic FTO AADT Trends, the results are not reliable for establishing a growth rate.

Table 5-2: Trends Analysis $\mathbf{R}^{2}$ Results

| Roadway | Segment | FTO Station | $R^{2}$ <br> No Build | $\begin{gathered} R^{2} \\ \text { Build } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| $1-75$ <br> Mainline | N of SR 326 Interchange | 360437 | 25.95 | 25.95 |
|  | N of NW 49 ${ }^{\text {th }}$ Street Interchange (Build) | 360438 | 60.64 | 62.61 |
|  | N of US 27 Interchange | 360438 | 60.64 | 62.61 |
|  | S of US 27 Interchange | 360439 | 61.21 | 63.80 |
| I-75 at US 27 Interchange | US 27 W of I-75 | 360459 | 39.77 | 39.42 |
|  | US 27 E of I-75 | 360033 | 53.02 | 53.75 |
|  | I-75 NB Off-Ramp | 362012 | 74.77 | 0.30 |
|  | I-75 NB On-Ramp | 362013 | 13.25 | 46.89 |
|  | I-75 SB Off-Ramp | 362014 | 5.12 | 46.44 |
|  | I-75 SB On-Ramp | 362015 | 76.37 | 74.89 |
| US 27 at <br> NW $35^{\text {th }}$ Avenue Road | NW 35 ${ }^{\text {th }}$ Avenue Road N of US 27 | 367008 | 89.16 | 88.03 |
|  | NW 35 ${ }^{\text {th }}$ Avenue Road S of US 27 | 367006 | - | - |
|  | US 27 W of NW $35{ }^{\text {th }}$ Avenue Road | 360033 | 53.02 | 53.75 |
|  | US 27 E of NW $35^{\text {th }}$ Avenue Road | 360033 | 53.02 | 53.75 |
| I-75 at NW 49 ${ }^{\text {th }}$ Street Interchange | NW 49 ${ }^{\text {th }}$ Street W of I-75 | 368039 | 98.48 | 98.40 |
|  | NW 49 ${ }^{\text {th }}$ Street E of I-75 | 368039 | 98.48 | 98.40 |
|  | I-75 NB Off-Ramp | - | - | - |
|  | I-75 NB On-Ramp | - | - | - |
|  | I-75 SB Off-Ramp | - | - | - |
|  | I-75 SB On-Ramp | - | - | - |
| I-75 at <br> SR 326 Interchange | SR 326 W of I-75 | - | - | - |
|  | SR 326 E of I-75 | 360465 | 58.75 | 58.05 |
|  | I-75 NB Off-Ramp | 362016 | 41.56 | 44.49 |
|  | I-75 NB On-Ramp | 362017 | 73.53 | 72.37 |
|  | I-75 SB Off-Ramp | 362018 | 77.97 | 72.53 |
|  | I-75 SB On-Ramp | 362019 | 80.80 | 69.75 |
|  | I-75 SB Loop Ramp | 362024 | 31.30 | 38.52 |

### 5.2.2 Development of Growth Rate

Several scenarios were considered when developing the project growth rates, scenarios included: (1) Trends Analysis based on historic AADTs and 2045 CFRPM Adjusted AADTs, summarized in Table 5-2; (2) calculation based on 2015 CFRPM Adjusted AADTs to 2045 CFRPM Adjusted AADTs, summarized in Table 5-3; (3) calculation based on 2017 Existing AADTs to 2045 CFRPM Adjusted AADTs, also summarized in Table 5-3; and (4) calculation based on Bureau of Economics and Business Research (BEBR) 2017 estimates and 2045 Population Projections, see Table 5-4.

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Table 5-3: CFRPM Growth Rate Summary


I-75 at NW 49th Street Project Development \& Environment Study
Table 5-4: Marion County - Population Growth

| Year | $\mathbf{2 0 1 7}$ | $\mathbf{2 0 4 5}$ | 2017/2045 Growth |
| :---: | ---: | ---: | :---: |
|  | 349,267 |  |  |
| Population | Low | 374,700 | $0.25 \%$ |
|  | Medium | 452,900 | $0.93 \%$ |
|  | High | 545,900 | $1.61 \%$ |

Source: BEBR Florida Population Estimates and Population Projection Studies
Results from the growth rate developments show that:

1) The historic growth from the trends analysis was deemed unreliable for establishing growth rates based on the overall low $R^{2}$ values.
2) 2015 CFRPM Adjusted AADTs to 2045 CFRPM Adjusted AADTs resulted in growth rates ranging from $0.86 \%$ to $3.32 \%$ for No Build and $0.54 \%$ to $2.73 \%$ for Build. The overall average growth rates were 2.12\% for No Build and 2.01\% for Build. The median growth rates were $2.28 \%$ for No Build and $2.14 \%$ for Build.
3) 2017 AADTs to 2045 CFRPM Adjusted AADTs resulted in growth rates ranging from $0.13 \%$ to $4.35 \%$ for No Build and $0.58 \%$ to $3.85 \%$ for Build. The overall average growth rates were $1.80 \%$ for No Build and 1.84\% for Build. The median growth rates were 1.67\% for No Build and 1.65\% for Build.
4) Population growth for Marion County between 2017 and 2045 resulted in growth rates of 0.25\% (Low), 0.93\% (Medium), and 1.61\% (High).

Overall, 2015 CFRPM Adjusted AADTs to 2045 CFRPM Adjusted AADTs growth rates are generally higher when compared to the other growth rate scenarios for the ramp segments and arterials; and are similar to the I-75 mainline. However, Medium and High BEBR population growth projections fall in line with the calculated 2017 AADTs to 2045 CFRPM Adjusted AADTs growth rates for the arterials. Also, as mentioned in Section 3, 2019 FTO volumes reflected a slight increase from 2017 volumes. Therefore, the 2015 to 2045 CFRPM Adjusted AADTs growth rates are recommended for the I-75 Mainline under No Build and Build alternatives; and the 2017 AADTs to 2045 CFRPM Adjusted AADTs annual growth rates along with the 2045 CFRPM Adjusted AADTs, are recommended for No Build and Build alternatives on the ramp segments and arterials. Table 5-5 summarizes the recommended growth rates and 2045 CFRPM Adjusted AADTs. Growth rate data and information are provided in Appendix G.

Table 5-5: Recommended Growth Rates

| Roadway | Segment | $\begin{aligned} & 2017 \text { Existing } \\ & \text { AADT } \end{aligned}$ | 2045 AADT |  | Growth Rate |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | No Build | Build | No Build | Build |  |
| I-75Mainline | N of SR 326 Interchange | 56,500 | 84,200 | 84,200 | 1.43\% | 1.43\% |  |
|  | $N$ of Proposed Interchange | 76,000 | 107,100 | 109,300 | 1.23\% | 1.31\% |  |
|  | $N$ of US 27 Interchange | 76,000 | 107,100 | 118,300 | 1.23\% | 1.59\% |  |
|  | S of US 27 Interchange | 75,000 | 119,200 | 123,300 | 1.67\% | 1.79\% |  |
| 1-75 at | US 27 W of I-75 | 31,100 | 51,100 | 49,300 | 1.79\% | 1.66\% |  |
| US 27 | US 27 E of I-75 | 29,100 | 55,300 | 53,800 | 2.32\% | 2.22\% |  |
| Interchange | 1-75 NB Off-Ramp | 8,100 | 14,600 | 12,800 | 2.13\% | 1.65\% |  |
|  | 1-75 NB On-Ramp | 2,200 | 2,700 | 3,600 | 0.73\% | 1.77\% |  |
|  | I-75 SB Off-Ramp | 2,800 | 2,900 | 4,300 | 0.13\% | 1.54\% |  |
|  | 1-75 SB On-Ramp | 7,500 | 15,200 | 13,500 | 2.55\% | 2.12\% |  |
| US 27 at | NW 44 Avenue N of US 27 | 8,900 | 15,100 | 12,000 | 1.91\% | 1.07\% | [2] A min 0.5\% growth applied to roadways (a) not in the |
| NW 44 | NW 44 Avenue S of US $27{ }^{[2]}$ | 400 | 4,100 | 2,500 | 8.67\% | 6.76\% | CFRPM where no comparable reference station exists; (b) |
| Avenue | US 27 W of NW 44 Avenue | 20,700 | 42,100 | 41,900 | 2.57\% | 2.55\% | or roadways with a resultant growth <0.0\% |
|  | US 27 E of NW 44 Avenue | 31,100 | 48,200 | 45,900 | 1.58\% | 1.40\% |  |
| US 27 at | NW $35^{\text {th }}$ Ave Rd N of US 27 | 7,500 | 24,700 | 21,600 | 4.35\% | 3.85\% | [2] see previous note |
| NW 35 ${ }^{\text {th }}$ | NW $35^{\text {th }}$ Ave RdS of US $27^{[2]}$ | 1,400 | 1,600 | 1,600 | 0.50\% | 0.50\% |  |
| Avenue | US 27 W of NW $35^{\text {th }}$ Ave Rd | 29,100 | 55,300 | 53,800 | 2.32\% | 2.22\% |  |
|  | US 27 E of NW $35^{\text {th }}$ Ave Rd | 25,000 | 44,500 | 45,100 | 2.08\% | 2.13\% |  |
| NW 49 Street at NW 44 Avenue | NW 44 Ave N of NW 49 St | 7,000 | 15,200 | 12,800 | 2.81\% | 2.18\% | [2] see previous note |
|  | NW 44 Ave S of NW 49 St | 7,100 | 13,800 | 9,700 | 2.40\% | 1.12\% | [3] Under Build Condition for NW 49 Street, consistent |
|  | NW 49 St W of NW $44 \mathrm{Ave}^{[2]}$ | 150 | 200 | 200 | 0.50\% | 0.50\% | with ramps, growth is the average of growth rates on US |
|  | NW 49 St E of NW $44 \mathrm{Ave}^{[3]}$ | 7,100 | 14,600 | 21,500 | 2.61\% | 1.85\% | 27 and SR 326 ramps. |
| I-75 at NW 49 ${ }^{\text {th }}$ Street Interchange | NW 49 ${ }^{\text {th }}$ Street W of l-75 ${ }^{[3]}$ |  | 14,600 | 21,500 | 2.61\% | 1.85\% |  |
|  | NW 49 ${ }^{\text {th }}$ Street E of $1-75^{[3]}$ |  | 14,600 | 17,500 | 2.61\% | 1.85\% |  |
|  | I-75 NB Off-Ramp ${ }^{[1]}$ |  |  | 9,200 |  | 1.85\% | [1] average of growth rates on US 27 and SR 326 ramps. |
|  | $1-75$ NB On-Ramp ${ }^{[1]}$ |  |  | 4,300 |  | 1.85\% |  |
|  | $1-75$ SB Off-Ramp ${ }^{[1]}$ |  |  | 4,200 |  | 1.85\% |  |
|  | $1-75$ SB On-Ramp ${ }^{[1]}$ |  |  | 8,900 |  | 1.85\% |  |
| I-75 at SR 326 | SR 326 W of I-75 | 10,300 | 12,500 | 12,200 | 0.69\% | 0.61\% |  |
| Interchange | SR 326 E of I-75 | 23,400 | 38,200 | 37,700 | 1.77\% | 1.72\% |  |
|  | 1-75 NB Off-Ramp | 11,000 | 15,800 | 16,300 | 1.30\% | 1.41\% |  |
|  | 1-75 NB On-Ramp | 3,300 | 9,100 | 8,600 | 3.69\% | 3.48\% |  |
|  | 1-75 SB Off-Ramp | 4,700 | 8,800 | 7,600 | 2.27\% | 1.73\% |  |
|  | I-75 SB On-Ramp | 3,400 | 4,400 | 4,000 | 0.93\% | 0.58\% |  |
|  | $1-75$ SB Loop Ramp | 5,900 | 10,600 | 11,400 | 2.11\% | 2.38\% |  |
| Overall Average $^{[4]}$MainlineRampsSurface Streets ${ }^{[4]}$ |  |  |  |  | 2.02\% | 1.83\% | [4] Average excludes segments reflected with note [2]; roadways where min $0.5 \%$ growth established |
|  |  |  |  |  | 1.44\% | 1.53\% |  |
|  |  |  |  |  | 1.76\% | 1.85\% |  |
|  |  |  |  |  | 2.29\% | 1.89\% |  |

11 AVG OF US 27 \& SR 326 RAMPS
[2] NO COMPARABLE ROAD IN CFRPM, MIN $0.5 \%$ GROWTH APPLIED TO $<0.0 \%$ GROWTH OR TO ROADWAYS NOT IN CFRPM
[3] Growth for NW 49 Street under Build Condition reflects average of adjacent interchange, consistent with ramps; not the 2017/2045 growth.
[4] Excludes segments reflected with note [2]

### 5.3 Future Traffic Volumes

Roadway segment 2025 and 2035 AADTs were developed by applying the recommended growth rates to the 2017 AADTs. These AADTs are the basis for both the Design Directional Hour Volumes (DDHV)s and intersection turning movement volumes presented in this section.

### 5.3.1 Future Year Annual Average Daily Traffic

The development of future year AADTs was based on the methodology described previously in this section. The balanced No Build and Build AADTs are provided in Tables 5-6 and 5-7.

Table 5-6: No Build AADT

| Roadway | Segment | AADT |  |  | D |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2025 | 2035 | 2045 |  |
| I-75 <br> Mainline | N of SR 326 Interchange | 70,900 | 81,600 | 94,200 | 0.543 |
|  | N of Proposed Interchange | 83,800 | 94,800 | 107,100 | 0.543 |
|  | N of US 27 Interchange | 83,800 | 94,800 | 107,100 | 0.543 |
|  | S of US 27 Interchange | 97,500 | 113,000 | 131,300 | 0.543 |
| I-75 at <br> US 27 Interchange | US 27 W of I-75 | 35,800 | 42,800 | 51,100 | 0.625 |
|  | US 27 E of I-75 | 35,000 | 44,000 | 55,300 | 0.617 |
|  | I-75 NB Off-Ramp | 9,600 | 11,800 | 14,600 | 1.000 |
|  | I-75 NB On-Ramp | 2,300 | 2,500 | 2,700 | 1.000 |
|  | I-75 SB Off-Ramp | 2,800 | 2,900 | 2,900 | 1.000 |
|  | I-75 SB On-Ramp | 9,200 | 11,800 | 15,200 | 1.000 |
| US 27 at NW 44 Avenue | NW 44 Avenue N of US 27 | 10,400 | 12,500 | 15,100 | 0.525 |
|  | NW 44 Avenue S of US 27 | 800 | 1,800 | 4,100 | 0.632 |
|  | US 27 W of NW 44 Avenue | 25,400 | 32,700 | 42,100 | 0.587 |
|  | US 27 E of NW 44 Avenue | 35,200 | 41,200 | 48,200 | 0.597 |
| US 27 at NW 35 Ave Rd | NW 35 Ave Rd N of US 27 | 10,500 | 16,100 | 24,700 | 0.535 |
|  | NW 35 Ave Rd S of US 27 | 1,500 | 1,500 | 1,600 | 0.650 |
|  | US 27 W of NW 35 Ave Rd | 35,000 | 44,000 | 55,300 | 0.617 |
|  | US 27 E of NW 35 Ave Rd | 29,500 | 36,200 | 44,500 | 0.641 |
| NW 49 Street at NW 44 Avenue | NW 44 Avenue N of NW 49 Street | 8,700 | 11,500 | 15,200 | 0.650 |
|  | NW 44 Avenue S of NW 49 Street | 8,600 | 10,900 | 13,800 | 0.539 |
|  | NW 49 Street W of NW 44 Avenue | 200 | 200 | 200 | 0.636 |
|  | NW 49 Street E of NW 44 Avenue | 8,700 | 11,300 | 14,600 | 0.630 |
| I-75 at <br> NW 49 Street Interchange | NW 49 Street W of I-75 | 8,700 | 11,300 | 14,600 | 0.635 |
|  | NW 49 Street E of I-75 | 8,700 | 11,300 | 14,600 | 0.635 |
|  | I-75 NB Off-Ramp |  |  |  |  |
|  | I-75 NB On-Ramp |  |  |  |  |
|  | I-75 SB Off-Ramp |  |  |  |  |
|  | I-75 SB On-Ramp |  |  |  |  |
| I-75 at <br> SR 326 Interchange | SR 326 W of I-75 | 10,900 | 11,700 | 12,500 | 0.621 |
|  | SR 326 E of I-75 | 26,900 | 32,100 | 38,200 | 0.548 |
|  | I-75 NB Off-Ramp | 12,200 | 13,900 | 15,800 | 1.000 |
|  | I-75 NB On-Ramp | 4,400 | 6,300 | 9,100 | 1.000 |
|  | I-75 SB Off-Ramp | 5,600 | 7,000 | 8,800 | 1.000 |
|  | I-75 SB On-Ramp | 3,700 | 4,000 | 4,400 | 1.000 |
|  | I-75 SB Loop Ramp | 7,000 | 8,600 | 10,600 | 1.000 |
| New segment |  |  |  |  |  |

Table 5-7: Build AADT

| Roadway | Segment |  |  |  | AADT |
| :---: | :--- | ---: | ---: | ---: | ---: |
|  |  | $\mathbf{2 0 2 5}$ | $\mathbf{2 0 3 5}$ | $\mathbf{2 0 4 5}$ |  |
| I-75 | N of SR 326 Interchange | 71,000 | 81,500 | 93,800 | 0.543 |
|  | N of Proposed Interchange | 84,300 | 96,000 | 109,300 | 0.543 |
|  | N of US 27 Interchange | 91,000 | 104,000 | 118,900 | 0.543 |
|  | S of US 27 Interchange | 103,400 | 119,100 | 137,300 | 0.543 |
| I-75 at | US 27 W of I-75 27 Interchange | US 27 E of I-75 | 35,500 | 41,800 | 49,300 |

New segment; ${ }^{[1]}$ AVG OF US 27 E of I-75\& SR 326 E of I-75
Build volumes at the interchange ramps adjacent to proposed NW 49 ${ }^{\text {th }}$ Street interchange reflect an increase, compared to No Build. Based on CFRPM select link runs, the predominant pattern to/from US 27 east of the interchange uses I-75 to access NW $44^{\text {th }}$ Avenue, north of NW 49 ${ }^{\text {th }}$ Street to/from residential areas south of SR 326. To/from SR 326 east of the interchange uses I-75 to access NW 44 ${ }^{\text {th }}$ Avenue south of NW 49 ${ }^{\text {th }}$ Street; west of the interchange, SR 326 vehicular traffic uses I-75 to access the vicinity of Ocala 489. The corresponding CFRPM plots are provided in Appendix G.

### 5.3.2 Design Directional Hour Volumes

The DDHVs for opening year (2025), interim (2035) and design (2045) year were developed using the standard equation: AADT $\times \mathrm{K}(0.09) \times \mathrm{D}$. The No Build and Build DDHVs, with corresponding $\%$ T are provided in Tables 5-8 and 5-9, respectively. The I-75 mainline DDHVs were then balanced with AM and PM peak hour ramp volumes (presented in Section 4.3.3) for use in the operational analysis in Section 5. Schematics of the balanced freeway volumes are provided on Figures 5-1 thru 5-4; volume balancing worksheets provided in Appendix H.

## Table 5-8: No Build DDHV

| Roadway | Segment | Tpeak | DDHV |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2025 | 2035 | 2045 |
| I-75 <br> Mainline | N of SR 326 Interchange | 0.10 | 3,460 | 3,990 | 4,600 |
|  | N of Proposed Interchange | 0.12 | 4,100 | 4,630 | 5,230 |
|  | N of US 27 Interchange | 0.12 | 4,100 | 4,630 | 5,230 |
|  | S of US 27 Interchange | 0.11 | 4,760 | 5,520 | 6,420 |
| I-75 at <br> US 27 Interchange | US 27 W of I-75 | 0.06 | 2,010 | 2,410 | 2,870 |
|  | US 27 E of I-75 | 0.06 | 1,940 | 2,440 | 3,070 |
|  | I-75 NB Off-Ramp | 0.14 | 860 | 1,060 | 1,310 |
|  | I-75 NB On-Ramp | 0.06 | 210 | 230 | 240 |
|  | I-75 SB Off-Ramp | 0.06 | 250 | 260 | 260 |
|  | I-75 SB On-Ramp | 0.14 | 830 | 1,060 | 1,370 |
| US 27 at NW 44 Avenue | NW 44 Avenue N of US 27 | 0.02 | 490 | 590 | 710 |
|  | NW 44 Avenue S of US 27 | 0.02 | 50 | 100 | 230 |
|  | US 27 W of NW 44 Avenue | 0.06 | 1,340 | 1,730 | 2,220 |
|  | US 27 E of NW 44 Avenue | 0.06 | 1,890 | 2,210 | 2,590 |
| US 27 at NW 35 Ave Rd | NW 35 Ave Rd N of US 27 | 0.10 | 510 | 780 | 1,190 |
|  | NW 35 Ave Rd S of US 27 | 0.10 | 90 | 90 | 90 |
|  | US 27 W of NW 35 Ave Rd | 0.06 | 1,940 | 2,440 | 3,070 |
|  | US 27 E of NW 35 Ave Rd | 0.06 | 1,700 | 2,090 | 2,570 |
| NW 49 Street at NW 44 Avenue | NW 44 Ave N of NW 49 Street | 0.10 | 510 | 670 | 890 |
|  | NW 44 Ave S of NW 49 Street | 0.10 | 420 | 530 | 670 |
|  | NW 49 St W of NW 44 Avenue | 0.12 | 10 | 10 | 10 |
|  | NW 49 St E of NW 44 Avenue | 0.12 | 490 | 640 | 830 |
| I-75 at NW 49 Street Interchange | NW 49 Street W of I-75 | 0.12 | 500 | 650 | 830 |
|  | NW 49 Street E of I-75 | 0.12 | 500 | 650 | 830 |
|  | I-75 NB Off-Ramp <br> I-75 NB On-Ramp <br> I-75 SB Off-Ramp <br> I-75 SB On-Ramp |  |  |  |  |
| I-75 at <br> SR 326 Interchange | SR 326 W of I-75 | 0.17 | 610 | 650 | 700 |
|  | SR 326 E of I-75 | 0.17 | 1,330 | 1,580 | 1,880 |
|  | I-75 NB Off-Ramp | 0.23 | 1,100 | 1,250 | 1,420 |
|  | I-75 NB On-Ramp | 0.23 | 400 | 570 | 820 |
|  | I-75 SB Off-Ramp | 0.23 | 500 | 630 | 790 |
|  | I-75 SB On-Ramp | 0.23 | 330 | 360 | 400 |
|  | I-75 SB Loop Ramp | 0.23 | 630 | 770 | 950 |
| New segment |  |  |  |  |  |

Table 5-9: Build DDHV

| Roadway | Segment | Tpeak | DDHV |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2025 | 2035 | 2045 |
| I-75 <br> Mainline | N of SR 326 Interchange | 0.10 | 3,470 | 3,980 | 4,580 |
|  | $N$ of Proposed Interchange | 0.12 | 4,120 | 4,690 | 5,340 |
|  | N of US 27 Interchange | 0.12 | 4,450 | 5,080 | 5,810 |
|  | S of US 27 Interchange | 0.11 | 5,050 | 5,820 | 6,710 |
| 1-75 at <br> US 27 Interchange | US 27 W of I-75 | 0.06 | 2,000 | 2,350 | 2,770 |
|  | US 27 E of I-75 | 0.06 | 1,930 | 2,400 | 2,990 |
|  | I-75 NB Off-Ramp | 0.14 | 830 | 980 | 1,150 |
|  | I-75 NB On-Ramp | 0.06 | 230 | 270 | 320 |
|  | I-75 SB Off-Ramp | 0.06 | 290 | 330 | 390 |
|  | I-75 SB On-Ramp | 0.14 | 800 | 980 | 1,220 |
| US 27 at NW 44 Avenue | NW 44 Avenue N of US 27 | 0.02 | 460 | 510 | 570 |
|  | NW 44 Avenue S of US 27 | 0.02 | 40 | 70 | 140 |
|  | US 27 W of NW 44 Avenue | 0.06 | 1,340 | 1,720 | 2,210 |
|  | US 27 E of NW 44 Avenue | 0.06 | 1,870 | 2,140 | 2,470 |
| US 27 at NW 35 Ave Rd | NW 35 Ave Rd N of US 27 | 0.10 | 490 | 710 | 1,040 |
|  | NW 35 Ave Rd S of US 27 | 0.10 | 90 | 90 | 90 |
|  | US 27 W of NW 35 Ave Rd | 0.06 | 1,930 | 2,400 | 2,990 |
|  | US 27 E of NW 35 Ave Rd | 0.06 | 1,710 | 2,110 | 2,600 |
| NW 49 Street <br> at NW 44 <br> Avenue | NW 44 Ave N of NW 49 Street | 0.10 | 490 | 600 | 750 |
|  | NW 44 Ave S of NW 49 Street | 0.10 | 380 | 420 | 470 |
|  | NW 49 St W of NW 44 Avenue | 0.12 | 10 | 10 | 10 |
|  | NW 49 St E of NW 44 Avenue | 0.12 | 840 | 1,010 | 1,220 |
| I-75 at <br> NW 49 Street Interchange | NW 49 Street W of I-75 | 0.12 | 850 | 1,020 | 1,230 |
|  | NW 49 Street E of I-75 | 0.12 | 630 | 770 | 920 |
|  | I-75 NB Off-Ramp | 0.12 | 580 | 690 | 830 |
|  | I-75 NB On-Ramp | 0.12 | 270 | 320 | 390 |
|  | I-75 SB Off-Ramp | 0.12 | 260 | 320 | 380 |
|  | I-75 SB On-Ramp | 0.12 | 560 | 670 | 800 |
| I-75 at <br> SR 326 Interchange | SR 326 W of I-75 | 0.17 | 600 | 640 | 680 |
|  | SR 326 E of I-75 | 0.17 | 1,320 | 1,570 | 1,860 |
|  | I-75 NB Off-Ramp | 0.23 | 1,110 | 1,280 | 1,470 |
|  | I-75 NB On-Ramp | 0.23 | 390 | 550 | 770 |
|  | I-75 SB Off-Ramp | 0.23 | 490 | 580 | 680 |
|  | I-75 SB On-Ramp | 0.23 | 320 | 340 | 360 |
|  | I-75 SB Loop Ramp | 0.23 | 640 | 810 | 1,030 |

New segment

Figure 5-1: No Build Mainline Balanced Volumes AM Peak Hour


Figure 5-2: No Build Mainline Balanced Volumes PM Peak Hour


Figure 5-3: Build Mainline Balanced Volumes AM Peak Hour

| Build AM Pe |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Distance (ft) |  | 1,500 | 3,168 | 1,500 |  |  |  |  |  | 1,500 | 380 | 1500 | 1,815 | 1,500 |  |
|  | Accel/Decel Lanes (ft) |  | 800 |  | 616 |  |  |  |  |  | 1,073 |  | 1500 |  | 268 |  |
|  | Segment Type | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic |
|  | Truck\% | 11 | 14 | 11 | 6 | 12 | 12 | 12 | 12 | 12 | 23 | 12 | 23 | 12 | 23 | 10 |
|  |  |  |  | $x \geqslant$ |  |  |  |  | $\ldots$ |  |  | $4$ |  | ${ }^{\text {Loop }}$ |  |  |
|  |  |  |  | $\longleftarrow$ |  |  |  | $\leftarrow$ |  |  |  |  |  |  |  |  |
|  |  |  |  | $\stackrel{\square}{\leftarrow}$ |  |  |  | $\stackrel{\square}{4}$ |  |  |  |  |  |  |  |  |
|  | 2045 | 5,825 | 1,092 | 4,733 | 306 | 5,039 | 883 | 4,156 | 351 | 4,507 | 307 | 4,200 | 959 | 3,241 | 442 | 3,683 |
|  | 2035 | 5,045 | 896 | 4,149 | 244 | 4,393 | 736 | 3,657 | 292 | 3,949 | 249 | 3,700 | 645 | 3,055 | 327 | 3,382 |
|  | 2025 | 4,318 | 677 | 3,641 | 193 | 3,834 | 615 | 3,219 | 244 | 3,463 | 183 | 3,280 | 412 | 2,868 | 211 | 3,079 |
|  | Interchange | US 27 |  |  |  | NW 49 Street |  |  |  |  | SR 326 |  |  |  |  |  |
|  | 2025 | 4,822 | 651 | 4,171 | 202 | 4,373 | 519 | 3,854 | 288 | 4,142 | 716 |  |  | 342 | 3,7 |  |
|  | 2035 | 5,543 | 832 | 4,711 | 263 | 4,974 | 622 | 4,352 | 346 | 4,698 | 961 |  |  | 501 | 4,2 |  |
|  | 2045 | 6,501 | 1,043 | 5,458 | 335 | 5,793 | 746 | 5.047 | 415 | 5.462 | 1,250 |  |  | 726 | 4,9 |  |
|  |  |  |  | $\xrightarrow{\square}$ |  |  |  | $\xrightarrow{\square}$ |  |  |  | $\cdots$ | $\rightarrow$ |  |  |  |
|  |  |  |  | $\xrightarrow{\longrightarrow}$ |  |  |  | $\longrightarrow$ |  |  |  | $\cdots$ | $\cdots$ |  |  |  |
|  |  |  |  | $N \text { 有 }$ | $\cdots$ |  |  | $\uparrow$ |  |  |  |  | $8$ |  | - |  |
|  | Truck\% | 11 | 14 | 11 | 6 | 12 | 12 | 12 | 12 | 12 | 23 |  |  | 23 | 10 |  |
|  | Segment Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge |  |  | Merge | Bas |  |
|  | Distance ( t ) |  | 1,500 | 3,029 | 1,500 |  |  |  |  |  | 1,500 |  |  | 1,500 |  |  |
|  | Accel/Decel Lanes ( t ) |  | 671 |  | 847 |  |  |  |  |  | 671 |  |  | 941 |  |  |

Figure 5-4: Build Mainline Balanced Volumes PM Peak Hour

| Build PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Distance ( t ) |  | 1,500 | 3,168 | 1,500 |  |  |  |  |  | 1,500 | 380 | 1500 | 1,815 | 1,500 |  |
|  | Accel/Decel Lanes (ft) |  | 800 |  | 616 |  |  |  |  |  | 1,073 |  | 1500 |  | 268 |  |
|  | Segment Type | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic |
|  | Truck\% | 11 | 14 | 11 | 6 | 12 | 12 | 12 | 12 | 12 | ${ }^{23}$ | 12 | 23 | 12 | ${ }^{23}$ | 10 |
|  |  |  |  |  |  |  |  |  | … |  |  | $4$ |  |  |  |  |
|  |  |  |  | $\longleftarrow$ |  |  |  | $\longleftarrow$ |  |  |  | $\leftarrow$ |  |  |  |  |
|  |  |  |  | - |  |  |  | $\stackrel{\square}{\square}$ |  |  |  |  |  |  |  |  |
|  | 2045 | 6,626 | 1,175 | 5,451 | 330 | 5,781 | 746 | 5,035 | 415 | 5,450 | 299 | 5,151 | 967 | 4,184 | 506 | 4,690 |
|  | 2035 | 5,691 | 933 | 4,758 | 249 | 5,007 | 622 | 4,385 | 346 | 4,731 | 235 | 4,496 | 697 | 3,799 | 419 | 4,218 |
|  | 2025 | 4,882 | 720 | 4,162 | 198 | 4,360 | 519 | 3,841 | 288 | 4,129 | 179 | 3,950 | 503 | 3,447 | 346 | 3,793 |
|  | Interchange | us 27 |  |  |  | NW 49 Street |  |  |  |  | SR 326 |  |  |  |  |  |
|  |  | 4,304 | 675 | 3,629 | 224 | 3,853 | 615 | 3,238 | 244 | 3,482 | 781 | 2,701 <br> 2,931 <br> 3,160 |  | 260 | $\begin{aligned} & 2,961 \\ & 3,376 \\ & 3,867 \end{aligned}$ |  |
|  |  | 4,995 | 868 | 4,127 | 346 | 4,409 | 736 | 3,673 | 292 | 3,965 | 1,034 |  |  | 445 |  |  |
|  |  | 5,796 | 1,110 | 4,686 | 346 | 5,032 | 883 | 4,149 | 351 | 4,500 | 1,340 |  |  | 707 |  |  |
|  |  |  |  | $\longrightarrow$ |  |  |  | $\longrightarrow$ |  |  |  |  |  |  |  |  |
|  |  |  |  | $\longrightarrow$ |  |  |  | $\longrightarrow$ |  |  |  |  |  |  |  |  |
|  |  |  |  | $N \text {, }$ | $\square$ |  |  | $\therefore \text { g }$ | - |  |  | $N$ | 夕 | $\square$ | -Z |  |
|  | Truck\% | 11 | 14 | 11 | 6 | 12 | 12 | 12 | 12 | 12 | 23 |  |  | 23 | 10 |  |
|  | Segment Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge |  |  | Merge | Bas |  |
|  | Distance (ft) |  | 1,500 | 3,029 | 1,500 |  |  |  |  |  | 1,500 |  |  | 1,500 |  |  |
|  | Accel/Decel Lanes (ft) |  | 671 |  | 847 |  |  |  |  |  | 671 |  |  | 941 |  |  |

### 5.3.3 Peak Hour Intersection Volumes

The development of future year intersection turning movement estimates is consistent with the procedures outlined in the FDOT Project Traffic Forecasting Handbook, 2019. The future intersection volumes were developed from the existing (2017) turning movement percentage breakdown and corresponding future AADT, K and D factors, using TMTool worksheets. The proposed NW 49 ${ }^{\text {th }}$ Street interchange volumes were developed based on the manual method; also, as outlined in the handbook and checked for reasonableness against the CFRPM Select Link Runs. The resultant intersection volumes were smoothed and balanced where necessary. Years 2025, 2035 and 2045 intersection turning movement volumes for AM and PM peak hours are provided on Figure 5-5 thru Figure 5-14. Detailed intersection movement volume breakdown and TMTool worksheets are provided in Appendix H.

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Figure 5-5: No Build Intersection \& Interchange Balanced Volumes (2025)


Figure 5-6: No Build Intersection \& Interchange Balanced Volumes (2035)


Figure 5-7: No Build Intersection \& Interchange Balanced Volumes (2045)


Figure 5-8: Build Diamond Intersection \& Interchange Balanced Volumes (2025)


Figure 5-9: Build Diamond Intersection \& Interchange Balanced Volumes (2035)


Figure 5-10: Build Diamond Intersection \& Interchange Balanced Volumes (2045)


Figure 5-11: Build SPUI Intersection \& Interchange Balanced Volumes (2025/35/45)


Figure 5-12: Build Parclo-SE Intersection \& Interchange Balanced Volumes (2025/35/45)


Figure 5-13: Build Parclo-NE Intersection \& Interchange Balanced Volumes (2025/35/45)


Figure 5-14: DDI Alternative Intersection \& Interchange Balanced Volumes (2025/35/45)

## 6 Operational Analysis

An operational analysis was performed to compare the No Build and Build alternatives for analysis years 2025, 2035 and 2045. Per the approved MLOU (see Appendix B), the analysis was performed for the peak hours as determined under existing conditions, using the methodologies documented in the HCM 2010 as applied using HCS 6.8, Synchro 10 and Vissim 2020.00-07. As previously mentioned, HCM 2000 was used under certain phasing and lane configuration conditions that are not recognized by HCM 2010 analysis methodologies. Per the FDOT 2014 Traffic Analysis Handbook, for future traffic a PHF of 0.95 was used for freeway facilities/urban arterials and 0.92 for other facilities. Clearance intervals used for each Build alternative analysis were calculated based on the concept designs, provided in Section 4. Detailed clearance interval calculation worksheets are provided in Appendix I.

The operational analysis provides a performance evaluation for each individual element within the system (for example freeway segments, freeway ramp junctions, crossroad ramp terminals and other crossroad intersections). The HCS, Synchro and Vissim worksheets and reports for the No Build and Build alternatives are provided in Appendix I.

### 6.1 No Build Analyses

This section presents the segment, merge/diverge and intersection analyses under No Build conditions. The No Build lane configuration and traffic control is illustrated in Figure 6-1.

Figures 6-2 thru 6-7 present the segmented breakdown of the I-75 mainline and interchange ramps under No Build; along with the summarized results for the 2025, 2035 and 2045 segment and merge/diverge analysis. The I-75 study segments were projected to meet the LOS D target in the No Build Condition for year 2025. For year 2035, the mainline segment south of US 27 was projected to operate at LOS E in the northbound direction during the AM peak hour and southbound direction during the PM peak hour. For year 2045 during the AM peak hour, northbound I-75 south of US 27 including the off-ramp diverge operates at LOS F and north of US 27 from the on-ramp merge to the off-ramp diverge to SR 326, operates at LOS E; southbound I-75 south of US 27 operates at LOS E beginning at the on-ramp merge. During the PM peak hour northbound I-75 south of US 27 operates at LOS E; southbound, north of US 27 from the on-ramp merge to the off-ramp diverge to US 27 , operates at LOS E and south of US 27 operates at LOS F beginning at the on-ramp merge. All other mainline segments are projected to meet the LOS D target. The merge/diverge locations projected to not meet the LOS D target
in 2045 are the US 27 ramps to/from the south during both the AM and PM peak hours; all other merge/diverge locations are projected to meet the LOS D target. The mainline/ramp schematics and HCS worksheets are provided in Appendix $I$.

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Figure 6-1: No Build Lane Configuration

Figure 6-2: No Build 2025 AM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-3: No Build 2025 PM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-4: No Build 2035 AM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-5: No Build 2035 PM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-6: No Build 2045 AM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-7: No Build 2045 PM I-75 Segment \& Merge/Diverge Analysis Summary


Table 6-1 summarizes the Synchro analysis results for the AM and PM peak hours, including intersection approach, overall intersection delay and corresponding LOS. In year 2025, during the AM peak hour, the LOS D target is met for overall intersection at all locations; however, several cross-street approaches on US 27 along with the northbound approach of the SR 326 off-ramp terminus are projected to fail. During the PM peak hour, in addition to cross-street approaches, the US 27 at NW 35th Avenue Road and the SR 326 northbound off-ramp terminus intersections operate at LOS E. During the AM and PM peak hours in year 2035, the same intersections of US 27 at NW 35th Avenue Road and the SR 326 northbound off-ramp terminus fail. In 2045, during the AM and PM peak hours, the only signalized intersection not projected to fail is the I-75 northbound ramps at US 27; however, the northbound off-ramp approach fails. Synchro outputs are provided in Appendix I.

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Table 6-1: No Build Intersection Delay and LOS

${ }^{1}$ Delay in sec/veh; ${ }^{2}$ LOS results based on HCM 2000 methodology.

### 6.2 Build Analyses

An FDOT ICE Stage 1 Screening was performed for the intersections along NW 49 ${ }^{\text {th }}$ Street at: NW $44^{\text {th }}$ Avenue, I-75 southbound ramp terminal and I-75 northbound ramp terminal. The screening is based on the FDOT CAP-X analysis rankings; worksheets require intersection lane geometry, peak hour volumes and \%trucks. The ranking results become input data for the ICE Stage 1 Screening Form along with basic roadway characteristics, environmental data, multimodal use(s), and roadway context classifications. This section presents the CAP-X analysis and ranking results by intersection type.

For the intersection of NW $49^{\text {th }}$ Street at NW $44^{\text {th }}$ Avenue, the ranking results for AM and PM peak hours along with average of AM/PM rank, are summarized in Table 6-2. Five intersection types had average AM/PM V/Cs less than 0.60. In ascending order, they include Displaced Left Turn Full, Partial Displaced Left Turn N-S, Quadrant Roadway N-W, Traffic Signal and Partial Displaced Left Turn E-W. Due to an AM peak hour V/C of 0.87 and right-of-way requirements, a roundabout was not considered in more detail for this location.

Table 6-2: Peak Hour VIC Rank at NW 44 ${ }^{\text {th }}$ Avenue at NW 49 ${ }^{\text {th }}$ Avenue

| Type of Intersection | AM PK |  | PM PK |  | AVERAGE |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | Ranking | V/C | Ranking | V/C | Ranking |
| Displaced Left Turn FULL | 0.55 | 4 | 0.45 | 1 | 0.50 | 1 |
| Partial Displaced Left Turn N-S | 0.44 | 1 | 0.58 | 3 | 0.51 | 2 |
| Quadrant Roadway N-W | 0.56 | 5 | 0.55 | 2 | 0.56 | 3 |
| Traffic Signal | 0.51 | 2 | 0.66 | 6 | 0.59 | 4 |
| Partial Displaced Left Turn E-W | 0.55 | 3 | 0.63 | 4 | 0.59 | 5 |
| Quadrant Roadway N-E | 0.79 | 7 | 0.69 | 7 | 0.74 | 6 |
| Quadrant Roadway S-E | 0.79 | 8 | 0.71 | 8 | 0.75 | 7 |
| 2 X 2 | 0.87 | 10 | 0.64 | 5 | 0.76 | 8 |
| Quadrant Roadway S-W | 0.84 | 9 | 0.74 | 9 | 0.79 | 9 |
| Signalized Restricted Crossing U-Turn E-W | 0.76 | 6 | 0.85 | 11 | 0.81 | 10 |
| Median U-Turn E-W | 0.88 | 11 | 0.75 | 10 | 0.82 | 11 |

For NW 49 ${ }^{\text {th }}$ Street at the I-75 ramp terminal intersections, the results for AM and PM peak hours along with average of AM/PM, are summarized in Table 6-3 for the southbound ramps and Table 6-4 for northbound. Traffic Signal was ranked \#1 for both ramp locations. A $2 \times 2$ roundabout ranked \#2 for the southbound ramps. For the northbound ramps, no other intersection type had an average AM/PM V/C less than 0.75 .

Table 6-3: Peak Hour VIC Rank at Southbound Ramp Terminal at NW 49 ${ }^{\text {th }}$ Street

| Type of Intersection | AM PK |  | PM PK |  | AVERAGE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | Ranking | V/C | Ranking | V/C | Ranking |
| Traffic Signal | 0.66 | 1 | 0.60 | 1 | 0.63 | 1 |
| $2 \times 2$ | 0.68 | 2 | 0.64 | 2 | 0.66 | 2 |
| 1NS X 2EW | 0.81 | 3 | 0.90 | 3 | 0.86 | 3 |
| 2NS X 1EW | 1.27 | 4 | 1.21 | 4 | 1.24 | 4 |
| Unsignalized Restricted Crossing U-Turn | 1.47 | 5 | 1.71 | 5 | 1.59 | 5 |
|  | V/C thresholds |  | < 0.75 | 0.75-0.88 | 0.88-1.00 | $\geq 1.00$ |

Table 6-4: Peak Hour VIC Rank at Northbound Ramp Terminal at NW 49 ${ }^{\text {th }}$ Street

| Type of Intersection | AM PK |  | PM PK |  | AVERAGE |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | Ranking | V/C | Ranking | V/C | Ranking |
| Traffic Signal | 0.52 | 1 | 0.51 | 1 | 0.52 | 1 |
| $\mathbf{2 X X}$ | 0.70 | 2 | 0.90 | 2 | 0.80 | 2 |
| 2NS X 1EW | 1.30 | 4 | 1.09 | 3 | 1.20 | 3 |
| 1NS X 2EW | 1.06 | 3 | 1.36 | 4 | 1.21 | 4 |
| Unsignalized Restricted Crossing U-Turn | 1.60 | 5 | 2.35 | 5 | 1.98 | 5 |

Based on right of way limitations, intersection volumes, and potential cost, a typical signalized intersection appears to be the appropriate control type for both northbound and southbound ramps. The CAP-X worksheet results, ICE Stage 1 Screening Forms, and supporting documentation are provided in Appendix $\mathbf{J}$.

The lane configuration and traffic control for the Diamond and AOI intersections are presented in Figure 6-8. The AOI intersection geometry is maintained for all build alternatives. The SPUI and Parclo-SE Build alternatives are illustrated in Figure 6-9 and the ParClo-NE and DDI are illustrated on Figure 6-10.

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Figure 6-10: Build Parclo-NE \& DDI Lane Configuration

### 6.2.1 Segment and Merge/Diverge Analysis

Figures 6-11 thru 6-16 present the segmented breakdown of the I-75 mainline and interchange ramps under all five Build alternatives; along with the summarized results for the 2025, 2035 and 2045 segment and merge/diverge analysis. The I-75 study segments were projected to meet the LOS D target in the Build Condition for year 2025. In year 2035, the northbound segment south of US 27 operates at LOS E during the AM peak hour. The southbound merge and mainline segment south of US 27 operates at LOS E during the PM peak hour.

In year 2045, under all five Build alternatives, most mainline segments and merge/diverge segments south of SR 326 do not meet the LOS D target during either the AM peak hour or PM peak hour. In general, the northbound segments do not meet the LOS D target during the AM peak hour and the southbound segments do not meet the LOS D target during the PM peak hour. The following summarizes the analysis segments of the NW 49 ${ }^{\text {th }}$ Street interchange per alternative that do not meet the LOS D target in 2045; HCS worksheets are provided in

## Appendix $I$.

- Diamond and DDI alternatives
o AM Peak Hour: Northbound diverge, northbound merge, and northbound basic segments (north and south of NW 49 ${ }^{\text {th }}$ Street)
o PM Peak Hour: northbound merge, southbound merge, and southbound basic segments (north and south of NW 49th Street)
- SPUI
o AM Peak Hour: Northbound diverge and northbound basic segments (north and south of NW 49 ${ }^{\text {th }}$ Street)
o PM Peak Hour: Southbound merge and southbound basic segments (north and south of NW 49 ${ }^{\text {th }}$ Street)
- ParClo SE
o AM Peak Hour: Northbound diverge and three (3) northbound basic segments
o PM Peak Hour: Southbound basic segments north and south of NW $49^{\text {th }}$ Street
- ParClo NE
o AM Peak Hour: Northbound diverge and three (3) northbound basic segments
o PM Peak Hour: Southbound basic segments north and south of NW 49 ${ }^{\text {th }}$ Street

Figure 6-11: Build 2025 (AM) I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-12: Build 2025 (PM) I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-13: Build 2035 (AM) I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-14: Build 2035 (PM) I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-15: Build 2045 (AM) I-75 Segment \& Merge/Diverge Analysis Summary


Figure 6-16: Build 2045 (PM) I-75 Segment \& Merge/Diverge Analysis Summary


### 6.2.2 Year of Failure Analysis

As shown in the No Build segment and merge/diverge analysis results, the segments of I-75 between US 27 and SR 326 do not meet the LOS D target in year 2045 and are anticipated to operate at LOS E during either the AM or PM peak hours. The proposed interchange along NW $49^{\text {th }}$ Street is projected to meet the LOS D target; however, similar No Build I-75 segment operations (segments operating at LOS E) are also projected under build conditions. Therefore, a year of failure analysis was performed for the build conditions based on the Diamond/DDI alternative where I-75 segments reach LOS E in 2045. The analysis was conducted by interpolating years 2035 and 2045 volumes and entering each year's volume into HCS until LOS E results were reached. Analysis results are summarized below and HCS worksheets are provided in Appendix $I$.

## o AM Northbound:

- I-75 mainline segment south of US 27-2035
- I-75 mainline basic segment between US 27 and NW 49 ${ }^{\text {th }}$ Street -2037
- NW 49 ${ }^{\text {th }}$ Street off-ramp diverge condition -2041
- NW 49 ${ }^{\text {th }}$ Street on-ramp merge condition - 2044
- I-75 mainline basic segment between NW 49 ${ }^{\text {th }}$ Street and SR 326-2041


## o PM Southbound:

- I-75 south of US 27-2035
- I-75 mainline basic segment between SR 326 and NW 49 ${ }^{\text {th }}$ Street - 2041
- NW 49 ${ }^{\text {th }}$ Street on-ramp merge condition - 2045
- I-75 mainline basic segment between NW 49 ${ }^{\text {th }}$ Street and US 27-2037

Based on the year of failure analysis, additional I-75 mainline improvements may be required in order for I-75 to meet the LOS D target through design year. The District is looking into potential improvements to the I-75 mainline via separate projects or other methods such as the I-75 PD\&E Study (FM Number 443623-1-22-01 \& 443624-1-22-01) to improve overall operations on the I75 mainline. The results and recommendations of this IJR will be shared with the I-75 PD\&E Study team and District Traffic Operations group.

### 6.2.3 Intersection Analysis

As part of the intersection analyses, signal timing and phasing optimization was performed to improve intersection operations. Signal timing and phasing inputs are presented in Appendix $\mathbf{I}$.

It is worth noting that total splits less than minimum splits would be allowed by maintaining agencies due to very low pedestrian activity and presence of pushbuttons for pedestrian interval actuation.

Table 6-5 presents the peak hour Delay and LOS for the intersections on NW 49 ${ }^{\text {th }}$ Street under each build alternative. The overall intersection LOS meets the LOS D target during AM and PM peak hours in years 2025, 2035 and 2045, under all five build alternatives. The approach intersection LOS for all movements also meet the LOS D target, under all five build alternatives except for two instances under 2045 conditions. The SPUI alternative, under 2045 conditions, exhibits deficient approach LOS on the eastbound approach of the NW 49 ${ }^{\text {th }}$ Street at I-75 ramps intersection during the AM and PM peak hours. During the AM peak hour, the eastbound approach operates at LOS F with a delay of 89.3 sec/veh. During the PM peak hour, the eastbound approach operates at LOS E with a delay of $75.8 \mathrm{sec} / \mathrm{veh}$. A comparison of the Build alternatives show that the DDI alternative ramp terminals operate best with LOS B overall intersection operations in 2045. Although in 2045 the northbound I-75 ramps intersection operates at LOS A under the ParClo NE alternative, the southbound I-75 ramps intersection operates at LOS C.

The volumes remain constant across all Build alternatives at the intersections on US 27 and SR 326. With consistent operations, the interchanges reflect similar results regarding Delay and LOS under all five build scenarios. Therefore, Table 6-6 presents the peak hour Delay and LOS under the Build Diamond alternative, for the signalized intersections falling within the AOI of the NW 49 ${ }^{\text {th }}$ Street interchange. In year 2025 during the AM peak hour, the overall intersection LOS D target is met at all locations; during the PM peak hour the US 27 at NW $35^{\text {th }}$ Avenue Road intersection operates at LOS E. In year 2035 during both AM and PM peak hours, the US 27 at NW 35 ${ }^{\text {th }}$ Avenue Road and SR 326 northbound ramp terminus intersections fail. In 2045 during both AM and PM peak hours, the only signalized intersections operating at the LOS D Target or above are the US 27 northbound ramps and the SR 326 northbound ramp intersection. The Synchro outputs are provided in Appendix I.

| Year | \# | Intersection | DIR | AM PEAK ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  | PM PEAK ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Diamond |  | SPUI |  | Parclo-SE |  | Parclo-NE |  | DDI ${ }^{2}$ |  |  | Diamond |  | SPUI |  | Parclo-SE |  | Parclo-NE |  | DDI ${ }^{2}$ |  |  |  |
|  |  |  |  | App. | Int. | App. | Int. Delay LOS | App. <br> Delay LOS | $\begin{gathered} \text { Int. } \\ \text { Delay LOS } \end{gathered}$ | App. <br> Delay LOS | $\begin{gathered} \text { Int. } \\ \text { Delay LOS } \end{gathered}$ | MVMT | App. Int. <br> Delay LOS Delay LOS  |  | App. Delay LOS | $\begin{gathered} \text { Int. } \\ \text { Delay LOS } \end{gathered}$ | App. <br> Delay LOS | Int. | App. <br> Delay LOS | Int. | $\begin{gathered} \text { App. } \\ \text { Delay LOS } \end{gathered}$ | Int. | MVMT | App. <br> Delay LOS |  | Int. <br> Delay LOS |
|  |  |  |  | Delay LOS <br> 42.7 <br> 35.1 <br> D <br> 17.9 <br> B <br> 23.6$\|$ | Delay LOS | Delay LOS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 7 | NW 44 Ave at NW 49 ST | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ |  | $26.4 \text { C }$ | $\begin{array}{ll} 43.1 & \mathrm{D} \\ 35.1 & \mathrm{D} \\ 17.9 & \mathrm{~B} \\ 23.5 & \mathrm{C} \end{array}$ | 26.4 C | $\begin{array}{ll} 43.1 & D \\ 35.1 & D \\ 17.9 & B \\ 23.5 & C \end{array}$ | 26.5 C | $\begin{array}{ll} 43.1 & D \\ 35.1 & D \\ 17.9 & B \\ 23.5 & C \end{array}$ | 26.5 C | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{ll} 42.7 & \mathrm{D} \\ 35.4 & \mathrm{D} \\ 17.8 & \mathrm{~B} \\ 23.5 & \mathrm{C} \end{array}$ | 26.5 C | $\begin{array}{ll} 43.5 & D \\ 36.3 & D \\ 17.3 & B \\ 23.1 & C \end{array}$ | 25.6 C | $\begin{array}{ll} 43.5 & \mathrm{D} \\ 36.2 & \mathrm{D} \\ 17.3 & \mathrm{~B} \\ 23.1 & \mathrm{C} \end{array}$ | 25.6 C | $\begin{array}{ll} 43.5 & \mathrm{D} \\ 36.3 & \mathrm{D} \\ 17.3 & \mathrm{~B} \\ 23.1 & \mathrm{C} \end{array}$ | 25.6 C | $\begin{array}{ll} 43.5 & \mathrm{D} \\ 36.3 & \mathrm{D} \\ 17.3 & \mathrm{~B} \\ 23.1 & \mathrm{C} \end{array}$ | 25.6 C | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{ll} 42.7 & \mathrm{D} \\ 36.0 & \mathrm{D} \\ 13.1 & \mathrm{~B} \\ 22.0 & \mathrm{C} \end{array}$ |  | 23.8 C |
| $\underset{\sim}{N}$ | 8 | 175 SB at NW 49 ST | $\begin{aligned} & \text { EB } \\ & \text { WB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | $\begin{array}{rl} 14.5 & \mathrm{~B} \\ 13.8 & \mathrm{~B} \\ 0.0 & 0 \\ 32.4 & \mathrm{C} \end{array}$ | 17.3 B | $\begin{array}{ll} 17.3 & \mathrm{~B} \\ 25.6 & \mathrm{C} \\ 35.8 & \mathrm{D} \\ 35.3 & \mathrm{D} \end{array}$ | 26.8 C | $\begin{array}{rl} 16.3 & \mathrm{~B} \\ 13.8 & \mathrm{~B} \\ 0.0 & 0 \\ 35.7 & \mathrm{D} \end{array}$ | 18.3 B | $\begin{array}{rl} 16.4 & \mathrm{~B} \\ 13.8 & \mathrm{~B} \\ 0.0 & 0 \\ 35.7 & \mathrm{D} \end{array}$ | 18.3 B | SBR <br> SBL <br> EBT <br> WBT | $\begin{array}{ll} 17.3 & B \\ 33.1 & C \\ 19.0 & B \\ 11.6 & \end{array}$ | 17.0 B | $\begin{array}{rl} 25.5 & \mathrm{C} \\ 26.2 & \mathrm{C} \\ 0.0 & 0 \\ 37.0 & \mathrm{D} \end{array}$ | 28.3 C | $\begin{array}{ll} 13.7 & \text { B } \\ 26.1 & C \\ 36.4 & D \\ 35.2 & D \end{array}$ | 26.7 c | $\begin{array}{rl} 15.7 & \mathrm{~B} \\ 13.1 & \mathrm{~B} \\ 0.0 & 0 \\ 37.0 & \mathrm{D} \end{array}$ | 18.7 B | $\begin{array}{rl} 14.7 & \mathrm{~B} \\ 16.3 & \mathrm{~B} \\ 0.0 & 0 \\ 43.5 & \mathrm{D} \end{array}$ | 21.5 C | SBR <br> SBL <br> EBT <br> WBT | $\begin{array}{rl} 16.3 & \mathrm{~B} \\ 30.4 & \mathrm{C} \\ 6.3 & \mathrm{~A} \\ 21.3 & \mathrm{C} \end{array}$ |  | 17.2 B |
|  | 9 | 175 NB <br> at NW 49 ST | $\begin{array}{\|c\|} \hline E B \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{array}$ | $\begin{array}{rc} 17.1 & \mathrm{~B} \\ 13.8 & \mathrm{~B} \\ 34.8 & \mathrm{C} \\ 0.0 & 0 \end{array}$ | 22.1 C |  |  | $\begin{array}{rl} 0.2 & \mathrm{~A} \\ 8.4 & \mathrm{~A} \\ 38.0 & \mathrm{D} \\ 0.0 & 0 \end{array}$ | 17.1 B | $\begin{array}{ll} 0.4 & A \\ 2.2 & A \\ 0.0 & 0 \\ 0.0 & 0 \end{array}$ | 1.2 A | NBL <br> NBR <br> EBT <br> WBT | $\begin{array}{ll} 33.9 & \text { C } \\ 15.3 & \text { B } \\ 13.6 & \text { B } \\ 16.8 & \text { B } \end{array}$ | 19.3 B | $\begin{array}{rl} 17.9 & \mathrm{~B} \\ 17.0 & \mathrm{~B} \\ 39.4 & \mathrm{D} \\ 0.0 & 0 \end{array}$ | 26.2 C |  |  | $\begin{array}{rl} 0.2 & \mathrm{~A} \\ 9.6 & \mathrm{~A} \\ 33.5 & \mathrm{C} \\ 0.0 & 0 \end{array}$ | 16.9 B | $\begin{array}{ll} 0.3 & \mathrm{~A} \\ 1.9 & \mathrm{~A} \\ 0.0 & 0 \\ 0.0 & 0 \end{array}$ | 0.9 A | NBL <br> NBR <br> EBT <br> WBT | $\begin{array}{ll} 32.2 & \text { C } \\ 16.1 & \text { B } \\ 10.0 & \text { B } \\ 16.3 & \text { } \end{array}$ |  | 18.3 B |
| NoN | 7 | NW 44 Ave at NW 49 ST | $\begin{array}{\|c\|} \hline \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{array}$ | $\begin{array}{ll} 42.7 & D \\ 34.1 & C \\ 21.1 & C \\ 25.3 & C \end{array}$ | 27.8 C | $\begin{array}{ll} 43.2 & D \\ 34.3 & C \\ 21.1 & C \\ 25.1 & C \end{array}$ | 27.8 C | $\begin{array}{ll} 43.2 & D \\ 34.5 & C \\ 21.1 & C \\ 25.1 & C \end{array}$ | 27.8 C | $\begin{array}{ll} 43.2 & D \\ 34.5 & C \\ 21.1 & C \\ 25.1 & C \end{array}$ | 27.8 c | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{ll} 42.7 & \mathrm{D} \\ 35.3 & \mathrm{D} \\ 20.9 & \mathrm{C} \\ 25.0 & \mathrm{C} \end{array}$ | 28.0 C | $\begin{array}{ll} 43.6 & \mathrm{D} \\ 35.7 & \mathrm{D} \\ 20.0 & \mathrm{C} \\ 25.0 & \mathrm{C} \end{array}$ | 27.3 C | $\begin{array}{ll} 43.6 & \mathrm{D} \\ 35.6 & \mathrm{D} \\ 20.0 & \mathrm{C} \\ 25.0 & \mathrm{C} \end{array}$ | 27.2 C | $\begin{array}{ll} 43.6 & D \\ 35.7 & D \\ 20.0 & C \\ 25.0 & C \end{array}$ | 27.3 C | $\begin{array}{ll} 43.6 & D \\ 35.7 & D \\ 20.0 & C \\ 25.0 & C \end{array}$ | 27.3 C | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{ll} 42.6 & \mathrm{D} \\ 35.3 & \mathrm{D} \\ 15.5 & \mathrm{~B} \\ 23.7 & \mathrm{C} \end{array}$ |  | 25.4 C |
|  | 8 | 175 SB at NW 49 ST | $\begin{aligned} & \text { EB } \\ & \text { WB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | $\begin{array}{rl} 15.6 & \mathrm{~B} \\ 16.3 & \mathrm{~B} \\ 0.0 & 0 \\ 33.4 & \mathrm{C} \end{array}$ | 19.2 B | $\begin{array}{ll} 24.3 & C \\ 26.4 & C \\ 35.6 & D \\ 34.2 & C \end{array}$ | 29.0 C | $\begin{array}{rl} 17.5 & \mathrm{~B} \\ 13.1 & \mathrm{~B} \\ 0.0 & 0 \\ 37.2 & \mathrm{D} \end{array}$ | 18.4 B | $\begin{array}{rl} 17.6 & \mathrm{~B} \\ 13.1 & \mathrm{~B} \\ 0.0 & 0 \\ 37.2 & \mathrm{D} \end{array}$ | 18.5 B | SBR <br> SBL <br> EBT <br> WBT | $\begin{array}{rl} 18.4 & \text { B } \\ 36.5 & \text { C } \\ 7.9 & \text { A } \\ 14.7 & B \end{array}$ | 15.6 B | $\begin{array}{rr} 27.1 & \mathrm{C} \\ 26.7 & \mathrm{C} \\ 0.0 & 0 \\ 39.8 & \mathrm{D} \end{array}$ | 29.5 C | $\begin{array}{ll} 15.3 & \mathrm{~B} \\ 27.0 & \mathrm{C} \\ 36.0 & \mathrm{D} \\ 34.0 & \mathrm{C} \end{array}$ | 27.0 | $\begin{array}{rl} 16.8 & \mathrm{~B} \\ 12.6 & \mathrm{~B} \\ 0.0 & 0 \\ 39.8 & \mathrm{D} \end{array}$ | 19.3 B | $\begin{array}{rl} 16.1 & \mathrm{~B} \\ 15.6 & \mathrm{~B} \\ 0.0 & 0 \\ 46.5 & \mathrm{D} \end{array}$ | 22.1 C | SBR <br> SBL <br> EBT <br> WBT | $\begin{array}{rl} 18.5 & B \\ 28.9 & C \\ 7.6 & \text { A } \\ 19.6 & B \end{array}$ |  | 16.9 |
|  | 9 | 175 NB <br> at NW 49 ST | $\begin{array}{\|l\|} \hline \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{array}$ | $\begin{array}{rl} 21.1 & C \\ 16.3 & B \\ 35.2 & D \\ 0.0 & 0 \end{array}$ | 24.4 C |  |  | $\begin{array}{rl} 0.2 & \mathrm{~A} \\ 10.0 & \mathrm{~A} \\ 37.9 & \mathrm{D} \\ 0.0 & 0 \end{array}$ | 17.9 B | $\begin{array}{ll} 0.5 & \mathrm{~A} \\ 2.4 & \mathrm{~A} \\ 0.0 & 0 \\ 0.0 & 0 \end{array}$ | 1.3 A | NBL <br> NBR <br> EBT <br> WBT | $\begin{array}{ll} 33.3 & \text { C } \\ 15.2 & \text { B } \\ 16.0 & \text { B } \\ 16.8 & \text { B } \end{array}$ | 20.0 B | $\begin{array}{rl} 22.8 & \mathrm{C} \\ 19.7 & \mathrm{~B} \\ 39.8 & \mathrm{D} \\ 0.0 & 0 \end{array}$ | 28.8 C |  |  | $\begin{array}{rl} 0.3 & \mathrm{~A} \\ 11.3 & \mathrm{~B} \\ 32.9 & \mathrm{C} \\ 0.0 & 0 \end{array}$ | 17.3 B | $\begin{array}{ll} 0.4 & \mathrm{~A} \\ 2.0 & \mathrm{~A} \\ 0.0 & 0 \\ 0.0 & 0 \end{array}$ | 0.9 A | NBL <br> NBR <br> EBT <br> WBT | $\begin{aligned} 30.9 & \text { C } \\ 17.7 & \text { B } \\ 8.5 & \text { A } \\ 18.2 & \text { B } \end{aligned}$ |  | 18.7 B |
| 華 | 7 | NW 44 Ave at NW 49 ST | $\begin{aligned} & \text { EB } \\ & \text { WB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | $\begin{array}{ll} 43.0 & D \\ 34.0 & C \\ 25.2 & C \\ 27.7 & C \end{array}$ | 29.7 C | $\begin{array}{ll} 43.4 & D \\ 34.2 & C \\ 25.3 & C \\ 27.2 & C \end{array}$ | 29.5 C | $\begin{array}{ll} 43.4 & D \\ 34.5 & C \\ 25.3 & C \\ 27.2 & C \end{array}$ | 29.6 C | $\begin{array}{ll} 43.4 & D \\ 34.5 & C \\ 25.3 & C \\ 27.2 & C \end{array}$ | 29.6 C | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{ll} 43.0 & D \\ 36.1 & D \\ 25.0 & C \\ 27.2 & C \end{array}$ | 30.1 C | $\begin{array}{ll} 43.9 & \mathrm{D} \\ 35.0 & \mathrm{C} \\ 23.7 & \mathrm{C} \\ 27.7 & \mathrm{C} \end{array}$ | 29.3 C | $\begin{array}{ll} 43.9 & \mathrm{D} \\ 34.8 & \mathrm{C} \\ 23.7 & \mathrm{C} \\ 27.7 \end{array}$ | 29.3 C | $\begin{array}{ll} 43.9 & \mathrm{D} \\ 35.0 & \mathrm{C} \\ 23.7 & \mathrm{C} \\ 27.7 & \mathrm{C} \end{array}$ | 29.3 C | $\begin{array}{ll} 43.9 & D \\ 35.0 & D \\ 23.7 & C \\ 27.7 & C \end{array}$ | 29.3 | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{ll} 42.6 & D \\ 33.2 & C \\ 21.8 & C \\ 27.2 & C \end{array}$ | D | 28.4 |
|  | 8 | 175 SB at NW 49 ST | $\begin{aligned} & \text { EB } \\ & \text { WB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | $\begin{array}{rl} 16.4 & \mathrm{~B} \\ 9.9 & \mathrm{~A} \\ 0.0 & 0 \\ 36.1 & \mathrm{D} \end{array}$ | 16.1 B | $\begin{array}{ll} 89.3 & F \\ 28.4 & C \\ 36.2 & D \\ 33.3 & C \end{array}$ | 51.2 D | $\begin{array}{rl} 18.8 & B \\ 12.4 & B \\ 0.0 & 0 \\ 42.7 & D \end{array}$ | 19.3 B | $\begin{array}{rl} \hline 18.9 & \mathrm{~B} \\ 12.4 & \mathrm{~B} \\ 0.0 & 0 \\ 42.8 & \mathrm{D} \end{array}$ | 19.3 B | SBR <br> SBL <br> EBT <br> WBT | $\begin{array}{ll} 21.4 & \text { C } \\ 34.8 & \text { C } \\ 18.2 & \text { B } \\ 13.8 & B \end{array}$ | 18.2 B | $\begin{array}{rl} 6.1 & \mathrm{~A} \\ 28.1 & \mathrm{C} \\ 0.0 & 0 \\ 43.5 & \mathrm{D} \end{array}$ | 25.5 C | $\begin{array}{ll} 75.8 & \mathrm{E} \\ 28.7 & \mathrm{C} \\ 37.0 & \mathrm{D} \\ 32.5 & \mathrm{C} \end{array}$ |  | $\begin{array}{rl} 19.5 & \mathrm{~B} \\ 11.8 & \mathrm{~B} \\ 0.0 & 0 \\ 43.4 & \mathrm{D} \end{array}$ | 20.3 C | $\begin{array}{rl} \hline 19.4 & \mathrm{~B} \\ 12.9 & \mathrm{~B} \\ 0.0 & 0 \\ 47.7 & \mathrm{D} \end{array}$ | 21.7 C | SBR <br> SBL <br> EBT <br> WBT | $\begin{array}{rl} 20.8 & C \\ 28.3 & C \\ 9.9 & A \\ 18.4 & B \end{array}$ |  | 17.3 |
|  | 9 | 175 NB at NW 49 ST | CB | $\begin{array}{rl} 18.3 & \mathrm{~B} \\ 19.0 & \mathrm{~B} \\ 36.0 & \mathrm{D} \\ 0.0 & 0 \end{array}$ | 24.9 C |  |  | $\begin{array}{rl} 0.3 & \mathrm{~A} \\ 11.6 & \mathrm{~B} \\ 37.7 & \mathrm{D} \\ 0.0 & 0 \end{array}$ | 18.8 B | $\begin{array}{ll} 0.6 & \mathrm{~A} \\ 2.8 & \mathrm{~A} \\ 0.0 & 0 \\ 0.0 & 0 \end{array}$ | 1.5 A | NBL <br> NBR <br> EBT <br> WBT | $\begin{array}{ll} 32.4 & \mathrm{C} \\ 16.3 & \mathrm{~B} \\ 13.6 & \mathrm{~B} \\ 18.6 & \mathrm{~B} \end{array}$ | 20.5 B | $\begin{array}{rl} 28.9 & C \\ 22.8 & C \\ 41.1 & D \\ 0.0 & 0 \end{array}$ | 32.3 C |  |  | $\begin{array}{rl} 0.5 & \mathrm{~A} \\ 13.3 & \mathrm{~B} \\ 32.1 & \mathrm{C} \\ 0.0 & 0 \end{array}$ | 17.9 B | $\begin{array}{ll} 0.5 & \mathrm{~A} \\ 2.2 & \mathrm{~A} \\ 0.0 & 0 \\ 0.0 & 0 \end{array}$ | 1.0 A | NBL <br> NBR <br> EBT <br> WBT | $\begin{array}{rl} 30.1 & \mathrm{C} \\ 19.3 & \mathrm{~B} \\ 7.3 & \mathrm{~A} \\ 20.2 & \mathrm{C} \end{array}$ |  | 19.3 |

Table 6-6: Build AOI Intersection Delay and LOS

| \# | Intersection | DIR | AM PEAK |  |  |  |  |  |  |  |  |  |  |  | PM PEAK |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2025 |  |  |  | 2035 |  |  |  | 2045 |  |  |  | 2025 |  |  |  | 2035 |  |  |  | 2045 |  |  |  |
|  |  |  | Approach |  | Intersection |  | Approach |  | Intersection |  | Approach |  | Intersection |  | Approach |  | Intersection |  | Approach |  | Intersection |  | Approach |  | Intersection |  |
|  |  |  | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS | Delay ${ }^{2}$ | LOS |
| 1 | NW 44 Ave at US 27 | EB <br> WB <br> NB <br> SB | $\begin{aligned} & 18.7 \\ & 18.6 \\ & 34.9 \\ & 28.9 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { C } \\ & \text { C } \end{aligned}$ | 20.7 | C | $\begin{aligned} & 36.0 \\ & 21.8 \\ & 48.2 \\ & 41.6 \end{aligned}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{C} \\ & \mathrm{D} \\ & \mathrm{D} \end{aligned}$ | 31.7 | C | $\begin{array}{r} 111.1 \\ 33.0 \\ 49.7 \\ 45.9 \end{array}$ | F | 70.5 | E | $\begin{aligned} & 15.3 \\ & 24.2 \\ & 56.2 \\ & 41.9 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{C} \\ & \mathrm{E} \\ & \mathrm{D} \end{aligned}$ | 24.0 | C | $\begin{aligned} & 21.9 \\ & 59.9 \\ & 57.7 \\ & 47.0 \end{aligned}$ | $\begin{gathered} \mathrm{C} \\ \mathrm{E} \\ \mathrm{E} \\ \mathrm{D} \end{gathered}$ | 45.4 | D | $\begin{array}{r} 39.0 \\ 171.5 \\ 60.4 \\ 48.3 \end{array}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{~F} \\ & \mathrm{E} \\ & \mathrm{D} \end{aligned}$ | 111.1 | F |
| 2 | $\mathrm{I}-75 \mathrm{SB}$ at US 27 | EB <br> WB <br> NB <br> SB | $\begin{array}{r} 16.3 \\ 6.3 \\ 0.0 \\ 39.9 \end{array}$ | $\begin{gathered} \mathrm{B} \\ \mathrm{~A} \\ 0 \\ \mathrm{D} \end{gathered}$ | 13.2 | B | $\begin{array}{r} 48.8 \\ 13.9 \\ 0.0 \\ 42.1 \end{array}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{~B} \\ & 0 \\ & \mathrm{D} \end{aligned}$ | 33.5 | C | $\begin{array}{r} 90.5 \\ 21.4 \\ 0.0 \\ 50.7 \end{array}$ | $\begin{aligned} & \mathrm{F} \\ & \mathrm{C} \\ & 0 \\ & \mathrm{D} \end{aligned}$ | 57.6 | E | $\begin{array}{r} 19.7 \\ 7.5 \\ 0.0 \\ 54.1 \end{array}$ | $\begin{gathered} \mathrm{B} \\ \mathrm{~A} \\ 0 \\ \mathrm{D} \end{gathered}$ | 13.7 | B | $\begin{array}{r} 38.9 \\ 17.0 \\ 0.0 \\ 60.9 \end{array}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{~B} \\ & 0 \\ & \mathrm{E} \end{aligned}$ | 26.8 | C | $\begin{array}{r} 62.2 \\ 53.7 \\ 0.0 \\ 97.9 \end{array}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{D} \\ & 0 \\ & \mathrm{~F} \end{aligned}$ | 58.5 | E |
| 3 | I-75 NB at US 27 | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{r} 1.0 \\ 12.3 \\ 32.1 \\ 0.0 \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { B } \\ & \text { C } \\ & 0 \end{aligned}$ | 11.5 | B | $\begin{array}{r} 0.8 \\ 16.2 \\ 32.0 \\ 0.0 \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { B } \\ & \text { C } \\ & 0 \\ & \hline \end{aligned}$ | 12.9 | B | $\begin{array}{r} 2.2 \\ 19.4 \\ 33.7 \\ 0.0 \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { B } \\ & \text { C } \\ & 0 \end{aligned}$ | 15.5 | B | $\begin{array}{r} 1.1 \\ 14.2 \\ 39.6 \\ 0.0 \end{array}$ | $\begin{aligned} & \hline \text { A } \\ & \text { B } \\ & \text { D } \\ & \hline \\ & \hline \end{aligned}$ | 15.1 | B | $\begin{array}{r} 1.4 \\ 18.4 \\ 43.7 \\ 0.0 \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { B } \\ & \text { D } \\ & 0 \end{aligned}$ | 18.2 | B | $\begin{array}{r} 1.5 \\ 45.4 \\ 77.3 \\ 0.0 \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { D } \\ & \text { E } \\ & 0 \end{aligned}$ | 39.6 | D |
| 4 | NW 35 Ave Rd at US 27 | EB <br> WB <br> NB <br> SB | $\begin{array}{r} 21.9 \\ 23.5 \\ 53.4 \\ 124.0 \end{array}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{D} \\ & \mathrm{~F} \end{aligned}$ | 36.2 | D | $\begin{array}{r} 34.9 \\ 48.0 \\ 54.0 \\ 232.0 \end{array}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{D} \\ & \mathrm{D} \\ & \mathrm{~F} \end{aligned}$ | 67.4 | E | $\begin{array}{r} 49.0 \\ 60.6 \\ 55.0 \\ 397.8 \end{array}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{E} \\ & \mathrm{E} \\ & \mathrm{~F} \end{aligned}$ | 112.7 | F | $\begin{array}{r} 38.9 \\ 69.4 \\ 52.8 \\ 122.4 \end{array}$ | $\begin{gathered} \mathrm{D} \\ \mathrm{E} \\ \mathrm{D} \\ \mathrm{~F} \end{gathered}$ | 63.5 | E | $\begin{array}{r} 71.8 \\ 128.5 \\ 53.6 \\ 289.0 \end{array}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{~F} \\ & \mathrm{D} \\ & \mathrm{~F} \end{aligned}$ | 129.7 | F | $\begin{array}{r} 99.6 \\ 193.5 \\ 55.0 \\ 517.8 \end{array}$ | $\begin{aligned} & \hline F \\ & F \\ & \text { D } \\ & \text { F } \end{aligned}$ | 218.1 | F |
| 6 | NW 44 Ave/-I75 SB Off at SR 326 | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{aligned} & 12.7 \\ & 12.7 \\ & 21.1 \\ & 15.0 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { C } \\ & \text { B } \end{aligned}$ | 13.9 | B | $\begin{aligned} & 14.6 \\ & 14.7 \\ & 23.8 \\ & 19.9 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { C } \\ & \text { B } \end{aligned}$ | 17.2 | B | $\begin{aligned} & 15.8 \\ & 15.9 \\ & 28.3 \\ & 24.2 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { C } \\ & \text { C } \end{aligned}$ | 19.4 | B | $\begin{aligned} & 15.2 \\ & 15.1 \\ & 26.0 \\ & 19.2 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { C } \\ & \text { B } \\ & \hline \end{aligned}$ | 17.5 | B | $\begin{aligned} & 18.8 \\ & 17.3 \\ & 27.3 \\ & 21.8 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { C } \\ & \text { C } \end{aligned}$ | 20.4 | C | $\begin{aligned} & 19.8 \\ & 20.5 \\ & 32.7 \\ & 31.5 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 24.9 | C |
| 7 | I-75 SB On-Ramp (Loop) at SR 326 | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \end{gathered}$ | $\begin{array}{r} 0.0 \\ 3.1 \\ 11.2 \\ \hline \end{array}$ | $\begin{gathered} \mathrm{A} \\ \mathrm{~A} \\ \mathrm{~B} \end{gathered}$ | 2.3 | A | $\begin{array}{r} 0.0 \\ 4.2 \\ 12.6 \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{~B} \end{aligned}$ | 2.9 | A | $\begin{array}{r} 0.0 \\ 6.5 \\ 13.6 \\ \hline \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { A } \\ & \text { B } \end{aligned}$ | 4.4 | A | $\begin{array}{r} \hline 0.0 \\ 1.2 \\ 10.9 \\ \hline \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { A } \\ & \text { B } \end{aligned}$ | 1.0 | A | $\begin{array}{r} \hline 0.0 \\ 1.6 \\ 12.3 \\ \hline \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { A } \\ & \text { B } \end{aligned}$ | 1.2 | A | $\begin{array}{r} 0.0 \\ 1.5 \\ 12.6 \\ \hline \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { A } \\ & \text { B } \end{aligned}$ | 1.2 | A |
| 8 | I-75 NB Off/I-75 NB On at SR $326^{1}$ | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{r} 8.2 \\ 23.9 \\ 74.7 \\ 0.0 \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{C} \\ & \mathrm{E} \\ & \mathrm{~A} \end{aligned}$ | 35.1 | D | $\begin{array}{r} 9.7 \\ 75.3 \\ 416.8 \\ 0.0 \end{array}$ | $\begin{gathered} \text { A } \\ \text { E } \\ \text { F } \\ \text { A } \end{gathered}$ | 164.1 | F | $\begin{array}{r} 13.9 \\ 251.1 \\ 774.4 \\ 0.0 \end{array}$ | $\begin{gathered} \text { B } \\ \text { F } \\ \text { F } \\ \text { A } \end{gathered}$ | 365.7 | F | $\begin{array}{r} 22.9 \\ 59.7 \\ 64.0 \\ 0.0 \end{array}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{E} \\ & \mathrm{E} \\ & \mathrm{~A} \end{aligned}$ | 52.8 | D | $\begin{array}{r} 28.7 \\ 149.4 \\ 244.7 \\ 0.0 \end{array}$ | $\begin{aligned} & \text { C } \\ & \text { F } \\ & \text { F } \\ & \text { A } \end{aligned}$ | 153.6 | F | $\begin{array}{r} 57.8 \\ 431.3 \\ 431.2 \\ 0.0 \end{array}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{~F} \\ & \mathrm{~F} \\ & \mathrm{~A} \end{aligned}$ | 367.2 | F |

Based on the intersection analysis for the AOI of the five Build alternatives, minor improvements at intersections on the surface streets were identified. In general, improvements to the surface streets are geometrically limited. Identified minor improvements include:

- US-27 and NW 44 ${ }^{\text {th }}$ Avenue:
o Modify lane assignment on southbound approach to reflect two southbound left turn lanes and one shared thru/right turn lane.
o Signal timing optimization and eliminate southbound/northbound split phasing.
- US-27 at I-75 Southbound:
o Signal timing/phasing modifications to operate westbound left turn phase as a lagging phase.
- US-27 and NW 35 ${ }^{\text {th }}$ Avenue Road:
o Signal timing/phasing modifications to include southbound right-turn overlap to extend both southbound right turn and eastbound left turn phases to address high traffic demand.
- SR 326 at I-75 Northbound:
o Signalize channelized northbound right turn movement and provide overlap phase for concurrent operations with westbound thru movement to meet high westbound right and northbound right turn traffic demand.


### 6.2.4 Vissim Analysis

A network analysis was performed based on the model calibrated under existing conditions to evaluate the study area as a system. The analysis was conducted for No Build and the five Build scenarios under AM and PM peak hours. Results for 2045 AM and PM are summarized in this section with detailed volume inputs and link summaries provided in Appendix I. The following list of MOEs were used:

- Intersections
o Volume (vehicles)
o Delay (seconds/vehicle)
o Queues (feet)
- Roadway Links
o Average Speed (mph)
o Travel Time
- Freeway Facility
o Average Speed (mph)
o Density (veh/mi/ln)
o Volume (vph)
- Network
o Total Delay (hrs)
o Total Stops (\# of stops)
o Average Speed (mph)
o Vehicles Arrived (vehicles)
o VMT
o Latent Delay (hours)
o Latent Demand (vehicles)


### 6.2.4.1 Network Coding

The No Build and Build alternatives geometry was coded by using the calibrated file and modifying the network based on the identified improvements from the Synchro Analysis. The same steps performed for the calibrated model were followed in the coding of roadway elements. I-75 mainline was initially coded with split links in order to facilitate the coding of the NW $49^{\text {th }}$ Street interchange alternatives.

Based on simulation observations, driver behavior settings were adjusted for the I-75 merge/diverge segments to improve merging characteristics between mainline and merging/diverging vehicles. It was necessary to modify the parameters for the subject segment types in order to replicate realistic merging/diverging characteristics. As identified in the merge/diverge HCS analysis, several merge/diverge segments operate at LOS E or LOS F during design year and sometimes consist of a short merge/diverge lane. The combination of a short merge lane and high vehicular density on the mainline results in queueing of vehicles on the on-ramp as they are unable to find a gap in I-75 mainline traffic to merge. Under preliminary simulations, the southbound merge queue was observed spilling back onto US 27 further exacerbating arterial conditions. Driver behavior parameters for the subject segment types were adjusted incrementally while observing arterial, ramp, and mainline operations in accordance with suggested ranges outlined in the 2014 FDOT Traffic Analysis Handbook. The following adjustments were made in order to strike a balance and realistic simulation in operations between the involved facilities (arterials, merge/diverge segments, and mainline):

- Safety distance lane change factor 0.2 (Suggested Range: 0.1 to 0.9)
- Maximum Cooperative Deceleration -18.0 ft/s ${ }^{2}$ (Suggested Range: -32.2 to -3 ft/s ${ }^{2}$ )


### 6.2.4.2 Vissim Analysis Results-Intersections

Tables 6-7 and 6-8 summarize the volume, LOS, delay, and queues for each intersection in year 2045 during AM and PM peak hours. It should be noted that delay results for intersection approaches are based on the Vissim defined node areas while queue length results are not bound by the node area; therefore, providing a measure of congestion caused by delays.

In general, US 27 on both sides of the interchange operate under oversaturated conditions with substantial delays and queue lengths. During the AM peak hour, the US 27 at I-75 southbound ramps intersection operates at an overall LOS C for all scenarios, although the southbound leftturn movement fails for all Build alternatives; during the PM peak hour, this intersection operates at an overall LOS B for all Build alternatives. The US 27 at I-75 northbound ramps intersection is projected to operate at an overall LOS D during the AM and PM peak hours for No Build and LOS C for all Build alternatives. The US 27 at NW $35^{\text {th }}$ Avenue Road intersection displays deficient LOS on the majority of movements during both peak hours. During the AM peak hour, the No Build scenario displays an overall LOS D while the Build alternatives display LOS C except for the SPUI alternative at LOS D; The PM peak hour displays LOS E for all scenarios. The US 27 at NW $44^{\text {th }}$ Avenue intersection displays an overall LOS D under all scenarios during the AM peak hour but is projected to fail under No Build during the PM peak hour with a projected LOS E. Several movements are projected to fail at the intersection of US 27 at NW $38^{\text {th }}$ Avenue, during both peak hours, however, the overall intersection LOS meets the LOS D Target or better. Queue length results for US 27 intersections show that delays experienced contribute to significant queue lengths and oversaturated operating conditions.

In addition, the No Build scenario displays notable LOS, delay, and queue impacts at the SR 326 intersections when compared to the Build alternatives which are projected to operate at the LOS D Target or better. For the No Build scenario during the AM peak hour, the northbound right-turn and westbound left-turn movements of the SR 326 at NW $44^{\text {th }}$ Avenue intersection exhibit LOS E with an overall intersection LOS D. During the PM peak hour, the same intersection performs at an overall LOS E with the northbound turning movements displaying LOS F. The SR 326 intersection at the I-75 southbound slip and loop ramps is projected to operate at an overall LOS A for all scenarios during both peak hours. The SR 326 at I-75 northbound ramps intersection is projected to generate significant queues on the westbound approach with average queue lengths over 4,000 feet under No Build and 3,000 feet under the Build alternatives.

Table 6-7: 2045 Vissim Intersection Delay \& LOS Summary (AM Peak)

| Intersection | Control | мvмт | No Build |  |  |  |  | Diamond |  |  |  |  | SPUI 2045 AM Peak ${ }^{1}$ Parclo SE |  |  |  |  |  |  |  |  |  | Parclo NE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Vol | Delay | LOS | AvgQ | MaxQ | Vol | Delay |  | AvgQ | MaxQ | Vol | Delay | LOS | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol Delay ${ }^{\text {DDI }}$ |  |  | AvgQ | MaxO |
| NW 49 St atNW 44 Ave | s | NBL | 7 | 26.2 | C | 1 | 28 | 9 | 23.9 | c | 1 | 23 | 8 | 26.4 | c | 2 | 25 | 9 | 26.1 | C | 1 | 25 | 8 | 25.0 | c | 1 | 26 | 9 | 24.6 | c | 1 |  |
|  |  | NBT | 223 | 32.3 | c | 59 | 283 | 145 | 34.6 | c | 21 | 104 | 144 | 34.2 | c | 20 | 101\| | 144 | 34.3 | c | 20 | 102 | 145 | 34.4 | c | 20 | 105 | 144 | 33.5 | c | 20 | 106 |
|  |  | NBR | 275 | 21.5 | c | 1 | 26 | 319 | 8.3 | A | 0 | 5 | 319 | 8.7 | A | 0 | 6 | 317 | 8.3 | A | 0 | 3 | 318 | 8.5 | A | 0 | 4 | 318 | 8.6 | A | 0 |  |
|  |  | SBL | 427 | 17.6 | B | 43 | 314 | 630 | 36.1 | D | 105 | 490 | 633 | 39.3 | D | 120 | 508\| | 635 | 40.4 | D | 125 | 522 | 631 | 39.2 | D | 117 | 506 | 634 | 37.9 | D | 112 | 499 |
|  |  | SBT | 405 | 11.7 | B | 15 | 126 | 338 | 12.7 | B | 13 | 131 | 338 | 14.2 | B | 13 | 119 | 338 | 14.4 | B | 14 | 136\| | 338 | 13.9 | B | 14 | 144 | 338 | 12.8 | B | 12 | 128 |
|  |  | SBR | 7 | 7.5 | A | 32 | 178\| | 5 | 15.3 | B | 13 | 131 | 6 | 17.0 | B | 13 | 119 \| | 5 | 15.0 | B | 14 | 136 | 5 | 15.9 | B | 14 | 144 | 5 | 15.4 | B | 12 | 128 |
|  |  | EBL | 6 | 36.1 | D | 4 | 42 | 7 | 43.7 | D | 5 | 52 | 6 | 47.4 | D | 6 | 51 | 7 | 43.7 | D | 5 | 52 | 7 | 43.7 | D | 5 | 52 | 7 | 46.3 | D | 5 | 52 |
|  |  | EBT | 9 | 45.5 | D | 4 | 42 | 15 | 44.0 | D | 5 | 52 | 14 | 51.3 | D | 6 | 51\| | 15 | 44.0 | D | 5 | 52 | 15 | 44.1 | D | 5 | 52 | 15 | 43.9 | D | 5 | 52 |
|  |  | EBR | 4 | 8.1 | A |  | 62 | 4 | 16.2 | B | 3 | 87 | 4 | 11.6 | B | 3 | 86\| | 4 | 16.2 | B | 3 | $87 \mid$ | 4 | 16.1 | B | 3 | 87 | 4 | 14.5 | B | 2 | 87 |
|  |  | WBL | 294 | 31.2 | c | 70 | 300 | 467 | 40.5 | D | 73 | 269 | 466 | 33.0 | c | 59 | 261 | 467 | 37.6 | D | 70 | 336\| | 471 | 36.6 | D | 72 | 321 | 466 | 41.5 | D | 74 | 337 |
|  |  | WBT | 13 | 38.7 | D | 70 | $300 \mid$ | 12 | 43.6 | D | 70 | 259 | 13 | 35.4 | D | 55 | 2371 | 12 | 40.0 | D | 60 | 275 | 13 | 35.5 | D | 60 | 218 | 13 | 44.7 | D | 71 | 303 |
|  |  | WBR | 257 | 22.8 | c | 89 | 326 | 445 | 40.3 | D | 70 | 259 | 443 | 32.2 | c | 55 | 2371 | 443 | 36.0 | D | 60 | 275 | 447 | 34.4 | c | 60 | 218 | 445 | 41.2 | D | 71 | 303 |
|  |  | Overall |  | 21.7 | c |  |  |  | 30.7 | c |  |  |  | 28.9 | c |  |  |  | 30.7 | c |  |  |  | 29.8 | c |  |  |  | 31.5 | c |  |  |
| SR 326 at NW 44 Ave | s | NBL | 52 | 41.3 | D | 116 | 332 | 22 | 27.8 | c | 11 | 128 | 22 | 28.8 | c | 11 | 125 | 22 | 27.6 | c | 12 | 132 | 22 | 25.5 | c | 12 | 135 | 21 | 25.7 | c | 11 | 126 |
|  |  | NBR | 254 | 63.2 | E | 124 | 329\| | 110 | 29.2 | c | 21 | 124 | 109 | 27.9 | c | 20 | 123 | 109 | 29.2 | c | 21 | 130\| | 109 | 30.0 | c | 22 | 131 | 109 | 28.8 | c | 20 | 124 |
|  |  | SBL | 308 | 46.2 | D | 148 | 548 \| | 286 | 25.7 | c | 54 | 309 | 287 | 25.3 | c | 53 | 3031 | 287 | 25.7 | c | 55 | 309\| | 288 | 26.0 | c | 55 | 313 | 286 | 25.2 | c | 53 | 296 |
|  |  | SBT | 81 | 49.8 | D | 148 | 548 \| | 27 | 28.1 | c | 54 | 309 | 27 | 27.9 | c | 53 | 303\| | 28 | 28.9 | c | 55 | 309 | 27 | 26.7 | c | 55 | 313 | 27 | 29.2 | c | 53 | 296 |
|  |  | SBR | 141 | 5.4 | A | 0 | 36 | 130 | 1.8 | A | 0 | 38 | 129 | 1.8 | A | 0 | 43 | 129 | 1.8 | A | 0 | 26 | 129 | 1.8 | A | 0 | 31 | 129 | 1.7 | A | 0 | 27 |
|  |  | EBT | 496 | 22.1 | c | 49 | 259 | 516 | 19.8 | B | 41 | 228 | 516 | 19.5 | B | 40 | 233 | 516 | 19.1 | B | 39 | 225 | 517 | 19.3 | B | 40 | 227 | 517 | 18.8 | B | 38 | 226 |
|  |  | EBR | 74 | 16.9 | B | 1 | 631 | 28 | 15.4 | B | 0 | 29 | 28 | 15.1 | B | 1 | 37 | 29 | 16.4 | B | 0 | 291 | 28 | 16.0 | B | 0 | 27 | 28 | 14.2 | B | 0 | 29 |
|  |  | WBL | 206 | 60.6 | E | 85 | 301 | 95 | 29.7 | c | 13 | 119 | 95 | 28.4 | c | 12 | 113 | 95 | 26.1 | c | 10 | 111 | 96 | 26.3 | c | 10 | 112 | 95 | 28.1 | c | 11 |  |
|  |  | WBT | 286 | 21.1 | c | 28 | 165 | 275 | 19.0 | B | 23 | 148 | 275 | 18.5 | B | 23 | 145\| | 276 | 19.1 | B | 23 | 145 | 277 | 19.6 | B | 25 | 150 | 275 | 18.7 | B | 22 | 138 |
|  |  | Overall |  | 36.3 | D |  |  |  | 20.7 | c |  |  |  | 20.3 | c |  |  |  | 20.3 | c |  |  |  | 20.6 | c |  |  |  | 20.1 | c |  |  |
| SR 326 at I-75 NB | s | NBL | 190 | 35.0 | C | 42 | 227 | 147 | 34.8 | C | 31 | 179 | 146 | 34.1 | C | 30 | 185 | 147 | 34.9 | C | 31 | 177 | 148 | 35.1 | D | 32 | 183 | 147 | 34.5 | C | 31 | 175 |
|  |  | NBR | 1023 | 12.2 | B | 152 | 978\| | 1083 | 11.3 | B | 72 | 801 | 1076 | 10.8 | B | 63 | 728 | 1084 | 11.3 | B | 85 | $870 \mid$ | 1080 | 11.6 | B | 104 | 937 | 1079 | 10.9 | B | 76 | 748 |
|  |  | EBL | 269 | 33.9 | c | 61 | 303\| | 207 | 27.1 | c | 31 | 218 | 209 | 28.1 | c | 32 | 233\| | 207 | 28.0 | c | 33 | 221 | 208 | 27.9 | c | 32 | 218 | 208 | 27.9 | c | 33 | 219 |
|  |  | EBT | 639 | 6.3 | A | 11 | 142 | 572 | 6.1 | A | 9 | 135 | 572 | 6.0 | A | 9 | 132 | 572 | 6.2 | A | , | 133\| | 573 | 6.3 | A | 10 | 134 | 573 | 6.0 | A | 9 | 119 |
|  |  | WBT | 1239 | 50.4 | D | 4078 | 4853 | 1312 | 41.0 | D | 2557 | 3603 | 1313 | 40.4 | D | 2612 | 3702 | 1308 | 41.4 | D | 2705 | 3741 | 1318 | 41.0 | D | 2437 | 3537 | 1307 | 41.5 | D | 2557 | 3645 |
|  |  | WBR | 420 | 44.7 | D | 3784 | 4616 | 482 | 35.3 | D | 2198 | 3289 | 483 | 35.3 | D | 2174 | 3239 | 480 | 35.4 | D | 2535 | 3689\| | 487 | 34.8 | c | 1875 | 2926 | 482 | 35.9 | D | 2149 | 3264 |
|  |  | Overall |  | 30.0 | c |  |  |  | 25.5 | c |  |  |  | 25.2 | c |  |  |  | 25.7 | c |  |  |  | 25.8 | c |  |  |  | 25.7 | c |  |  |
| $\left\lvert\, \begin{gathered} \text { US } 27 \text { at } 1-75 \\ \text { SB } \end{gathered}\right.$ | s | SBL | 149 | 44.9 | D | 40 | 186 | 212 | 58.8 | E | 91 | 323 | 211 | 59.4 | E | 93 | 306 | 213 | 57.6 | E | 90 | 325 | 213 | 57.4 | E | 90 | 319 | 213 | 56.9 | E | 88 | 308 |
|  |  | SBR | 59 | 2.5 | A | 0 | 0 | 91 | 11.8 | B | 1 | 9 | 91 | 12.0 | B | 1 | 8 | 90 | 11.6 | B | 1 | 8 | 91 | 11.8 | B | 1 | 10 | 92 | 10.7 | B | 1 |  |
|  |  | EBT | 1494 | 35.0 | c | 362 | 819 | 1511 | 37.4 | D | 422 | 825 | 1517 | 37.5 | D | 416 | 832 | 1511 | 38.0 | D | 420 | 832 | 1512 | 37.0 | D | 413 | 827 | 1523 | 36.2 | D | 404 | 826 |
|  |  | EBR | 620 | 25.0 | c | 145 | 812 | 548 | 23.3 | c | 96 | 648 | 551 | 22.5 | c | 94 | 594 | 546 | 22.5 | c | 93 | 656 | 547 | 23.0 | c | 97 | 607 | 552 | 22.6 | c | 101 | 688 |
|  |  | WBL | 534 | 21.6 | c | 123 | 407\| | 467 | 22.2 | c | 99 | 399 | 465 | 22.4 | c | 98 | 394 | 466 | 22.5 | c | 100 | 392 | 465 | 21.7 | c | 95 | 398 | 467 | 22.2 | c | 96 | 397 |
|  |  | WBT | 1457 | 5.7 | A | 31 | 334 | 1535 | 5.2 | A | 27 | 293 | 1524 | 5.2 | A | 26 | 292 | 1539 | 5.3 | A | 28 | 283 | 1535 | 5.2 | A | 27 | 286 | 1536 | 5.2 | A | 26 | 270 |
|  |  | Overall |  | 21.9 | c |  |  |  | 23.2 | c |  |  |  | 23.2 | c |  |  |  | 23.3 | c |  |  |  | 22.9 | c |  |  |  | 22.6 | c |  |  |
| $\left\lvert\, \begin{gathered} \text { US } 27 \text { at } 1-75 \\ \text { NB } \end{gathered}\right.$ | s | NBL | 487 | 46.4 | D | 71 | 269 | 412 | 38.0 | D | 58 | 228 | 407 | 43.9 | D | 61 | 243 | 412 | 38.8 | D | 58 | 228 | 410 | 41.6 | D | 60 | 227 | 410 | 37.5 | D | 57 | 223 |
|  |  | NBR | 692 | 78.7 | E | 878 | 2524 | 623 | 64.0 | E | 195 | 773 | 615 | 75.2 | E | 480 | 1442 | 623 | 67.0 | E | 240 | 892 | 617 | 74.4 | E | 338 | 1116 | 619 | 61.8 | E | 261 | 826 |
|  |  | EBL | 73 | 12.7 | B | 1 | 44 | 110 | 15.0 | B | 4 | 84 | 112 | 17.5 | B | 6 | 93\| | 109 | 14.9 | B | 4 | 78 | 111 | 15.7 | B | 4 | 86 | 112 | 17.7 | B | 5 | 93 |
|  |  | EBT | 1567 | 22.8 | c | 36 | 273\| | 1611 | 22.8 | c | 39 | 286 | 1610 | 24.7 | c | 41 | 273\| | 1606 | 22.9 | c | 41 | 274 | 1607 | 24.2 | c | 38 | 265 | 1622 | 21.8 | c | 35 | 266 |
|  |  | WBT | 971 | 27.6 | c | 43 | 314 | 1123 | 17.6 | B | 45 | 392 | 1118 | 17.5 | B | 45 | 388 | 1126 | 18.3 | B | 47 | 381 | 1126 | 17.5 | B | 45 | 371 | 1125 | 17.0 | B | 44 | 350 |
|  |  | WBT>L | 536 | 89.4 | F | 538 | 1143\| | 469 | 46.2 | D | 163 | 660 | 466 | 44.0 | D | 146 |  | 468 | 49.5 | D | 186 | $759 \mid$ | 468 | 44.9 | D | 155 |  | 469 | 42.5 | D | 134 | 571 |
|  |  | WBR | 142 | 17.3 | B |  |  | 202 | 11.2 | B | , |  | 200 | 11.0 | B |  |  | 201 | 10.7 | B |  |  | 203 | 10.9 | B | 0 |  | 202 | 10.2 | B | 0 |  |
|  |  | Overall |  | 42.5 |  |  |  |  | 30.4 | c |  |  |  | 32.8 | c |  |  |  | 31.4 | c |  |  |  | 32.4 | c |  |  |  | 29.0 | c |  |  |

${ }^{1}$ Volume in vph; delay in sec/veh; LOS is Estimated LOS using HCM2010 thresholds; Queue Lengths in feet
(continued next page)

| Intersection | Control | мvmт | 2045 AM Peak ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | No Build |  |  |  |  | Diamond |  |  |  |  | SPUI 20, |  |  |  |  | Parclo SE |  |  |  |  | Parclo NE |  |  |  |  | DDI |  |  |  |  |
|  |  |  | Vol | Delay | LOS | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | LOS | AvgQ | MaxQ | Vol | Delay | LOS | AvgQ | MaxQ |
| $\begin{gathered} \text { US } 27 \text { at NW } \\ 35 \text { Ave Rd } \end{gathered}$ | s | NBL | 22 | 89.9 | F | 21 | 125 | 24 | 71.8 | E | 21 | 124 | 24 | 71.9 | E | 21 | 124 | 24 | 71.7 | E | 21 | 124 | 24 | 71.2 | E | 21 | 124 | 24 | 70.6 | E | 21 | 124 |
|  |  | NBT | 22 | 67.2 | E | 21 | $125 \mid$ | 20 | 70.5 | E | 21 | $124 \mid$ | 20 | 70.4 | E | 21 | 124 | 20 | 70.5 | E | 21 | 124 | 20 | 70.4 | E | 21 | 124 | 20 | 70.5 | E | 21 | 124 |
|  |  | NBR | 10 | 34.6 | c | 28 | 140\| | 11 | 32.2 | c | 27 | 139 | 11 | 31.1 | c | 27 | 139 | 11 | 31.1 | c | 27 | 139 | 11 | 32.4 | c | 27 | 139 | 11 | 31.1 | c | 27 | 139 |
|  |  | SBL | 214 | 101.9 | F | 183 | 498 | 201 | 84.4 | F | 123 | 388 | 202 | 90.4 | F | 137 | 411 | 201 | 84.5 | F | 126 | 424 | 201 | 84.5 | F | 126 | 415 | 201 | 84.0 | F | 125 | 395 |
|  |  | SBT | 6 | 76.9 | E | 2 | 26 | 8 | 67.4 | E | 3 | 29 | 8 | 70.1 | E | 3 | 29 | 8 | 62.8 | E | 3 | $29 \mid$ | 8 | 63.4 | E | 3 | 29 | 8 | 64.1 | E | 3 | 29 |
|  |  | SBR | 563 | 98.9 | F | 606 | 1127 | 607 | 40.0 | D | 193 | 7031 | 607 | 43.4 | D | 208 | 699 | 607 | 38.9 | D | 182 | 689 | 608 | 39.1 | D | 185 | 675 | 607 | 33.7 | C | 150 | 648 |
|  |  | EBL | 510 | 50.7 | D | 433 | 1181\| | 493 | 53.3 | D | 443 | 1157\| | 495 | 54.6 | D | 457 | 1161 | 495 | 53.1 | D | 432 | 1147\| | 491 | 55.4 | E | 464 | 1190 | 496 | 52.6 | D | 428 | 1152 |
|  |  | EBT | 1699 | 16.0 | B | 145 | 1067 | 1692 | 15.3 | B | 137 | 990 | 1691 | 15.8 | B | 141 | 972 | 1692 | 15.6 | B | 139 | 990 | 1688 | 16.0 | B | 126 | 1001 | 1699 | 15.5 | B | 145 | 980 |
|  |  | EBR | 40 | 12.3 | B | 0 | 44 | 40 | 10.2 | B | 0 | $47 \mid$ | 40 | 10.3 | B | 0 | 46 | 40 | 10.9 | B | 0 | 48 | 40 | 11.8 | B | 0 | 46 | 39 | 11.1 | B | 0 | 43 |
|  |  | WBL | 32 | 55.1 | E | 3 | 45 | 35 | 39.1 | D | 3 | 46 | 35 | 40.7 | D | 3 | 47 | 35 | 42.7 | D | 4 | 49 \| | 35 | 43.0 | D | 3 | 46\| | 36 | 39.8 | D | 3 | 46 |
|  |  | WBT | 1075 | 83.8 | F | 1013 | 1787\| | 1163 | 44.9 | D | 306 | 1034 | 1159 | 45.4 | D | 353 | 1092 | 1168 | 45.2 | D | 301 | 1037 | 1166 | 44.0 | D | 304 | 1042 | 1167 | 41.3 | D | 251 | 976 |
|  |  | WBR | 297 | 32.6 | C | 768 | 1453\| | 281 | 17.4 | B | 141 | $700 \mid$ | 282 | 18.0 | B | 183 | 758 | 284 | 17.6 | B | 132 | 704 | 284 | 16.8 | B | 139 | 709 | 285 | 15.4 | B | 95 | 645 |
|  |  | Overall |  | 52.4 | D |  |  |  | 34.4 | c |  |  |  | 35.5 | D |  |  |  | 34.4 | c |  |  |  | 34.5 | c |  |  |  | 32.4 | c |  |  |
| $\begin{gathered} \text { US } 27 \text { at NW } \\ 44 \text { Ave } \end{gathered}$ | s | NBL | 51 | 56.8 | E | 18 | 89 | 33 | 50.3 | D | 10 | 70 | 33 | 52.1 | D | 10 | 65 | 34 | 53.4 | D | 11 | 68 | 33 | 53.6 | D | 11 | 71 | 34 | 50.4 | D | 10 | 69 |
|  |  | NBT | 12 | 49.9 | D | 3 | 271 | 6 | 51.7 | D | 1 | 19 | 6 | 53.2 | D | 2 | 17 | 6 | 50.7 | D | 2 | 19\| | - | 50.1 | D | 1 | 19 | 6 | 48.0 | D | 2 | 21 |
|  |  | NBR | 126 | 25.6 | c | 17 | 123 | 76 | 38.4 | D | 15 | $95 \mid$ | 76 | 36.6 | D | 14 | 971 | 75 | 38.3 | D | 15 | 105 | 76 | 39.9 | D | 16 | 112 | 76 | 31.9 | c | 11 | 96 |
|  |  | SBL | 547 | 51.7 | D | 97 | 320 | 430 | 56.0 | E | 76 | 252 | 431 | 56.3 | E | 76 | 250 | 432 | 55.3 | E | 75 | 250 | 429 | 56.1 | E | 75 | 243 | 433 | 55.5 | E | 74 | 254 |
|  |  | SBT | 17 | 41.2 | D | 97 | 320 | 8 | 43.7 | D | 76 | 252 | 8 | 37.2 | D | 76 | 250 | 8 | 43.4 | D | 75 | 250 | 8 | 44.5 | D | 75 | 243 | 8 | 37.6 | D | 74 | 254 |
|  |  | SBR | 190 | 15.8 | B | 108 | 335\| | 162 | 14.6 | B | 87 | 267 | 163 | 13.7 | B | 87 | 265 | 163 | 14.0 | B | 86 | 265 | 163 | 13.8 | B | 87 | 258 | 163 | 13.8 | B | 85 | 269 |
|  |  | EBL | 124 | 92.6 | F | 2920 | 3686\| | 108 | 78.9 | E | 1979 | 2914 | 106 | 78.7 | E | 1845 | 2825 | 107 | 80.1 | F | 1949 | 2911 | 107 | 81.3 | F | 1911 | 2829 | 107 | 81.0 | F | 2020 | 2945 |
|  |  | EBT | 1473 | 80.7 | F | 3008 | 3716\| | 1612 | 75.0 | E | 2102 | 3013 | 1609 | 72.9 | E | 2114 | 3022 | 1599 | 75.2 | E | 2128 | 3088 | 1600 | 75.0 | E | 2086 | 2994 | 1611 | 73.9 | E | 2170 |  |
|  |  | EBR | 47 | 71.4 | E | 238 | 330\| | 30 | 59.0 | E | 523 | 774 | 30 | 58.5 | E | 538 | 760 | 30 | 59.5 | E | 569 | 968 \| | 31 | 57.7 | E | 730 | 983 | 30 | 60.6 | E | 258 | 482 |
|  |  | WBL | 77 | 41.2 | D | 14 | 104 | 56 | 34.1 | c | 7 | 67 | 56 | 33.2 | c | 6 | 75 | 56 | 33.6 | c | 7 | $70 \mid$ | 56 | 34.4 | c | 7 | 77) | 57 | 36.1 | D | 7 | 80 |
|  |  | WBT | 1115 | 30.4 | c | 138 | 693 | 1292 | 26.5 | c | 139 | 696 | 1288 | 27.3 | c | 146 | 711 | 1296 | 27.8 | c | 155 | 762 | 1293 | 25.7 | c | 128 | 680 | 1293 | 26.2 | c | 135 | 674 |
|  |  | WBR | 298 | 13.2 | B | 19 | 188\| | 246 | 12.3 | B | 13 | 168 | 245 | 12.2 | B | 12 | 159 | 246 | 13.0 | B | 12 | 164 | 246 | 11.8 | B | 12 | 167 | 246 | 11.8 | B | 13 | 164 |
|  |  | Overall |  | 52.2 | D |  |  |  | 49.1 | D |  |  |  | 48.6 | D |  |  |  | 49.7 | D |  |  |  | 48.8 | D |  |  |  | 48.4 | D |  |  |
| SR 326 at I 75 SB Slip \&Loop Ramps | u | NBR | 56 | 11.7 | B | 6 | 89 | 51 | 10.0 | A | S | 88 | 51 | 10.1 | B | 5 | 88 | 52 | 9.9 | A | 5 | 87 | 51 | 10.4 | B | 5 | 87 | 51 | 10.1 | B | 5 | 88 |
|  |  | EBT | 757 | 1.7 | A | 0 | 12 | 631 | 1.4 | A | 0 | 22 | 631 | 1.4 | A | 0 | 14 | 629 | 1.4 | A | 0 | 14 | 631 | 1.4 | A | 0 | 19 | 631 | 1.4 | A | 0 | 25 |
|  |  | EBR | 53 | 1.1 | A | 0 | 12 | 57 | 1.2 | A | 0 | 22 | 56 | 1.2 | A | 0 | 14 | 56 | 1.2 | A | 0 | 14 | 56 | 1.3 | A | 0 | 19 | 57 | 1.3 | A | 0 | 25 |
|  |  | WBL | 51 | 14.9 | B | 10 | 153\| | 50 | 8.6 | A | 6 | 133 | 51 | 9.1 | A | 6 | 133 | 50 | 9.2 | A | 6 | 141\| | 51 | 9.4 | A | 6 | 144 | 49 | 9.3 | A | 7 |  |
|  |  | WBT | 492 | 1.9 | A | 4 | 135 | 372 | 3.3 | A | 3 | 136 | 369 | 3.6 | A | 3 | 158 | 371 | 3.2 | A | 4 | 161 | 371 | 3.1 | A | 3 | 130 | 370 | 2.9 | A | 3 | 153 |
|  |  | WBR | 753 | 3.7 | A | 4 | 135 | 892 | 5.5 | A | 3 | 136 | 895 | 5.6 | A | 3 | 158 | 889 | 5.5 | A | 4 | 161 | 898 | 5.2 | A | 3 | 130 | 891 | 5.3 | A | 3 | 153 |
|  |  | wbu | 99 | 16.8 | B | 14 | 137\| | 98 | 10.6 | B | 8 | 115 | 98 | 11.4 | B | 9 | 120 | 97 | 10.9 | B | 9 | 123\| | 99 | 11.2 | B | 10 | 127 | 98 | 10.9 | B | 9 | 124 |
|  |  | Overall |  | 3.7 | A |  |  |  | 4.3 | A |  |  |  | 4.4 | A |  |  |  | 4.3 | A |  |  |  | 4.2 | A |  |  |  | 4.2 | A |  |  |
| US 27 at NW38 Ave | u | NBL | 1486 | 0.9 | A | 0 | 25 | 1585 | 0.9 | A | 1 | 34 | 1574 | 0.9 | A | , | 53 | 1587 | 1.0 | A | 1 | 44 | 1585 | 0.9 | A | 8 | ${ }^{37}$ | 1585 | 0.9 | A | 0 | 25 |
|  |  | NBR | 25 | 613.0 | F | 233 | 336 | 21 | 968.6 | F | 389 | 503 | 25 | 914.4 | F | 365 | 482 | 24 | 857.3 | F | 353 | 463 | 22 | 1002.5 | F | 388 | 499 | 23 | 957.0 | F | 373 | 487 |
|  |  | EBT | 2095 | 24.3 | C | 692 | 1609 | 2040 | 29.3 | c | 1178 | 2076 | 2048 | 27.8 | C | 1034 | 1875 | 2036 | 29.0 | C | 1018 | 1869 | 2042 | 28.8 | C | 1049 | 1895 | 2057 | 27.5 | C | 1059 | 1925 |
|  |  | EBR | 11 | 12.0 | B | 692 | 1609 | 21 | 22.3 | c | 1178 | 2076 | 22 | 17.5 | B | 1034 | 1875 | 22 | 18.8 | B | 1018 | 1869 | 21 | 17.6 | B | 1049 | 1895 | 22 | 16.6 | B | 1059 | 1925 |
|  |  | WBL | 31 | 34.4 | c | 7 | 52 | 42 | 34.4 | c | 8 | 61 | 43 | 39.9 | D | 10 | 67 | 42 | 36.0 | D | 9 | 64 | 41 | 36.9 | D | 9 | 63 | 43 | 34.3 | c | 8 | 60 |
|  |  | WBT | 10 | 110.9 | F | 1 |  | 11 | 296.8 | F | 1 | 66 | 13 | 276.9 | F | 1 | 70 | 13 | 288.3 | F | 1 | 67 | 12 | 314.3 | F | 1 | 62 | 12 | 290.2 | F | 1 | 63 |
|  |  | Overall |  | 17.4 | B |  |  |  | 20.9 | c |  |  |  | 20.6 | c |  |  |  | 20.4 | c |  |  |  | 21.1 | c |  |  |  | 19.6 | B |  |  |
| $\underset{\substack{\text { NW } 49 \text { St at } \\ \text { I-75 SB }}}{ }$ | s | EBT |  |  |  |  |  | 454 | 22.4 | C | 43 | 208 | 232 | 33.1 | C | 29 | 144 | 455 | 28.2 | C | 52 | 269 | 454 | 28.3 | C | 50 | 250 | 456 | 12.6 | B | 20 | 218 |
|  |  | EBR |  |  |  |  |  | 509 | 3.1 | A | 4 | 132 | 510 | 3.9 | A | 1 | 94 | 511 | 3.6 | A | 4 | 143\| | 510 | 3.0 | A | 3 | 114 | 512 | 2.8 | A | 8 | 201 |
|  |  | WBL |  |  |  |  |  | 747 | 6.3 | A | 17 | 167 | 343 | 37.7 | D | 48 | 177 | 745 | 12.9 | B | 33 | 264 | 752 | 6.9 | A | 17 | 150\| | 344 | 24.9 | c | 89 | 421 |
|  |  | WBT |  |  |  |  |  | 343 | 48.9 | D | 63 | 182 | 314 | 17.6 | B | 20 | 127 | 342 | 42.7 | D | 55 | 168 | 342 | 37.7 | D | 49 | 190 | 746 | 45.0 | D | 180 | 557 |
|  |  | SBL |  |  |  |  |  | 166 | 34.3 | c | 36 | 185 | 166 | 33.9 | c | 26 | 117 | 166 | 34.1 | c | 35 | 175 | 168 | 35.1 | D | 37 | 189 | 167 | 24.1 | c | 27 | 166 |
|  |  | SBR |  |  |  |  |  | 180 | 9.8 | A | 16 | 161 | 180 | 10.2 | B | 17 | 149 | 180 | 9.4 | A | 16 | $154 \mid$ | 181 | 9.7 | A | 16 | 159 | 179 | 14.9 | B | 17 | 161 |
|  |  | Overall |  |  |  |  |  |  | 16.9 | B |  |  |  | 5.5 | A |  |  |  | 19.3 | B |  |  |  | 16.7 | B |  |  |  | 23.3 | c |  |  |
| $\underset{\substack{\text { NW } 49 ~ S t ~ a t ~ \\ \text { I-75 NB }}}{ }$ | s | EBL |  |  |  |  |  | 223 | 21.7 | C | 0 | 2 | 224 | 31.2 | C | 27 | 151 | 224 | 0.6 | A | 0 | 13 | 223 | 8.3 | A |  | 126 | 223 | 4.2 | A | 5 | 90 |
|  |  | EBT |  |  |  |  |  | 398 | 7.4 | A | 10 | 143 | 232 | 33.1 | c | 29 | 144 | 396 | 4.3 | A | 7 | 82 | 692 | 0.1 | A | 0 | 39 | 398 | 31.5 | c | 54 | 237 |
|  |  | WBR |  |  |  |  |  | 182 | 0.6 | A | 0 | 3 | 182 | 1.0 | A | 0 | 29 | 182 | 0.6 | A | 23 | 39 | 182 | 0.3 | A | 0 | 0 | 182 | 0.4 105 | A | 0 | 4 192 |
|  |  | WBT |  |  |  |  |  | 658 | 18.2 | B | 48 | 258 | 314 | 17.6 | B | 20 | 127 | 841 | 8.3 | A | 23 | 197 | 659 | 0.4 | A | 0 | 20 | 659 | 10.5 | B | 24 | 192 |
|  |  | NBL |  |  |  |  |  | 433 | 32.9 | C | 56 |  | 430 | 37.7 | D | 61 | 221 | 432 | 31.8 | C | 55 | 216 | 438 | 34.9 | C | 147 | 409 | 431 | 36.7 | D | 64 | 228 |
|  |  | NBR |  |  |  |  |  | 304 | 9.2 | A | 25 | 182 | 302 | 9.2 | A | 26 | 192 | 303 | 8.6 | A | 5 | 151 | 296 | 13.7 | B | 38 | 203 |  | 8.8 | A | 15 | 184 |
|  |  | Overall |  |  |  |  |  |  | 16.8 | B |  |  |  | 5.5 | A |  |  |  | 12.7 | B |  |  |  | 8.3 | A |  |  |  | 17.8 | B |  |  |

Table 6-8: 2045 Vissim Intersection Delay \& LOS Summary (PM Peak)

| Intersection | Control | mvmт | No Build |  |  |  |  | Diamond |  |  |  |  | SPUI 2045 PM Peak ${ }^{1}$ Parclo SE |  |  |  |  |  |  |  |  |  | Parclo NE |  |  |  |  | DDI |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | LOS | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ |
| NW 49 St at NW 44 Ave | s | NBL | 10 | 26.5 | c | , | 31 | 13 | 28.3 | C | ${ }^{2}$ | 29 | 13 | 28.7 | c | , | 30 | 13 | 28.3 | C | , | 31 | 13 | 28.6 | C | , | 29 | 13 | 26.8 | C | - |  |
|  |  | NBT | 328 | 30.0 | c | 58 | 265 | 283 | 31.6 | c | 33 | 148 | 284 | 32.4 | c | 34 | 147\| | 282 | 31.4 | c | 33 | 148 | 283 | 32.1 | c | 34 | 146 | 279 | 32.5 | c | 34 | 151 |
|  |  | NBR | 218 | 21.4 | c | 0 | 11 | 412 | 10.3 | B | 0 | 20 | 413 | 10.3 | B | 0 | 18 | 412 | 10.1 | B | 0 | 19 | 413 | 10.5 | B | 0 | 21 | 411 | 10.6 | B | 0 | 23 |
|  |  | SBL | 250 | 16.1 | B | 21 | 176 | 520 | 40.1 | D | 92 | 410 | 519 | 39.7 | D | 90 | 394 | 519 | 39.0 | D | 88 | 396 | 518 | 40.0 | D | 91 | 384 | 521 | 39.4 | D | 88 | 391 |
|  |  | SBT | 295 | 11.8 | B | 11 | 104 | 300 | 12.8 | B | 13 | 122 | 300 | 13.4 | B | 14 | 118 | 300 | 12.5 | B | 12 | 112 | 300 | 13.2 | B | 13 | 112 | 301 | 12.7 | B | 12 | 114 |
|  |  | SBR | 8 | 8.0 | A | 27 | 156 | 5 | 14.4 | B | 13 | 122 | 5 | 14.5 | B | 14 | 118\| | 5 | 13.7 | B | 12 | 112 | 5 | 14.5 | B | 13 | 112 | 5 | 11.5 | B | 12 | 114 |
|  |  | EBL | 4 | 32.0 | c | 3 | 41 | 4 | 45.3 | D | 5 | 59 | 4 | 45.3 | D | 5 | 59\| | 4 | 45.3 | D | 5 | 59 | 4 | 45.3 | D | 5 | 59 | 4 | 59.3 | E | 6 |  |
|  |  | EBT | 9 | 39.1 | D | 3 | 41 | 12 | 46.6 | D | 5 | 59 | 12 | 46.6 | D | 5 | 59\| | 12 | 46.6 | D | 5 | 59 | 12 | 46.6 | D | 5 | 59 | 12 | 43.8 | D | 6 | 57 |
|  |  | EBR | 12 | 7.1 | A | 6 | 61 | 15 | 9.2 | A | 3 | 90 | 15 | 9.3 | A | 3 | 90\| | 15 | 9.4 | A | 3 | 90 | 15 | 9.3 | A | 3 | 90 | 15 | 11.8 | B | 3 | 88 |
|  |  | WBL | 300 | 29.7 | c | 104 | 403 | 360 | 39.2 | D | 56 | 199 | 363 | 25.9 | c | 37 | 182 | 362 | 45.6 | D | 61 | 205 | 357 | 31.1 | C | 45 | 195 | 361 | 37.2 | D | 51 | 224 |
|  |  | WBT | 20 | 40.4 | D | 104 | 403 | 18 | 49.0 | D | 107 | 337 | 18 | 33.3 | c | 63 | 308\| | 18 | 57.3 | E | 117 | 397 | 19 | 38.5 | D | 83 | 300 | 18 | 44.8 | D | 98 | 390 |
|  |  | WBR | 414 | 26.7 | c | 124 | 429 | 576 | 45.5 | D | 107 | 337 | 579 | 28.6 | c | 63 | 308 | 580 | 52.3 | D | 117 | 397 | 574 | 36.9 | D | 83 | 300 | 579 | 42.3 | D | 98 | 390 |
|  |  | Overall |  | 23.5 | c |  |  |  | 32.0 | c |  |  |  | 26.2 | c |  |  |  | 34.2 | c |  |  |  | 28.8 | c |  |  |  | 31.0 | c |  |  |
| SR 326 at NW 44 Ave | s | NBL | 82 | 154.7 | F | 589 | 777 | 40 | 25.5 | c | 18 | 150 | 40 | 27.6 | c | 18 | 152 | 39 | 26.5 | c | 17 | 147 | 41 | 27.2 | c | 18 | 150 | 41 | 25.5 | c | 17 | 150 |
|  |  | NBR | 319 | 196.5 | F | 587 | 773 | 129 | 30.0 | c | 26 | 145 | 129 | 29.6 | c | 25 | 147\| | 128 | 30.0 | c | 25 | 142 | 128 | 30.6 | c | 26 | 145 | 130 | 29.4 | c | 25 | 145 |
|  |  | SBL | 326 | 41.5 | D | 124 | 489 | 307 | 26.8 | c | 59 | 307 | 306 | 25.9 | c | 56 | 296 | 305 | 26.7 | c | 59 | 299 | 305 | 26.0 | c | 57 | 303 | 307 | 26.0 | c | 57 | 288 |
|  |  | SBT | 61 | 45.4 | D | 124 | 489 | 21 | 28.9 | c | 59 | 307 | 21 | 28.1 | c | 56 | 296 | 21 | 27.9 | c | 59 | 299 | 21 | 27.7 | c | 57 | 303 | 21 | 30.0 | c | 57 |  |
|  |  | SBR | 178 | 4.2 | A | 1 | 57 | 170 | 2.4 | A | 1 | 64 | 170 | 2.5 | A | 1 | 56 | 170 | 2.5 | A | 1 | 61 | 170 | 2.5 | A | 1 | 64 | 170 | 2.3 | A | , |  |
|  |  | EBT | 462 | 22.5 | c | 47 | 244 | 424 | 19.7 | B | 34 | 196 | 421 | 19.7 | B | 34 | 199\| | 425 | 19.9 | B | 35 | 197\| | 423 | 20.0 | B | 35 | 206 | 422 | 19.8 | B | 35 | 193 |
|  |  | EBR | 60 | 16.9 | B | 1 | 48 | 25 | 13.3 | B | 0 | 12 | 24 | 12.9 | B | 0 | 13\| | 24 | 14.8 | B | 0 |  | 24 | 15.6 | B | 0 | 15 | 24 | 14.1 | B | 0 |  |
|  |  | WBL | 189 | 47.4 | D | 54 | 225 | 86 | 25.0 | c | 10 | 101 | 88 | 25.4 | c | 10 | 102 | 87 | 24.9 | c | 9 | 99 | 87 | 24.5 | c | 9 | 108 | 86 | 24.6 | c | 9 | 102 |
|  |  | WBT | 357 | 22.2 | c | 35 | 185 | 413 | 21.9 | c | 38 | 185 | 416 | 21.7 | c | 37 | 191\| | 415 | 22.2 | c | 38 | 179 | 420 | 22.2 | c | 40 | 197 | 411 | 21.1 | c | 37 | 185 |
|  |  | Overall |  | 59.2 | E |  |  |  | 21.1 | c |  |  |  | 20.8 | c |  |  |  | 21.2 | c |  |  |  | 21.1 | c |  |  |  | 20.6 | c |  |  |
| SR 326 at I-75 NB | s | NBL | 242 | 37.1 | D | 56 | 258 | 186 | 33.5 | c | 40 | 208 | 186 | 33.5 | c | 39 | 205 | 188 | 33.4 | C | 40 | 217 | 192 | 33.6 | c | 41 | 216 | 187 | 33.2 | C | 39 | 220 |
|  |  | NBR | 1055 | 14.5 | B | 167 | 1107\| | 1114 | 9.6 | A | 58 | 735 | 1115 | 10.2 | B | 66 | 795 | 1114 | 9.6 | A | 59 | 808 | 1113 | 9.8 | A | 69 | 838 | 1114 | 9.8 | A | 62 | 795 |
|  |  | EBL | 206 | 25.9 | c | 32 | 232 | 162 | 23.5 | c | 19 | 183 | 162 | 22.6 | c | 17 | 182 | 162 | 23.1 | c | 18 | 175 | 161 | 23.0 | c | 17 | 179 | 162 | 23.7 | c | 18 | 181 |
|  |  | EBT | 686 | 7.2 | A | 13 | 150\| | 497 | 6.6 | A | 9 | 133 | 497 | 6.3 | A | 8 | 123\| | 496 | 6.7 | A | 9 | 126 | 499 | 6.1 | A | 8 | 124 | 496 | 6.4 | A | 8 | 124 |
|  |  | WBT | 1141 | 55.4 | E | 4379 | 4874 | 1296 | 43.6 | D | 3371 | 4277\| | 1304 | 42.3 | D | 3077 | 4049 | 1294 | 43.0 | D | 3057 | 4013 | 1318 | 41.8 | D | 2619 | 3734 | 1299 | 42.8 | D | 3210 | 4081 |
|  |  | WBR | 446 | 48.4 | D | 4312 | 4805 | 495 | 37.0 | D | 3250 | 4189 | 502 | 36.6 | D | 2606 | 3681 | 498 | 37.3 | D | 2933 | 3923 | 506 | 35.2 | D | 1913 | 2903 | 499 | 36.0 | D | 2620 | 3547 |
|  |  | Overall |  | 31.5 | c |  |  |  | 26.3 | c |  |  |  | 25.9 | c |  |  |  | 26.1 | c |  |  |  | 25.5 | c |  |  |  | 25.9 | c |  |  |
| $\underset{\text { SB }}{\text { US } 27 \text { at } 1-75}$ | s | SBL | 130 | 49.8 | D | 39 | 194 | 190 | 56.4 | E | 80 | 314 | 191 | 53.5 | D | 78 | 307 | 190 | 53.1 | D | 75 | 299 | 191 | 52.3 | D | 69 | 283 | 189 | 56.2 | E | 82 | 302 |
|  |  | SBR | 90 | 3.1 | A | 0 |  | 137 | 9.5 | A | 0 | 6 | 137 | 9.7 | A | 0 | 3 | 138 | 9.3 | A | 0 | 0 | 139 | 6.8 | A | 0 | 0 | 137 | 10.6 | B | 0 |  |
|  |  | EBT | 1245 | 38.2 | D | 262 | 736 | 1256 | 28.7 | c | 175 | 674 | 1264 | 29.6 | c | 187 | $672 \mid$ | 1259 | 31.0 | c | 189 | 658 | 1252 | 29.2 | c | 175 | 658 | 1250 | 28.6 | c | 175 | 668 |
|  |  | EBR | 553 | 22.3 | c | 96 | 597 | 503 | 26.8 | c | 104 | 506 | 504 | 20.7 | c | 72 | 489 | 505 | 22.9 | c | 77 | 501 | 498 | 27.2 | c | 96 | 523 | 497 | 25.3 | c | 93 | 487 |
|  |  | WBL | 547 | 15.3 | B | 77 | 402 | 508 | 20.5 | c | 88 | 401 | 514 | 15.7 | B | 71 | 396\| | 513 | 16.9 | B | 74 | 397\| | 507 | 18.5 | B | 79 | 397 | 507 | 18.2 | B | 79 | 393 |
|  |  | WBT | 1900 | 14.6 | B | 89 | 382 | 1879 | 8.2 | A | 51 | 338 | 1892 | 5.9 | A | 41 | 3291 | 1897 | 9.6 | A | 59 | 339 | 1892 | 6.4 | A | 43 | 339 | 1879 | 8.5 | A | 53 | 348 |
|  |  | Overall |  | 23.0 | c |  |  |  | 19.7 | B |  |  |  | 17.6 | B |  |  |  | 19.8 | B |  |  |  | 18.3 | B |  |  |  | 19.2 | B |  |  |
| $\underset{N B}{ } \underset{\text { NB }}{27}$ at $1-75$ | s | NBL | 613 | 45.5 | D | 166 | 501 | 550 | 32.4 | C | 67 | 256 | 550 | 31.3 | C | 65 | 255 | 549 | 34.5 | C | 72 | 282 | 550 | 31.0 | C | 64 | 250 | 549 | 32.4 | C | 67 | 262 |
|  |  | NBR | 626 | 55.1 | E | 163 | 633 | 556 | 34.1 | c | 55 | 227 | 558 | 32.4 | c | 51 | 224 | 555 | 40.2 | D | 67 | 289 | 556 | 31.5 | c | 51 | 223 | 556 | 33.4 | c | 52 | 215 |
|  |  | EBL | 71 | 27.3 | c | 4 | 58 | 100 | 26.6 | c | 7 | 86 | 101 | 27.1 | c | 8 | 901 | 100 | 29.0 | c | 9 | 97\| | 99 | 26.1 | c | 7 | 95 | 100 | 27.5 | c | 8 |  |
|  |  | EBT | 1297 | 27.8 | c | 52 | 320 | 1339 | 15.6 | B | 27 | 255 | 1356 | 15.3 | B | 25 | 253 | 1341 | 19.2 | B | 34 | 276 | 1337 | 14.4 | B | 26 | 259 | 1337 | 14.9 | B | 26 | 247 |
|  |  | WBT | 1291 | 31.6 | c | 137 | 738 | 1335 | 25.7 | c | 105 | 661 | 1346 | 24.0 | c | 98 | 631 | 1352 | 25.3 | c | 108 | 682 | 1344 | 24.6 | c | 104 | 667 | 1338 | 26.0 | c | 110 | 676 |
|  |  | WBT>L | 548 | 59.7 | E | 300 | 1030 | 508 | 53.3 | D | 222 | 848 | 518 | 45.5 | D | 180 | $760 \mid$ | 516 | 47.7 | D | 185 | 785 | 510 | 47.5 | D | 187 | 773 | 510 | 51.1 | D | 205 | 772 |
|  |  | WBR | 141 | 17.7 | B | 0 | 22 | 181 | 15.5 | B | 0 |  | 180 | 14.9 | B | 0 | 35\| | 182 | 14.4 | B | 0 | 36 | 183 | 14.4 | B | 0 | 39 | 179 | 15.2 | B | 0 | 31 |
|  |  | Overall |  | 38.5 |  |  |  |  | 27.2 | c |  |  |  | 25.5 | c |  |  |  | 28.6 | c |  |  |  | 25.4 | c |  |  |  | 26.8 | c |  |  |

Volume in vph; delay in sec/veh; LOS is Estimated LOS using HCM2010 thresholds; Queue Lengths in feet

| Intersection | Control | мvmт | No Build |  |  |  |  | Diamond |  |  |  |  | SPUI 2045 PM Peak ${ }^{1}$ |  |  |  |  |  |  |  |  |  | Parclo NE |  |  |  |  | DDI |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Vol | Delay | LoS | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ | Vol | Delay | Los | AvgQ | MaxQ |
| US 27 at NW 35 Ave Rd | s | NBL | 35 | 78.2 | E | 23 | 132 | 36 | 79.1 | E | 23 | 134 | 35 | 77.8 | E | 25 | 135 | 36 | 78.6 | E | 23 | 132 | 36 | 78.4 | E | 24 | 132 | 35 | 78.6 | E | 24 | 132 |
|  |  | NBT | 11 | 70.9 | E | 23 | 132 | 9 | 64.2 | E | 23 | $134 \mid$ | 9 | 75.7 | E | 25 | 135 | 9 | 66.6 | E | 23 | 132 | 9 | 68.2 | E | 24 | 132 | 9 | 67.0 | E | 24 | 132 |
|  |  | NBR | 16 | 35.0 | c | 30 | 147\| | 17 | 31.6 | c | 30 | 149 | 17 | 28.9 | c | 32 | 150 | 17 | 31.4 | c | 30 | 148\| | 17 | 33.2 | c | 31 | 148 | 17 | 33.0 | c | 31 | 148 |
|  |  | SBL | 220 | 121.0 | F | 236 | 720 | 199 | 121.7 | F | 259 | 601 | 202 | 113.8 | F | 207 | 522 | 203 | 116.2 | F | 220 | $539 \mid$ | 202 | 109.0 | F | 120 | 398 | 201 | 110.5 | F | 295 | 644 |
|  |  | SBT | 10 | 113.4 | F | 6 | 43 | 8 | 106.9 | F | 4 | 34 | 8 | 94.9 | F | 3 | 32 | 8 | 99.8 | F | 3 | 33\| | 8 | 94.7 | F | 3 | 31 | 8 | 101.7 | F | 3 | 32 |
|  |  | SBR | 664 | 107.0 | F | 799 | 1359\| | 691 | 112.2 | F | 981 | 1499\| | 700 | 102.9 | F | 883 | 1416 | 701 | 107.2 | F | 884 | 1390\| | 698 | 103.4 | F | 885 | 1421\| | 691 | 98.6 | F | 819 | 1362 |
|  |  | EBL | 490 | 59.9 | E | 473 | 1109\| | 497 | 51.9 | D | 325 | 1059 | 503 | 53.3 | D | 324 | 1061 | 498 | 57.0 | E | 390 | 1114 | 495 | 52.5 | D | 314 | 1052 | 501 | 53.7 | D | 324 | 1122 |
|  |  | EBT | 1396 | 15.7 | B | 55 | 632 | 1360 | 13.3 | B | 32 | 451 | 1373 | 13.8 | B | 49 | 608 | 1357 | 14.7 | B | 46 | 495\| | 1356 | 13.9 | B | 48 | 607 | 1360 | 13.9 | B | 38 | 543 |
|  |  | EBR | 33 | 12.1 | B | 0 | 41 | 34 | 8.9 | A | 0 | 34 | 34 | 9.9 | A | 0 | 37 | 33 | 9.6 | A | 0 | 33 | 34 | 10.0 | A | 0 | 43 | 35 | 9.4 | A | 0 | 39 |
|  |  | WBL | 24 | 55.8 | E | 1 | 35 | 25 | 52.7 | D | 2 | 39 | 24 | 49.6 | D | 2 | 35 | 25 | 53.3 | D | 2 | 37) | 24 | 47.4 | D | 1 | 371 | 24 | 52.0 | D | 1 | 35 |
|  |  | WBT | 1283 | 88.3 | F | 2692 | 2976 | 1301 | 87.2 | F | 2688 | 2979 | 1311 | 85.6 | F | 2691 | 2976 | 1318 | 84.5 | F | 2686 | 2978 | 1313 | 86.7 | F | 2689 | 2977\| | 1304 | 86.5 | F | 2686 | 2979 |
|  |  | WBR | 223 | 44.4 | D | 2359 | 2643 | 195 | 44.7 | D | 2354 | 2645 | 194 | 43.3 | D | 2357 | 2642 | 197 | 42.8 | D | 2352 | 2645 | 194 | 43.3 | D | 2355 | 2643 | 195 | 41.6 | D | 2353 | 2645 |
|  |  | Overall |  | 63.3 | E |  |  |  | 62.4 | E |  |  |  | 60.5 | E |  |  |  | 61.8 | E |  |  |  | 60.8 | E |  |  |  | 59.7 | E |  |  |
| US 27 at NW44 Ave | s | NBL | 61 | 55.8 | E | 20 | 94 | 40 | 52.9 | D | 13 | 73 | 39 | 51.6 | D | 13 | 73 | 39 | 50.7 | D | 12 | 72 | 39 | 54.4 | D | 13 | 72 | 39 | 53.8 | D | 13 | 72 |
|  |  | NBT | 7 | 59.8 | E | 2 | $20 \mid$ | 4 | 51.6 | D | 1 | 15\| | 4 | 55.5 | E | 1 | 15 | 4 | 55.4 | E | 1 | 15\| | 4 | 57.9 | E | 1 | 16 | 4 | 59.0 | E | 1 | 15 |
|  |  | NBR | 150 | 9.9 | A | 8 | 115 | 87 | 6.8 | A | 3 | 59 | 88 | 6.6 | A |  | 60 | 87 | 7.1 | A | 3 | 64 | 87 | 9.3 | A | 4 | 71 | 87 | 7.2 | A | 4 | 68 |
|  |  | SBL | 422 | 48.3 | D | 79 | 268 \| | 334 | 45.3 | D | 62 | 214 | 335 | 45.3 | D | 61 | 209 | 334 | 45.1 | D | 60 | 199 | 333 | 45.3 | D | 61 | 202 | 334 | 45.6 | D | 61 | 201 |
|  |  | SBT | 13 | 35.4 | D | 79 | 268 | 5 | 33.2 | c | 62 | 214 | 6 | 42.0 | D | 61 | 209 | 6 | 37.5 | D | 60 | 199\| | 6 | 38.6 | D | 61 | 202 | 6 | 36.1 | D | 61 | 201 |
|  |  | SBR | 207 | 19.8 | B | 90 | 282 | 173 | 17.9 | B | 73 | 229 \| | 172 | 19.0 | B | 73 | 224 | 173 | 18.6 | B | 72 | 214 | 173 | 18.8 | B | 72 | 216 | 173 | 17.8 | B | 72 | 216 |
|  |  | EBL | 184 | 136.4 | F | 1402 | 2176 | 159 | 74.4 | E | 253 | 915 | 158 | 74.8 | E | 251 | 930 | 161 | 75.4 | E | 232 | 889 | 159 | 77.5 | E | 272 | 980 | 159 | 75.6 | E | 225 | 910 |
|  |  | EBT | 1241 | 71.4 | E | 1380 | 2157\| | 1354 | 30.6 | c | 258 | 930 | 1353 | 30.6 | c | 249 | 919 | 1358 | 29.6 | c | 231 | 878 | 1346 | 33.4 | c | 265 | 997 | 1349 | 30.1 | c | 226 | 913 |
|  |  | EBR | 49 | 61.8 |  | 30 | 52 | 33 | 27.7 | c | 0 | $0 \mid$ | 33 | 26.4 | c | 0 |  | 34 | 26.9 | c | 0 | 0 | 34 | 28.6 | c | 0 | 0 | 34 | 25.7 | c | 0 |  |
|  |  | WBL | 61 | 48.0 | D | 7 | 89 | 39 | 37.6 | D | 4 | 55 | 39 | 35.2 | D | 4 | 55 | 39 | 36.2 | D | 3 | 55 | 39 | 38.4 | D | 4 | 57 | 39 | 35.2 | D | 3 | 51 |
|  |  | WBT | 1526 | 60.1 | E | 1793 | 2432 | 1654 | 48.3 | D | 1066 | 1874\| | 1657 | 47.1 | D | 886 | 1743 | 1674 | 49.0 | D | 1234 | 2027 | 1667 | 51.0 | D | 1083 | 1985\| | 1668 | 48.4 | D | 1047 | 1853 |
|  |  | WBR | 366 | 37.3 | D | 37 | 244 | 287 | 28.2 | c | 20 | 185\| | 288 | 27.1 | c | 20 | 181 | 292 | 29.1 | c | 20 | 180 | 290 | 30.1 | c | 22 | 187\| | 290 | 28.7 | c | 20 | 180 |
|  |  | Overall |  | 59.5 | E |  |  |  | 39.6 | D |  |  |  | 39.1 | D |  |  |  | 39.7 | D |  |  |  | 41.9 | D |  |  |  | 39.6 | D |  |  |
| SR 326 at I 75 SB Slip \& Loop Ramps | u | NBR | 34 | 11.1 | B | 3 | 75 | 31 | 9.6 | A | 3 | 73 | 31 | 9.6 | A | 3 | 72 | 31 | 9.1 | A | 3 | 73 | 31 | 8.8 | A | 3 | 74 | 31 | 9.2 | A | 3 | 71 |
|  |  | EBT | 812 | 1.1 | A | 0 | 7 | 582 | 0.9 | A | 0 | $10 \mid$ | 580 | 0.9 | A | 0 | 20 | 580 | 0.9 | A | 0 | 12 | 581 | 0.9 | A | 0 | $13 \mid$ | 581 | 0.9 | A | 0 | 12 |
|  |  | EBR | 28 | 1.0 | A | 0 | 7 | 38 | 1.1 | A | 0 | 10 | 38 | 1.1 | A | 0 | 20 | 38 | 1.0 | A | 0 | 12 | 38 | 1.1 | A | 0 | $13 \mid$ | 38 | 1.0 | A | 0 | 12 |
|  |  | WBL | 10 | 11.5 | B | 2 | 85 | 32 | 6.7 | A | 1 | 75 | 33 | 6.2 | A | 2 | 77 | 32 | 6.8 | A | 1 | 73\| | 32 | 6.3 | A |  | 81 | 32 | 6.9 | A | 1 | 72 |
|  |  | WBT | 548 | 2.3 | A | 5 | 161 | 502 | 3.6 | A | 4 | 155 | 504 | 3.5 | A | 4 | 177 | 502 | 3.4 | A | 3 | 153 | 508 | 3.7 | A | 3 | 146 | 501 | 3.7 | A | 3 | 139 |
|  |  | WBR | 756 | 4.4 | A | 5 | 161 | 874 | 5.5 | A | 4 | 155 | 880 | 5.6 | A | 4 | 177 | 874 | 5.5 | A | 3 | 153\| | 890 | 5.6 | A | 3 | 146 | 877 | 5.6 | A | 3 | 139 |
|  |  | wBu | 49 | 14.0 | B | 5 | 74 | 46 | 7.5 | A | 3 | 65 | 47 | 8.2 | A | 3 |  | 46 | 7.5 | A | 3 | 63 | 47 | 8.0 | A | 3 | 82 | 45 | 8.0 | A | 2 |  |
|  |  | Overall |  | 3.0 | A |  |  |  | 3.7 | A |  |  |  | 3.8 | A |  |  |  | 3.7 | A |  |  |  | 3.8 | A |  |  |  | 3.8 | A |  |  |
| US 27 at NW38 Ave 38 Ave | u | NBL | 1954 | 13.7 | B | 67 | 315 | 1974 | 5.4 | A | 20 | 141 | 1986 | 2.9 | A | 5 | 91 | 1994 | 7.6 | A | 32 | 218 | 1987 | 3.3 | A | 7 | 124 | 1974 | 5.1 | A | 22 | 141 |
|  |  | NBR | 25 | 191.8 | F | 41 | 116 | 36 | 75.2 | E | 21 | 98 | 37 | 73.0 | E | 21 | 101 | 37 | 79.3 | E | 19 | 93 | 37 | 62.0 | E | 18 | 92 | 37 | 45.4 | D | 13 | 86 |
|  |  | EBT | 1777 | 16.5 | B | 230 | 669 | 1731 | 9.8 | A | 77 | 374 | 1738 | 9.9 | A | 80 | 366 | 1731 | 10.0 | A | 88 | 334 | 1717 | 11.7 | B | 118 | 424 | 1714 | 9.3 | A | 51 | 318 |
|  |  | EBR | 24 | 9.3 | A | 230 | 669 | 34 | 6.0 | A | 77 | 374 | 33 | 6.8 | A | 80 | 366 | 33 | 5.6 | A | 88 | 334 | 33 | 7.2 | A | 118 | 424 | 33 | 6.1 | A | 51 | 318 |
|  |  | WBL | 24 | 59.4 | E | 18 | 86 | 37 | 40.0 | D | 13 | 81 | 38 | 17.9 | B | 4 | 57 | 37 | 44.4 | D | 20 | 130 | 38 | 18.8 | B | 5 | 57 | 38 | 33.7 | c | 16 | 104 |
|  |  | WBT | 23 | 190.4 | F | 37 | 118 | 21 | 60.7 | E | 8 |  | 22 | 20.5 | c | 3 |  | 22 | 99.6 | F | 11 | 93 | 23 | 22.1 | c | 3 |  | 22 | 82.5 | F | 7 |  |
|  |  | Overall |  | 17.3 | B |  |  |  | 8.7 | A |  |  |  | 7.1 | A |  |  |  | 10.1 | B |  |  |  | 7.8 | A |  |  |  | 8.1 | A |  |  |
| $\underset{\substack{\mathrm{NW} \\ \mathrm{I}-75 \mathrm{SB} \\ \mathrm{St} \\ \text { at }}}{ }$ | s | EBT |  |  |  |  |  | 508 | 18.2 | B | 35 | 251 | 320 | 33.0 | C | 40 | 189 | 507 | 29.9 | C | 61 | 256 | 507 | 20.1 | C | 39 | 219 | 509 | 12.3 | B | 21 | 202 |
|  |  | EBR |  |  |  |  |  | 435 | 2.0 | A | 1 | 77 | 435 | 3.0 | A | 1 | 56 | 436 | 2.4 | A | 2 | 93\| | 434 | 2.2 | A | 2 | 89 | 434 | 2.3 | A | 10 | 265 |
|  |  | WBL |  |  |  |  |  | 744 | 2.9 | A | , | 96 | 285 | 37.6 | D | 40 | 146 | 740 | 20.9 | c | 58 | 323\| | 726 | 6.9 | A | 16 | $147 \mid$ | 285 | 27.3 | c | 84 | 357 |
|  |  | WBT |  |  |  |  |  | 283 | 30.9 | c | 34 | 149 | 226 | 16.9 | B | 14 | 96 | 285 | 35.0 | c | 39 | $139 \mid$ | 287 | 42.7 | D | 46 | 162 | 739 | 46.9 | D | 176 | 493 |
|  |  | SBL |  |  |  |  |  | 196 | 34.5 | c | 42 | 215 | 195 | 32.9 | c | 29 | 124 | 195 | 35.0 | c | 43 | 212 | 195 | 39.2 | D | 49 | 248 | 196 | 26.4 | c | 34 | 207 |
|  |  | SBR |  |  |  |  |  | 217 | 10.0 | A | 20 | 177\| | 217 | 10.9 | B | 22 | 170 | 217 | 9.5 | A | 20 | 165 | 219 | 10.3 | B | 21 | 180 | 219 | 14.8 | B | 20 | 171 |
|  |  | Overall |  |  |  |  |  |  | 12.6 | B |  |  |  | 5.7 | A |  |  |  | 21.2 | c |  |  |  | 16.1 | B |  |  |  | 24.4 | c |  |  |
| $\underset{\mathrm{l}-75 \mathrm{NB}}{\mathrm{NW} 49 \mathrm{St}}$ | s | EBL |  |  |  |  |  | 190 | 29.5 | C | 0 |  | 189 | 31.2 | C | 25 | 132 | 187 | 0.4 | A | 0 | 7 | 194 | 4.2 | A | 1 | 56 | 189 | 9.1 | A | 15 | 177 |
|  |  | EBT |  |  |  |  |  | 517 | 5.8 | A | 8 | 152 | 320 | 33.0 | c | 40 | 189 | 515 | 12.1 | B | 23 | 155 | 861 | 0.1 | A | 0 | 25 | 516 | 36.3 | D | 84 | 328 |
|  |  | WBR |  |  |  |  |  | 157 | 0.5 | A | 38 |  | 158 | 0.7 | A | 0 | 16 | 157 | 0.6 | A | 1 | 44 | 158 | 0.2 | A | 0 | 0 | 157 | 0.2 | A | 0 | 0 |
|  |  | WBT |  |  |  |  |  | 512 | 18.6 | B | 38 | 222 | 226 | 16.9 | B | 14 | 96 | 671 | 9.0 | A | 19 | 173 | 512 | 1.5 | A | 2 | 76 | 511 | 9.7 | A | 18 | 161 |
|  |  | NBL |  |  |  |  |  | 517 | 31.1 | C | 62 |  | 516 | 37.8 | D | 72 | 251 | 518 | 30.3 | C | 61 | 238 | 501 | 101.6 | F | 606 | 942 | 516 | 37.9 | D | 78 | 256 |
|  |  | NBR |  |  |  |  |  | 350 | 9.9 | A | 30 | 215 | 350 | 10.2 | B | 33 | 203 | 350 | 9.3 | A | 10 | 182 | 349 | 19.3 | B | 65 | 254 |  | 10.1 | B | 20 | 209 |
|  |  | Overall |  |  |  |  |  |  | 16.8 | B |  |  |  | 5.7 | A |  |  |  | 15.2 | B |  |  |  | 23.9 | c |  |  |  | 21.8 | c |  |  |

NW 49th Street displays acceptable overall intersection LOS at NW 44th Avenue and both I-75 northbound and southbound ramp intersections. Under all scenarios, the overall LOS meets the LOS D target or performs better. However, it is worth noting that the northbound left-turn movement under the Parclo-NE alternative is projected to fail during the PM peak hour.

In general, most intersection results are similar to those obtained from the Synchro analysis. Lower delays are observed in the Vissim analysis for the intersections of SR 326 at I-75 northbound ramps, US 27 at northbound ramps, and US 27 at southbound ramps. Although lower delays are recorded for the subject intersections, arterial through movement queue lengths are extensive and indicative of the oversaturated conditions and high delays obtained in from the Synchro analysis.

### 6.2.4.3 Vissim Analysis Results - Roadway Links

Tables 6-9 and 6-10 summarize the average speeds and average travel times during the AM and PM peak hours.

The Build alternatives generally maintain good operating conditions. The lowest average speeds on the I-75 mainline basic segments occur south of US 27 and range between 42 and 59 mph . Speeds steadily increase to the north; both northbound and southbound. NW 49 ${ }^{\text {th }}$ Street between NW $44^{\text {th }}$ Avenue and I-75 has average speeds between 18 and 22 mph westbound and between 25 and 29 mph eastbound. US 27 operates at a lowest average speed of approximately 25 mph in the eastbound direction west of I-75 during the AM peak hour, and approximately 24 mph in the eastbound direction east of I-75 during the AM peak hour. SR 326 average speeds on both sides of I-75 are greater than 32 mph in both direction except the westbound segment east of I-75 exhibiting speeds under 25 mph during both peak hours.

Compared to No Build conditions, the Build alternatives show very similar changes amongst each other in terms of average speed. Across all build alternatives average speeds improve during both the AM and PM peak hours on the following segments:

- I-75 northbound, south of US 27
- I-75 southbound Off-Ramp to SR 326
- I-75 northbound On-Ramp from SR 326
- I-75 northbound Off-Ramp to US 27
- SR 326 eastbound, west of I-75
- SR 326 westbound, east of I-75
- NW 44 ${ }^{\text {th }}$ Avenue northbound, south of NW 49 ${ }^{\text {th }}$ Street
- NW 44 ${ }^{\text {th }}$ Avenue northbound, south of SR 326
- US 27 eastbound, east of I-75

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Table 6-9: 2045 Vissim Average Speed Summary (mph)

| Location |  | 2045 AM Peak |  |  |  |  |  | 2045 PM Peak |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | No Build | Diamond | SPUI | Parclo SE | Parclo NE | DDI | No Build | Diamond | SPUI | Parclo SE | Parclo NE | DDI |
| $\begin{gathered} \text { I-75 } \\ \text { Ramps } \end{gathered}$ | I-75 SB Off-Ramp to SR 326 | 38.6 | 42.6 | 42.6 | 42.5 | 42.5 | 42.6 | 40.2 | 42.6 | 42.6 | 42.6 | 42.6 | 42.6 |
|  | I-75 NB Off-Ramp to SR 326 | 32.6 | 32.5 | 32.9 | 32.7 | 32.3 | 33.0 | 31.3 | 33.1 | 32.8 | 33.2 | 32.8 | 33.2 |
|  | I-75 SB On-Ramp from SR 326 | 35.3 | 35.2 | 35.3 | 35.2 | 35.3 | 35.3 | 35.2 | 35.1 | 35.1 | 35.1 | 35.0 | 35.1 |
|  | I-75 SB On-Ramp from SR 326 (Loop) | 41.6 | 41.1 | 41.0 | 41.2 | 41.1 | 41.0 | 41.5 | 41.0 | 41.1 | 41.2 | 41.1 | 41.1 |
|  | 1-75 NB On-Ramp from SR 326 | 15.4 | 31.1 | 31.1 | 31.0 | 31.0 | 31.1 | 15.5 | 31.2 | 31.2 | 31.2 | 31.2 | 31.2 |
|  | 1-75 SB Off-Ramp to US 27 | 36.5 | 34.5 | 34.5 | 34.4 | 34.3 | 34.5 | 36.6 | 34.8 | 34.6 | 34.6 | 34.8 | 34.5 |
|  | I-75 NB Off-Ramp to US 27 | 55.8 | 60.8 | 59.0 | 60.5 | 59.3 | 61.6 | 58.8 | 64.3 | 64.7 | 63.7 | 64.6 | 64.4 |
|  | I-75 SB On-Ramp from US 27 | 35.5 | 35.6 | 35.6 | 35.6 | 35.6 | 35.6 | 35.4 | 32.3 | 34.3 | 33.8 | 32.7 | 33.8 |
|  | I-75 NB On-Ramp from US 27 | 33.6 | 33.6 | 33.6 | 33.6 | 33.5 | 33.6 | 33.7 | 33.6 | 33.6 | 33.6 | 33.6 | 33.6 |
|  | 1-75 SB Off-Ramp to NW 49 St |  | 35.6 | 35.6 | 35.6 | 35.6 | 40.6 |  | 35.5 | 35.6 | 35.5 | 35.5 | 40.6 |
|  | 1-75 NB Off-Ramp to NW 49 St |  | 35.3 | 35.1 | 35.4 | 35.7 | 30.4 |  | 35.2 | 34.9 | 35.3 | 35.7 | 30.3 |
|  | I-75 SB On-Ramp from NW 49 St |  | 34.6 | 34.8 | 34.0 | 33.9 | 29.5 |  | 32.2 | 35.0 | 34.7 | 34.3 | 29.9 |
|  | 1-75 NB On-Ramp from NW 49 St |  | 34.2 | 34.3 | 35.8 | 35.4 | 30.7 |  | 33.1 | 34.8 | 35.8 | 34.6 | 30.8 |
|  | I-75 NB Loop (Parclo SE On/Parclo NE Off) |  |  |  | 35.6 | 39.8 |  |  |  |  | 35.7 | 29.3 |  |
| I-75 <br> Mainline | $1-75$ NB S of US 27 | 55.3 | 63.6 | 61.1 | 63.0 | 62.8 | 62.6 | 61.9 | 64.7 | 64.7 | 64.7 | 64.7 | 64.7 |
|  | $1-75$ SB S of US 27 | 62.3 | 62.0 | 62.5 | 62.0 | 62.5 | 62.6 | 58.9 | 46.3 | 48.0 | 47.9 | 42.5 | 48.7 |
|  | 1-75 NB N of US 27 | 66.9 | 66.2 | 66.3 | 66.3 | 66.4 | 66.3 | 67.4 | 66.6 | 66.8 | 66.7 | 66.8 | 67.0 |
|  | 1-75 SB N of US 27 | 67.4 | 66.9 | 66.9 | 66.9 | 66.9 | 66.9 | 67.3 | 66.6 | 66.6 | 66.8 | 66.6 | 66.7 |
|  | I-75 NB S of SR 326 | 60.9 | 63.2 | 63.6 | 63.5 | 63.3 | 63.2 | 60.6 | 62.6 | 62.8 | 62.9 | 62.6 | 62.4 |
|  | 1-75 SB S of SR 326 | 65.5 | 65.2 | 65.2 | 65.2 | 65.2 | 65.3 | 64.9 | 64.4 | 64.1 | 64.4 | 64.2 | 64.3 |
|  | I-75 NB N of SR 326 | 67.2 | 67.1 | 67.2 | 67.2 | 67.2 | 67.2 | 67.8 | 67.8 | 67.8 | 67.8 | 67.8 | 67.8 |
|  | 1-75 SB N of SR326 | 68.6 | 68.6 | 68.6 | 68.6 | 68.6 | 68.6 | 68.3 | 68.1 | 68.1 | 68.1 | 68.1 | 68.1 |
| US 27 | US 27 EB W of I-75 | 25.1 | 25.2 | 25.3 | 25.2 | 25.1 | 25.5 | 28.9 | 31.3 | 31.6 | 30.8 | 31.3 | 31.0 |
|  | US 27 WB W of l-75 | 43.2 | 43.2 | 43.2 | 43.2 | 43.2 | 43.2 | 32.8 | 37.7 | 39.0 | 36.5 | 37.5 | 37.7 |
|  | US 27 EB E of I-75 | 24.0 | 24.5 | 23.4 | 24.3 | 23.7 | 24.6 | 25.0 | 28.6 | 28.3 | 27.1 | 28.7 | 28.6 |
|  | US 27 WB E of I-75 | 26.8 | 33.5 | 33.9 | 33.3 | 33.7 | 33.9 | 28.6 | 30.1 | 30.6 | 30.8 | 31.1 | 30.4 |
|  | US 27 EB E of NW 35 Ave Rd | 42.7 | 42.7 | 42.7 | 42.7 | 42.8 | 42.7 | 43.0 | 42.9 | 42.9 | 43.0 | 42.9 | 42.9 |
|  | US 27 WB E of NW 35 Ave Rd | 31.0 | 34.7 | 34.7 | 34.6 | 34.9 | 35.2 | 30.6 | 30.9 | 30.7 | 31.4 | 31.1 | 31.0 |
| NW 44 <br> Ave | NW 44 Av NB S of NW 49 St | 38.1 | 42.6 | 42.6 | 42.7 | 42.7 | 42.7 | 38.2 | 41.6 | 41.5 | 41.6 | 41.5 | 41.5 |
|  | NW 44 Av SB S of NW 49 St | 43.0 | 41.9 | 42.0 | 42.0 | 42.0 | 41.8 | 43.1 | 42.2 | 42.3 | 42.3 | 42.3 | 42.1 |
|  | NW 44 Av NB N of NW 49 St | 40.8 | 39.2 | 39.3 | 39.4 | 39.3 | 39.2 | 40.5 | 39.5 | 39.5 | 39.5 | 39.5 | 39.4 |
|  | NW 44 Av SB N of NW 49 St | 38.9 | 32.8 | 32.0 | 31.7 | 32.1 | 32.5 | 41.7 | 34.8 | 34.9 | 35.0 | 34.9 | 35.2 |
|  | NW 44 Ave NB S of SR 326 | 15.4 | 18.9 | 19.1 | 19.0 | 19.0 | 19.0 | 14.1 | 18.9 | 18.8 | 18.8 | 18.7 | 18.8 |
|  | NW 44 Ave SB S of SR 326 | 28.9 | 29.0 | 28.9 | 28.9 | 29.0 | 28.9 | 28.8 | 28.8 | 28.8 | 28.7 | 28.9 | 28.8 |
| SR 326 | SR 326 EB W of I-75 | 39.9 | 40.6 | 40.6 | 40.7 | 40.6 | 40.7 | 40.3 | 41.3 | 41.2 | 41.2 | 41.1 | 41.3 |
|  | SR 326 WB W of I-75 | 34.4 | 34.9 | 35.1 | 35.3 | 35.5 | 35.3 | 32.5 | 32.9 | 32.7 | 32.5 | 32.7 | 33.0 |
|  | SR 326 EB E of I-75 | 43.8 | 43.9 | 43.9 | 43.9 | 43.9 | 43.9 | 43.8 | 43.9 | 43.9 | 43.9 | 43.9 | 44.0 |
|  | SR 326 WB E of I-75 | 22.5 | 25.9 | 26.3 | 25.4 | 25.4 | 25.5 | 21.3 | 23.0 | 24.4 | 24.3 | 24.5 | 24.1 |
| NW 49 St | NW 49 St EB W of I-75 |  | 28.3 | 28.6 | 25.9 | 28.4 | 24.9 |  | 27.8 | 28.7 | 25.6 | 29.5 | 26.1 |
|  | NW 49 St WB W of I-75 |  | 21.5 | 20.3 | 20.5 | 20.6 | 18.3 |  | 20.2 | 20.2 | 21.0 | 20.7 | 18.6 |
|  | NW 49 St EB E of I-75 |  | 32.5 | 36.0 | 35.3 | 35.8 | 30.4 |  | 31.9 | 35.9 | 35.2 | 35.8 | 30.4 |
|  | NW 49 St WB E of I-75 |  | 34.5 | 35.8 | 34.6 | 35.9 | 30.5 |  | 34.9 | 36.0 | 35.0 | 36.1 | 30.7 |

Table 6-10: 2045 Vissim Average Travel Times (sec)


### 6.2.4.4 Vissim Analysis Results - Freeway Links

Volume, speed, and density time plots for I-75 are provided in Figures 6-17 through 6-40. In general, the majority of segments are able to process demand volumes and speeds are mostly maintained within 5-10 mph of the 70 mph posted speed limit. Similar to the results obtained in HCS, operating speeds decrease, and densities increase within the vicinity of the US 27 interchange. The lowest average speeds occur on the I-75 basic segments south of US 27, 41.4 mph during the AM peak period in the northbound direction and 48.5 mph during the PM peak period in the southbound direction. In addition, the volume time plots reveal that during the AM peak period, northbound I-75 segments north of US 27 result in a difference of more than 400 vph between processed and demand volume for time periods 2,5 , and 8 . However, the model does recover processing demand volumes to within the 400 vph threshold in the last four (4) time periods or beyond the 400 vph threshold of additional vehicles processed when compared to demand.

The five (5) build alternatives generally show similar results and trends as the No Build condition with reduced speeds and higher density in proximity to the US 27 interchange. The increase in overall demand volumes on the I-75 mainline results in reduced speeds on the I-75 southbound and US 27 merge segment falling below 30 mph for most of the PM peak period.

Overall, these operational results trends are similarly observed in the HCS analysis.

Figure 6-17: No Build 2045 Speed and Density Time Plots (AM Peak)

|  |  | NORT | HOU | D I-75 | - TIME | PLOTS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  | Averag | Speed | mph) |  |  |  |
| 12 | 67.0 | 66.6 | 67.2 | 67.5 | 66.9 | 65.0 | 67.4 | 65.8 | 66.7 |
| 11 | 66.3 | 63.1 | 66.0 | 66.9 | 66.7 | 63.5 | 67.0 | 65.8 | 66.7 |
| 10 | 65.1 | 58.1 | 65.8 | 67.4 | 66.9 | 64.9 | 67.4 | 65.7 | 66.7 |
| 9 | 64.2 | 54.0 | 65.1 | 67.2 | 66.8 | 65.1 | 67.5 | 65.8 | 66.8 |
| 8 | 59.2 | 43.2 | 62.7 | 66.7 | 66.6 | 61.3 | 66.8 | 65.7 | 66.5 |
| 7 | 58.1 | 41.4 | 63.3 | 66.8 | 66.4 | 60.0 | 66.7 | 65.3 | 66.3 |
| 6 | 64.0 | 54.8 | 65.1 | 67.1 | 66.5 | 61.1 | 66.4 | 65.5 | 66.3 |
| 5 | 66.1 | 64.9 | 65.8 | 67.3 | 66.7 | 64.7 | 67.4 | 65.5 | 66.8 |
| 4 | 66.9 | 66.2 | 66.8 | 67.6 | 66.9 | 64.7 | 67.4 | 66.0 | 66.8 |
| 3 | 67.1 | 66.6 | 67.2 | 67.7 | 67.1 | 65.4 | 67.7 | 66.4 | 67.3 |
| 2 | 67.4 | 66.9 | 67.5 | 67.9 | 67.5 | 66.1 | 68.2 | 66.5 | 67.6 |
| 1 | 68.0 | 67.1 | 68.0 | 68.2 | 67.9 | 66.7 | 68.5 | 67.1 | 68.2 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basi |
| Int. | I-75 | US 27 Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 16,377 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > |


| Time | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 26.1 | 26.4 | 21.2 | 22.3 | 22.8 | 23.8 | 17.5 | 21.3 | 21.1 |
| 11 | 28.9 | 30.8 | 23.6 | 24.5 | 24.3 | 25.6 | 18.4 | 21.9 | 21.6 |
| 10 | 29.6 | 37.5 | 22.7 | 23.2 | 23.5 | 24.2 | 17.7 | 21.5 | 21.2 |
| 9 | 30.2 | 43.7 | 23.3 | 23.4 | 23.6 | 24.3 | 17.8 | 21.6 | 21.4 |
| 8 | 34.7 | 53.3 | 25.2 | 24.8 | 25.0 | 28.2 | 19.3 | 23.0 | 22.9 |
| 7 | 38.8 | 57.5 | 26.1 | 25.7 | 25.9 | 32.5 | 19.8 | 23.8 | 23.4 |
| 6 | 33.5 | 44.0 | 25.4 | 25.9 | 26.2 | 29.3 | 20.1 | 23.8 | 23.5 |
| 5 | 31.3 | 31.4 | 25.1 | 25.4 | 25.3 | 25.6 | 18.6 | 22.5 | 22.1 |
| 4 | 27.1 | 26.9 | 21.7 | 22.5 | 22.4 | 23.2 | 17.0 | 20.5 | 20.2 |
| 3 | 25.7 | 25.4 | 20.4 | 21.2 | 21.3 | 21.7 | 15.9 | 19.1 | 18.8 |
| 2 | 23.0 | 22.4 | 17.9 | 18.7 | 18.3 | 18.2 | 13.4 | 16.4 | 16.0 |
| 1 | 18.1 | 17.9 | 14.3 | 14.9 | 14.6 | 14.7 | 10.7 | 13.0 | 12.7 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | I-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 16,377 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | > | > | > | > | > | > | $>$ |

[^6] (Posted Speed-Avg. Speed)

SOUTHBOUND I-75 - TIME PLOTS

| Time | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.8 | 68.7 | 68.5 | 66.1 | 67.1 | 66.3 | 67.5 | 68.0 | 67.4 | 62.5 | 65.2 |
| 11 | 68.6 | 68.7 | 68.3 | 66.1 | 67.1 | 66.1 | 67.5 | 68.0 | 67.2 | 61.4 | 64.4 |
| 10 | 68.7 | 68.6 | 68.3 | 66.0 | 66.9 | 66.0 | 67.5 | 68.0 | 67.3 | 62.1 | 64.8 |
| 9 | 68.7 | 68.6 | 68.3 | 66.0 | 66.9 | 66.3 | 67.5 | 68.0 | 67.3 | 62.3 | 65.0 |
| 8 | 68.6 | 68.8 | 68.4 | 66.0 | 66.9 | 66.2 | 67.4 | 68.0 | 67.2 | 60.9 | 64.1 |
| 7 | 68.3 | 68.2 | 67.8 | 66.0 | 66.2 | 65.5 | 67.2 | 67.9 | 66.9 | 60.1 | 62.7 |
| 6 | 68.3 | 68.1 | 67.9 | 66.2 | 66.7 | 65.8 | 67.2 | 67.9 | 67.0 | 59.9 | 63.8 |
| 5 | 68.4 | 68.5 | 68.1 | 66.2 | 66.8 | 66.0 | 67.2 | 67.9 | 67.1 | 61.8 | 64.5 |
| 4 | 68.7 | 68.6 | 68.4 | 66.1 | 67.1 | 66.3 | 67.5 | 68.1 | 67.3 | 62.5 | 65.2 |
| 3 | 68.8 | 68.8 | 68.5 | 66.3 | 67.4 | 66.3 | 67.6 | 68.1 | 67.4 | 63.8 | 65.8 |
| 2 | 69.0 | 69.0 | 68.7 | 66.4 | 67.5 | 66.7 | 67.8 | 68.3 | 67.6 | 64.4 | 66.5 |
| 1 | 69.4 | 69.3 | 69.1 | 66.6 | 67.9 | 67.3 | 68.2 | 68.5 | 68.2 | 65.7 | 67.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > |


| Time | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 14.9 | 14.7 | 12.9 | 17.5 | 17.3 | 18.8 | 18.5 | 18.5 | 17.7 | 25.5 | 24.5 |
| 11 | 16.6 | 16.3 | 14.3 | 18.7 | 18.4 | 20.4 | 20.0 | 19.8 | 19.1 | 27.3 | 26.0 |
| 10 | 16.1 | 15.8 | 13.9 | 18.4 | 18.1 | 19.9 | 19.4 | 19.1 | 18.4 | 26.3 | 25.1 |
| 9 | 16.1 | 15.8 | 13.8 | 18.1 | 17.9 | 19.5 | 19.0 | 18.7 | 17.9 | 25.7 | 24.6 |
| 8 | 15.9 | 15.6 | 13.8 | 18.2 | 18.0 | 19.6 | 19.5 | 19.7 | 19.1 | 27.8 | 26.3 |
| 7 | 18.8 | 18.5 | 16.3 | 20.6 | 20.6 | 22.5 | 21.8 | 21.4 | 20.8 | 29.5 | 28.3 |
| 6 | 18.8 | 18.6 | 16.2 | 20.2 | 20.0 | 21.9 | 21.4 | 21.1 | 20.4 | 29.5 | 27.6 |
| 5 | 18.4 | 17.9 | 15.6 | 19.7 | 19.5 | 21.3 | 20.7 | 20.2 | 19.4 | 27.3 | 26.1 |
| 4 | 15.7 | 15.4 | 13.5 | 17.8 | 17.6 | 19.2 | 18.7 | 18.5 | 17.9 | 25.2 | 24.1 |
| 3 | 15.0 | 14.7 | 12.9 | 17.0 | 16.6 | 18.3 | 17.7 | 17.3 | 16.7 | 23.1 | 22.3 |
| 2 | 13.8 | 13.4 | 11.6 | 15.2 | 14.8 | 16.3 | 15.6 | 15.3 | 14.6 | 19.9 | 19.3 |
| 1 | 10.8 | 10.6 | 9.4 | 12.3 | 12.1 | 13.1 | 12.7 | 12.4 | 11.7 | 15.9 | 15.4 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3,001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | vel | > | > | > | > | > | > | > | > | > |  |

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0 \quad>$
Using HCM 2010 thresholds for informational purposes

| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 5249 | 5256 | 4278 | 4518 | 4569 | 4620 | 3534 | 4208 | 4226 |
|  | Demand | 5162 | 5162 | 4159 | 4362 | 4362 | 4362 | 3331 | 3974 | 3974 |
|  | Diff. | 87 | 94 | 119 | 156 | 207 | 258 | 203 | 234 | 252 |
| 11 | Processed | 5740 | 5718 | 4672 | 4914 | 4863 | 4840 | 3695 | 4331 | 4330 |
|  | Demand | 5744 | 5744 | 4629 | 4855 | 4855 | 4855 | 3707 | 4422 | 4422 |
|  | Diff. | -4 | -26 | 43 | 59 | 8 | -15 | -12 | -91 | -92 |
| 10 | Processed | 5583 | 5535 | 4473 | 4693 | 4713 | 4705 | 3580 | 4245 | 4246 |
|  | Demand | 5578 | 5578 | 4495 | 4714 | 4714 | 4714 | 3600 | 4294 | 4294 |
|  | Diff. | 5 | -43 | -22 | -21 | -1 | -9 | -20 | -49 | -48 |
| 9 | Processed | 5616 | 5595 | 4513 | 4713 | 4721 | 4721 | 3596 | 4265 | 4278 |
|  | Demand | 5587 | 5587 | 4502 | 4722 | 4722 | 4722 | 3605 | 4301 | 4301 |
|  | Diff. | 29 | 8 | 11 | -9 | -1 | -1 | -9 | -36 | -23 |
| 8 | Processed | 5636 | 5809 | 4711 | 4961 | 5002 | 5063 | 3871 | 4540 | 4569 |
|  | Demand | 5458 | 5458 | 4398 | 4613 | 4613 | 4613 | 3522 | 4202 | 4202 |
|  | Diff. | 178 | 351 | 313 | 348 | 389 | 450 | 349 | 338 | 367 |
| 7 | Processed | 6309 | 6088 | 4940 | 5151 | 5151 | 5168 | 3957 | 4665 | 4651 |
|  | Demand | 6468 | 6468 | 5212 | 5467 | 5467 | 5467 | 4174 | 4980 | 4980 |
|  | Diff. | -159 | -380 | -272 | -316 | -316 | -299 | -217 | -315 | -329 |
| 6 | Processed | 6357 | 6147 | 4952 | 5199 | 5224 | 5246 | 3992 | 4673 | 4684 |
|  | Demand | 6506 | 6506 | 5243 | 5499 | 5499 | 5499 | 4199 | 5009 | 5009 |
|  | Diff. | -149 | -359 | -291 | -300 | -275 | -253 | -207 | -336 | -325 |
| 5 | Processed | 6201 | 6055 | 4930 | 5131 | 5050 | 4960 | 3760 | 4426 | 4425 |
|  | Demand | 6367 | 6367 | 5131 | 5381 | 5381 | 5381 | 4109 | 4902 | 4902 |
|  | Diff. | -166 | -312 | -201 | -250 | -331 | -421 | -349 | -476 | -477 |
| 4 | Processed | 5430 | 5335 | 4345 | 4557 | 4504 | 4492 | 3437 | 4066 | 4058 |
|  | Demand | 5494 | 5494 | 4427 | 4643 | 4643 | 4643 | 3545 | 4230 | 4230 |
|  | Diff. | -64 | -159 | -82 | -86 | -139 | -151 | -108 | -164 | -172 |
| 3 | Processed | 5165 | 5075 | 4112 | 4301 | 4282 | 4251 | 3226 | 3803 | 3792 |
|  | Demand | 5248 | 5248 | 4229 | 4435 | 4435 | 4435 | 3387 | 4040 | 4040 |
|  | Diff. | -83 | -173 | -117 | -134 | -153 | -184 | -161 | -237 | -248 |
| 2 | Processed | 4661 | 4507 | 3631 | 3803 | 3715 | 3599 | 2733 | 3270 | 3254 |
|  | Demand | 4821 | 4821 | 3885 | 4074 | 4074 | 4074 | 3111 | 3711 | 3711 |
|  | Diff. | -160 | -314 | -254 | -271 | -359 | -475 | -378 | -441 | -457 |
| 1 | Processed | 3691 | 3589 | 2910 | 3049 | 2978 | 2933 | 2208 | 2621 | 2605 |
|  | Demand | 3796 | 3796 | 3059 | 3208 | 3208 | 3208 | 2450 | 2922 | 2922 |
|  | Diff. | -105 | -207 | -149 | -159 | -230 | -275 | -242 | -301 | -317 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | l-75 | US 27 Interchange |  |  | I-75 | SR 326 Interchange |  |  | I-75 |
| Direction | Travel | > | > | > | > | > | > | > | > | > |


| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 3086 | 3025 | 2658 | 3466 | 3476 | 3740 | 3746 | 3773 | 3585 | 4761 | 4785 |
|  | Demand | 3091 | 3091 | 2651 | 3401 | 3401 | 3676 | 3676 | 3676 | 3496 | 4575 | 4575 |
|  | Diff. | -5 | -66 | 7 | 65 | 75 | 64 | 70 | 97 | 89 | 186 | 210 |
| 11 | Processed | 3406 | 3352 | 2933 | 3709 | 3701 | 4047 | 4041 | 4035 | 3859 | 5025 | 5017 |
|  | Demand | 3440 | 3440 | 2950 | 3785 | 3785 | 4091 | 4091 | 4091 | 3890 | 5092 | 5092 |
|  | Diff. | -34 | -88 | -17 | -76 | -84 | -44 | -50 | -56 | -31 | -67 | -75 |
| 10 | Processed | 3323 | 3260 | 2852 | 3640 | 3640 | 3935 | 3917 | 3911 | 3724 | 4888 | 4879 |
|  | Demand | 3341 | 3341 | 2865 | 3675 | 3675 | 3972 | 3972 | 3972 | 3778 | 4945 | 4945 |
|  | Diff. | -18 | -81 | -13 | -35 | -35 | -37 | -55 | -61 | -54 | -57 | -66 |
| 9 | Processed | 3315 | 3255 | 2820 | 3591 | 3594 | 3881 | 3847 | 3817 | 3621 | 4785 | 4796 |
|  | Demand | 3346 | 3346 | 2869 | 3681 | 3681 | 3978 | 3978 | 3978 | 3784 | 4952 | 4952 |
|  | Diff. | -31 | -91 | -49 | -90 | -87 | -97 | -131 | -161 | -163 | -167 | -156 |
| 8 | Processed | 3270 | 3213 | 2822 | 3600 | 3601 | 3884 | 3950 | 4026 | 3850 | 5047 | 5052 |
|  | Demand | 3269 | 3269 | 2803 | 3596 | 3596 | 3887 | 3887 | 3887 | 3697 | 4838 | 4838 |
|  | Diff. | 1 | -56 | 19 | 4 | 5 | -3 | 63 | 139 | 153 | 209 | 214 |
| 7 | Processed | 3856 | 3786 | 3318 | 4082 | 4082 | 4429 | 4399 | 4368 | 4177 | 5285 | 5303 |
|  | Demand | 3874 | 3874 | 3322 | 4262 | 4262 | 4606 | 4606 | 4606 | 4381 | 5734 | 5734 |
|  | Diff. | -18 | -88 | -4 | -180 | -180 | -177 | -207 | -238 | -204 | -449 | -431 |
| 6 | Processed | 3856 | 3794 | 3296 | 4012 | 4002 | 4324 | 4305 | 4306 | 4098 | 5268 | 5265 |
|  | Demand | 3896 | 3896 | 3341 | 4287 | 4287 | 4633 | 4633 | 4633 | 4406 | 5767 | 5767 |
|  | Diff. | -40 | -102 | -45 | -275 | -285 | -309 | -328 | -327 | -308 | -499 | -502 |
| 5 | Processed | 3778 | 3686 | 3190 | 3910 | 3904 | 4210 | 4173 | 4111 | 3902 | 5042 | 5043 |
|  | Demand | 3813 | 3813 | 3270 | 4195 | 4195 | 4534 | 4534 | 4534 | 4312 | 5644 | 5644 |
|  | Diff. | -35 | -127 | -80 | -285 | -291 | -324 | -361 | -423 | -410 | -602 | -601 |
| 4 | Processed | 3240 | 3174 | 2774 | 3535 | 3537 | 3815 | 3789 | 3775 | 3611 | 4710 | 4698 |
|  | Demand | 3290 | 3290 | 2821 | 3620 | 3620 | 3912 | 3912 | 3912 | 3721 | 4870 | 4870 |
|  | Diff. | -50 | -116 | -47 | -85 | -83 | -97 | -123 | -137 | -110 | -160 | -172 |
| 3 | Processed | 3095 | 3038 | 2651 | 3367 | 3363 | 3638 | 3580 | 3543 | 3381 | 4406 | 4393 |
|  | Demand | 3143 | 3143 | 2695 | 3458 | 3458 | 3737 | 3737 | 3737 | 3554 | 4652 | 4652 |
|  | Diff. | -48 | -105 | -44 | -91 | -95 | -99 | -157 | -194 | -173 | -246 | -259 |
| 2 | Processed | 2847 | 2769 | 2392 | 3017 | 3007 | 3255 | 3181 | 3127 | 2972 | 3847 | 3843 |
|  | Demand | 2887 | 2887 | 2476 | 3176 | 3176 | 3433 | 3433 | 3433 | 3265 | 4273 | 4273 |
|  | Diff. | -40 | -118 | -84 | -159 | -169 | -178 | -252 | -306 | -293 | -426 | -430 |
| 1 | Processed | 2256 | 2212 | 1942 | 2465 | 2460 | 2645 | 2591 | 2534 | 2400 | 3128 | 3117 |
|  | Demand | 2273 | 2273 | 1949 | 2501 | 2501 | 2703 | 2703 | 2703 | 2571 | 3365 | 3365 |
|  | Diff. | -17 | -61 | -7 | -36 | -41 | -58 | -112 | -169 | -171 | -237 | -248 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 | Interch | ange | I-75 |
| Direction | f Travel | > | > | > | > | > | > | > | > | > | > |  |

Volume (vph): XXXX Difference greater than 400vph (Based on FDOT Traffic Analysis Handbook Calibration Volume> 2,700 vph)

Figure 6-19: No Build 2045 Speed and Density Time Plots (PM Peak)

NORTHBOUND I-75-TIME PLOTS

| Time <br> Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 67.7 | 66.4 | 67.6 | 67.9 | 67.6 | 64.5 | 68.3 | 66.2 | 67.7 |  |  |  |  |  |  |
| 11 | 66.8 | 57.9 | 66.8 | 67.6 | 67.4 | 65.0 | 68.3 | 66.1 | 67.6 |  |  |  |  |  |  |
| 10 | 64.2 | 54.7 | 66.1 | 67.5 | 67.1 | 59.4 | 67.6 | 66.2 | 67.4 |  |  |  |  |  |  |
| 9 | 63.9 | 54.5 | 66.2 | 67.4 | 66.9 | 58.9 | 67.6 | 66.1 | 67.3 |  |  |  |  |  |  |
| 8 | 66.5 | 57.1 | 66.2 | 67.5 | 67.0 | 61.5 | 67.7 | 66.1 | 67.2 |  |  |  |  |  |  |
| 7 | 66.8 | 64.5 | 66.9 | 67.7 | 67.0 | 63.5 | 67.9 | 66.1 | 67.3 |  |  |  |  |  |  |
| 6 | 67.0 | 64.4 | 67.1 | 67.6 | 67.2 | 58.8 | 67.7 | 66.1 | 67.3 |  |  |  |  |  |  |
| 5 | 66.9 | 62.5 | 67.1 | 67.7 | 67.1 | 61.8 | 67.8 | 66.1 | 67.3 |  |  |  |  |  |  |
| 4 | 67.0 | 66.4 | 67.4 | 67.6 | 67.0 | 62.8 | 67.9 | 65.9 | 67.3 |  |  |  |  |  |  |
| 3 | 67.0 | 65.9 | 67.4 | 67.7 | 67.2 | 63.9 | 68.0 | 66.2 | 67.5 |  |  |  |  |  |  |
| 2 | 67.3 | 65.3 | 67.4 | 67.7 | 67.3 | 64.6 | 68.1 | 66.2 | 67.5 |  |  |  |  |  |  |
| 1 | 67.2 | 66.3 | 67.5 | 67.5 | 67.2 | 64.4 | 68.1 | 66.0 | 67.6 |  |  |  |  |  |  |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |  |  |  |  |  |  |
| Int. | I-75 | US 27 Interchange | I-75 | SR 326 Interchange | $1-75$ |  |  |  |  |  |  |  |  |  |  |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 16,377 | 1,500 | 3,094 | 1,495 | 3,759 |  |  |  |  |  |  |
| Direction of Travel | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ | $>$ |  |  |  |  |  |  |  |


| Time | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 20.6 | 20.9 | 15.9 | 17.1 | 17.1 | 18.3 | 12.1 | 15.7 | 15.4 |
| 11 | 22.8 | 31.0 | 17.5 | 18.4 | 18.6 | 19.4 | 12.9 | 16.8 | 16.4 |
| 10 | 27.0 | 38.7 | 19.1 | 19.6 | 20.0 | 24.8 | 14.1 | 17.8 | 17.5 |
| 9 | 30.2 | 39.9 | 20.4 | 21.2 | 21.4 | 26.2 | 14.7 | 18.4 | 18.1 |
| 8 | 27.5 | 35.7 | 20.9 | 21.6 | 21.9 | 24.7 | 15.2 | 18.9 | 18.6 |
| 7 | 27.4 | 28.4 | 20.9 | 21.7 | 21.6 | 22.9 | 14.7 | 18.3 | 17.9 |
| 6 | 25.7 | 26.8 | 19.3 | 20.3 | 20.6 | 25.5 | 14.3 | 18.1 | 17.8 |
| 5 | 26.4 | 29.3 | 20.1 | 21.0 | 21.1 | 23.7 | 14.5 | 18.1 | 17.8 |
| 4 | 26.0 | 26.0 | 20.0 | 20.9 | 21.2 | 23.1 | 14.5 | 18.4 | 18.0 |
| 3 | 26.0 | 25.9 | 19.4 | 20.4 | 20.4 | 21.5 | 14.0 | 17.5 | 17.1 |
| 2 | 23.3 | 24.3 | 18.0 | 19.1 | 19.1 | 20.1 | 13.3 | 16.8 | 16.6 |
| 1 | 24.1 | 24.1 | 18.1 | 19.3 | 19.4 | 20.2 | 13.2 | 16.7 | 16.4 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 16,377 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | > | > | > | > | > | > | > |

## AVERAGE SPEED DIFFERENCE (mph)

Diff.: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph Upper: $70<65 \quad<60<55<50<45$ Lower: $\begin{array}{lllllll}65 & 60 & 55 & 50 & 45 & 0\end{array}$ (Posted Speed-Avg. Speed)

SOUTHBOUND I-75 - TIME PLOTS

| Time | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.5 | 68.2 | 68.0 | 65.8 | 66.6 | 66.0 | 67.3 | 68.0 | 67.0 | 60.8 | 63.2 |
| 11 | 68.4 | 68.6 | 68.0 | 65.9 | 66.6 | 65.8 | 67.1 | 68.0 | 66.8 | 59.1 | 61.7 |
| 10 | 68.3 | 68.1 | 67.6 | 65.9 | 66.2 | 65.5 | 67.0 | 67.9 | 66.5 | 52.7 | 59.6 |
| 9 | 67.9 | 67.6 | 67.5 | 65.9 | 65.6 | 65.1 | 66.8 | 67.8 | 66.4 | 49.0 | 55.8 |
| 8 | 67.6 | 67.8 | 67.4 | 66.1 | 66.0 | 65.4 | 66.7 | 67.9 | 66.2 | 48.1 | 55.4 |
| 7 | 67.7 | 67.6 | 67.3 | 65.9 | 65.4 | 65.0 | 66.8 | 67.8 | 66.1 | 48.5 | 57.0 |
| 6 | 68.0 | 68.3 | 67.7 | 66.0 | 66.0 | 65.1 | 66.8 | 67.7 | 66.3 | 51.7 | 57.8 |
| 5 | 67.9 | 68.2 | 67.5 | 66.0 | 66.0 | 65.4 | 66.8 | 67.9 | 66.5 | 54.8 | 59.9 |
| 4 | 67.9 | 67.9 | 67.4 | 66.0 | 65.3 | 64.9 | 66.8 | 67.9 | 66.4 | 51.3 | 57.7 |
| 3 | 67.9 | 68.4 | 67.7 | 66.0 | 66.0 | 65.1 | 66.8 | 67.7 | 66.3 | 56.3 | 61.3 |
| 2 | 68.3 | 68.3 | 67.8 | 66.0 | 66.2 | 65.5 | 67.1 | 67.9 | 66.6 | 58.7 | 61.2 |
| 1 | 68.2 | 68.1 | 67.7 | 66.2 | 66.4 | 65.9 | 67.1 | 68.0 | 66.8 | 59.2 | 62.2 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basi |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > |  |


| Time | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 16.9 | 16.8 | 15.1 | 19.8 | 19.6 | 21.0 | 20.7 | 20.6 | 20.2 | 28.2 | 27.1 |
| 11 | 18.4 | 18.0 | 16.3 | 21.1 | 20.9 | 22.7 | 22.2 | 22.0 | 21.6 | 30.9 | 29.5 |
| 10 | 19.4 | 19.3 | 17.3 | 21.9 | 21.8 | 23.6 | 23.2 | 23.3 | 22.6 | 36.7 | 32.2 |
| 9 | 22.3 | 22.0 | 19.7 | 24.1 | 24.2 | 26.1 | 25.3 | 25.0 | 24.5 | 42.2 | 36.6 |
| 8 | 22.9 | 22.4 | 20.1 | 24.2 | 24.2 | 26.0 | 25.4 | 24.9 | 24.6 | 44.2 | 37.2 |
| 7 | 23.2 | 22.9 | 20.5 | 24.6 | 24.7 | 26.5 | 25.6 | 24.9 | 24.5 | 42.5 | 35.2 |
| 6 | 21.5 | 21.0 | 18.8 | 23.2 | 23.2 | 25.2 | 24.6 | 24.4 | 23.9 | 39.8 | 34.7 |
| 5 | 22.2 | 21.8 | 19.7 | 24.0 | 23.9 | 25.6 | 24.9 | 24.4 | 24.0 | 37.0 | 33.0 |
| 4 | 21.8 | 21.5 | 19.1 | 23.4 | 23.7 | 25.4 | 24.7 | 24.3 | 24.0 | 40.0 | 35.0 |
| 3 | 21.9 | 21.2 | 19.0 | 23.5 | 23.5 | 25.3 | 24.3 | 23.7 | 23.2 | 34.3 | 30.7 |
| 2 | 19.4 | 19.2 | 17.3 | 21.7 | 21.6 | 23.3 | 22.7 | 22.4 | 22.1 | 31.6 | 30.3 |
| 1 | 20.3 | 19.9 | 17.7 | 21.9 | 21.9 | 23.5 | 22.9 | 22.6 | 22.1 | 31.1 | 29.5 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3,001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 16,086 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > |

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$ Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0>$ Using HCM 2010 thresholds for informational purposes

NORTHBOUND I-75 - TIME PLOT

| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 4180 | 4154 | 3231 | 3474 | 3475 | 3514 | 2471 | 3108 | 3118 |
|  | Demand | 4125 | 4125 | 3161 | 3363 | 3363 | 3363 | 2352 | 2924 | 2924 |
|  | Diff. | 55 | 29 | 70 | 111 | 112 | 151 | 119 | 184 | 194 |
| 11 | Processed | 4520 | 4552 | 3498 | 3736 | 3761 | 3769 | 2647 | 3323 | 3326 |
|  | Demand | 4486 | 4486 | 3437 | 3657 | 3657 | 3657 | 2558 | 3180 | 3180 |
|  | Diff. | 34 | 66 | 61 | 79 | 104 | 112 | 89 | 143 | 146 |
| 10 | Processed | 4813 | 4886 | 3769 | 3975 | 4030 | 4091 | 2853 | 3534 | 3544 |
|  | Demand | 4727 | 4727 | 3622 | 3854 | 3854 | 3854 | 2696 | 3351 | 3351 |
|  | Diff. | 86 | 159 | 147 | 121 | 176 | 237 | 157 | 183 | 193 |
| 9 | Processed | 5403 | 5276 | 4055 | 4280 | 4291 | 4289 | 2977 | 3657 | 3666 |
|  | Demand | 5401 | 5401 | 4139 | 4403 | 4403 | 4403 | 3080 | 3828 | 3828 |
|  | Diff. | 2 | -125 | -84 | -123 | -112 | -114 | -103 | -171 | -162 |
| 8 | Processed | 5479 | 5376 | 4143 | 4378 | 4407 | 4414 | 3088 | 3742 | 3749 |
|  | Demand | 5485 | 5485 | 4203 | 4472 | 4472 | 4472 | 3128 | 3888 | 3888 |
|  | Diff. | -6 | -109 | -60 | -94 | -65 | -58 | -40 | -146 | -139 |
| 7 | Processed | 5494 | 5392 | 4196 | 4402 | 4336 | 4308 | 3001 | 3621 | 3624 |
|  | Demand | 5573 | 5573 | 4271 | 4544 | 4544 | 4544 | 3178 | 3950 | 3950 |
|  | Diff. | -79 | -181 | -75 | -142 | -208 | -236 | -177 | -329 | -326 |
| 6 | Processed | 5162 | 5130 | 3889 | 4120 | 4150 | 4174 | 2898 | 3580 | 3589 |
|  | Demand | 5219 | 5219 | 3999 | 4254 | 4254 | 4254 | 2976 | 3699 | 3699 |
|  | Diff. | -57 | -89 | -110 | -134 | -104 | -80 | -78 | -119 | -110 |
| 5 | Processed | 5303 | 5208 | 4052 | 4271 | 4249 | 4262 | 2960 | 3584 | 3592 |
|  | Demand | 5375 | 5375 | 4119 | 4382 | 4382 | 4382 | 3065 | 3810 | 3810 |
|  | Diff. | -72 | -167 | -67 | -111 | -133 | -120 | -105 | -226 | -218 |
| 4 | Processed | 5230 | 5181 | 4033 | 4249 | 4254 | 4247 | 2961 | 3634 | 3639 |
|  | Demand | 5273 | 5273 | 4041 | 4299 | 4299 | 4299 | 3007 | 3738 | 3738 |
|  | Diff. | -43 | -92 | -8 | -50 | -45 | -52 | -46 | -104 | -99 |
| 3 | Processed | 5227 | 5118 | 3915 | 4129 | 4104 | 4081 | 2864 | 3480 | 3461 |
|  | Demand | 5326 | 5326 | 4081 | 4342 | 4342 | 4342 | 3037 | 3775 | 3775 |
|  | Diff. | -99 | -208 | -166 | -213 | -238 | -261 | -173 | -295 | -314 |
| 2 | Processed | 4712 | 4680 | 3640 | 3875 | 3859 | 3874 | 2711 | 3342 | 3354 |
|  | Demand | 4749 | 4749 | 3639 | 3872 | 3872 | 3872 | 2708 | 3366 | 3366 |
|  | Diff. | -37 | -69 | 1 | 3 | -13 | 2 | 3 | -24 | -12 |
| 1 | Processed | 4862 | 4788 | 3668 | 3906 | 3905 | 3890 | 2707 | 3313 | 3323 |
|  | Demand | 4920 | 4920 | 3770 | 4011 | 4011 | 4011 | 2806 | 3488 | 3488 |
|  | Diff. | -58 | -132 | -102 | -105 | -106 | -121 | -99 | -175 | -165 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | I-75 | US 27 Interchange |  |  | I-75 | SR 326 Interchange |  |  | I-75 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > |

SOUTHBOUND I-75 - TIME PLOT

| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | Processed | 3478 | 3439 | 3076 | 3907 | 3905 | 4158 | 4173 | 4218 | 4055 | 5116 | 5124 |
|  | Demand | 3486 | 3486 | 3054 | 3744 | 3744 | 3988 | 3988 | 3988 | 3821 | 4793 | 4793 |
|  | Diff. | -8 | -47 | 22 | 163 | 161 | 170 | 185 | 230 | 234 | 323 | 331 |
| 11 | Processed | 3777 | 3714 | 3324 | 4168 | 4168 | 4472 | 4474 | 4484 | 4337 | 5449 | 5443 |
|  | Demand | 3791 | 3791 | 3321 | 4072 | 4072 | 4337 | 4337 | 4337 | 4155 | 5212 | 5212 |
|  | Diff. | -14 | -77 | 3 | 96 | 96 | 135 | 137 | 147 | 182 | 237 | 231 |
| 10 | Processed | 3979 | 3938 | 3517 | 4324 | 4321 | 4634 | 4673 | 4725 | 4511 | 5619 | 5680 |
|  | Demand | 3995 | 3995 | 3500 | 4291 | 4291 | 4570 | 4570 | 4570 | 4378 | 5493 | 5493 |
|  | Diff. | -16 | -57 | 17 | 33 | 30 | 64 | 103 | 155 | 133 | 126 | 187 |
| 9 | Processed | 4541 | 4461 | 3986 | 4757 | 4759 | 5079 | 5073 | 5088 | 4877 | 5975 | 5973 |
|  | Demand | 4565 | 4565 | 3999 | 4903 | 4903 | 5222 | 5222 | 5222 | 5003 | 6276 | 6276 |
|  | Diff. | -24 | -104 | -13 | -146 | -144 | -143 | -149 | -134 | -126 | -301 | -303 |
| 8 | Processed | 4635 | 4557 | 4054 | 4786 | 4792 | 5092 | 5080 | 5070 | 4886 | 5983 | 6004 |
|  | Demand | 4636 | 4636 | 4062 | 4980 | 4980 | 5304 | 5304 | 5304 | 5081 | 6374 | 6374 |
|  | Diff. | -1 | -79 | -8 | -194 | -188 | -212 | -224 | -234 | -195 | -391 | -370 |
| 7 | Processed | 4708 | 4636 | 4126 | 4862 | 4849 | 5154 | 5121 | 5065 | 4853 | 5956 | 5916 |
|  | Demand | 4710 | 4710 | 4127 | 5059 | 5059 | 5389 | 5389 | 5389 | 5162 | 6476 | 6476 |
|  | Diff. | -2 | -74 | -1 | -197 | -210 | -235 | -268 | -324 | -309 | -520 | -560 |
| 6 | Processed | 4376 | 4301 | 3815 | 4589 | 4600 | 4928 | 4930 | 4957 | 4740 | 5829 | 5849 |
|  | Demand | 4411 | 4411 | 3864 | 4738 | 4738 | 5046 | 5046 | 5046 | 4834 | 6064 | 6064 |
|  | Diff. | -35 | -110 | -49 | -149 | -138 | -118 | -116 | -89 | -94 | -235 | -215 |
| 5 | Processed | 4514 | 4453 | 3982 | 4739 | 4728 | 5023 | 4991 | 4974 | 4786 | 5874 | 5866 |
|  | Demand | 4543 | 4543 | 3980 | 4880 | 4880 | 5197 | 5197 | 5197 | 4979 | 6246 | 6246 |
|  | Diff. | -29 | -90 | 2 | -141 | -152 | -174 | -206 | -223 | -193 | -372 | -380 |
| 4 | Processed | 4448 | 4368 | 3860 | 4630 | 4636 | 4937 | 4937 | 4945 | 4781 | 5902 | 5923 |
|  | Demand | 4457 | 4457 | 3904 | 4787 | 4787 | 5099 | 5099 | 5099 | 4884 | 6127 | 6127 |
|  | Diff. | -9 | -89 | -44 | -157 | -151 | -162 | -162 | -154 | -103 | -225 | -204 |
| 3 | Processed | 4456 | 4356 | 3858 | 4651 | 4646 | 4937 | 4870 | 4815 | 4605 | 5633 | 5611 |
|  | Demand | 4501 | 4501 | 3943 | 4835 | 4835 | 5149 | 5149 | 5149 | 4933 | 6188 | 6188 |
|  | Diff. | -45 | -145 | -85 | -184 | -189 | -212 | -279 | -334 | -328 | -555 | -577 |
| 2 | Processed | 3981 | 3941 | 3517 | 4291 | 4281 | 4571 | 4573 | 4574 | 4414 | 5500 | 5514 |
|  | Demand | 4014 | 4014 | 3516 | 4311 | 4311 | 4592 | 4592 | 4592 | 4399 | 5519 | 5519 |
|  | Diff. | -33 | -73 | 1 | -20 | -30 | -21 | -19 | -18 | 15 | -19 | -5 |
| 1 | Processed | 4156 | 4068 | 3602 | 4349 | 4353 | 4629 | 4614 | 4609 | 4431 | 5472 | 5473 |
|  | Demand | 4158 | 4158 | 3643 | 4466 | 4466 | 4757 | 4757 | 4757 | 4557 | 5717 | 5717 |
|  | Diff. | -2 | -90 | -41 | -117 | -113 | -128 | -143 | -148 | -126 | -245 | -244 |
| Type |  | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | I-75 | SR 326 Interchange |  |  |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > |


| NORTHBOUND I-75-TIME PLOTS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 66.8 | 66.9 | 66.9 | 66.5 | 65.8 | 64.4 | 67.0 | 65.9 | 64.4 | 65.1 | 67.5 | 66.0 | 66.7 |
| 11 | 66.5 | 66.6 | 66.4 | 66.0 | 64.9 | 63.8 | 66.6 | 65.7 | 64.1 | 64.9 | 67.5 | 65.9 | 66.7 |
| 10 | 66.6 | 65.5 | 66.1 | 66.1 | 65.1 | 64.1 | 66.8 | 65.5 | 63.4 | 65.0 | 67.6 | 65.5 | 66.6 |
| 9 | 66.6 | 66.8 | 66.8 | 66.5 | 65.4 | 64.2 | 66.9 | 66.0 | 64.8 | 65.3 | 67.6 | 65.7 | 66.7 |
| 8 | 64.4 | 63.4 | 65.7 | 65.2 | 63.7 | 64.1 | 66.7 | 64.7 | 62.4 | 64.3 | 67.2 | 65.5 | 66.4 |
| 7 | 62.8 | 61.4 | 65.5 | 65.9 | 64.6 | 62.8 | 66.5 | 64.7 | 62.3 | 63.9 | 67.1 | 65.3 | 66.3 |
| 6 | 63.7 | 65.4 | 66.4 | 66.1 | 64.4 | 63.4 | 66.6 | 65.0 | 62.2 | 63.8 | 67.1 | 65.3 | 66.2 |
| 5 | 65.5 | 66.7 | 66.5 | 64.9 | 63.7 | 63.3 | 66.5 | 65.8 | 63.6 | 65.0 | 67.4 | 65.6 | 66.5 |
| 4 | 66.8 | 67.0 | 66.9 | 66.9 | 65.8 | 64.8 | 67.0 | 66.4 | 64.8 | 65.3 | 67.6 | 66.2 | 67.0 |
| 3 | 66.9 | 66.9 | 66.9 | 66.9 | 66.2 | 64.9 | 67.2 | 66.7 | 65.6 | 65.7 | 67.8 | 66.4 | 67.2 |
| 2 | 67.3 | 67.1 | 67.2 | 67.2 | 66.6 | 65.0 | 67.6 | 67.0 | 66.4 | 66.3 | 68.1 | 66.7 | 67.5 |
| 1 | 67.9 | 67.2 | 67.7 | 67.6 | 67.3 | 66.0 | 68.1 | 67.6 | 67.3 | 66.7 | 68.5 | 67.2 | 68.1 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 2 | Interch |  | I-75 | NW 49 | T Inte | hange | 1-75 | SR 32 | Interc | ange | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > |


| Time |  |  |  |  |  | erage D | sity (v | $\mathrm{h} / \mathrm{mi} / \mathrm{l}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 27.5 | 27.4 | 23.3 | 25.1 | 25.4 | 26.0 | 22.0 | 24.3 | 25.1 | 24.9 | 18.4 | 22.0 | 21.9 |
| 11 | 30.2 | 29.8 | 25.3 | 27.2 | 27.5 | 28.2 | 23.3 | 25.3 | 26.0 | 25.7 | 19.0 | 22.8 | 22.5 |
| 10 | 29.4 | 29.7 | 24.9 | 26.4 | 26.8 | 27.4 | 22.7 | 25.1 | 26.0 | 25.4 | 18.8 | 22.9 | 22.4 |
| 9 | 29.4 | 29.0 | 24.3 | 25.9 | 26.3 | 27.0 | 22.4 | 24.5 | 25.0 | 24.9 | 18.6 | 22.6 | 22.3 |
| 8 | 31.5 | 33.6 | 26.2 | 28.2 | 28.9 | 28.8 | 24.2 | 27.1 | 28.1 | 27.3 | 20.1 | 24.1 | 23.8 |
| 7 | 35.5 | 35.9 | 28.0 | 29.4 | 30.0 | 31.1 | 25.5 | 28.3 | 29.5 | 28.9 | 21.2 | 25.3 | 24.9 |
| 6 | 34.9 | 33.3 | 27.4 | 29.3 | 30.0 | 30.6 | 25.1 | 28.1 | 29.4 | 28.6 | 20.8 | 25.0 | 24.8 |
| 5 | 33.0 | 31.7 | 26.9 | 29.2 | 29.7 | 29.8 | 24.4 | 26.2 | 27.1 | 26.5 | 19.6 | 23.5 | 23.1 |
| 4 | 28.4 | 27.9 | 23.7 | 25.2 | 25.6 | 26.2 | 21.9 | 23.8 | 24.3 | 24.2 | 18.1 | 21.4 | 21.1 |
| 3 | 26.9 | 26.5 | 22.2 | 23.5 | 23.8 | 24.2 | 20.2 | 22.0 | 22.4 | 22.4 | 16.6 | 19.7 | 19.4 |
| 2 | 24.3 | 23.6 | 19.7 | 20.8 | 20.9 | 21.5 | 17.6 | 18.8 | 18.9 | 18.9 | 14.1 | 17.0 | 16.7 |
| 1 | 19.0 | 18.7 | 15.6 | 16.6 | 16.6 | 16.9 | 14.0 | 15.1 | 15.1 | 15.2 | 11.3 | 13.5 | 13.2 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | I-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > |


| Time | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.9 | 68.8 | 68.4 | 65.7 | 66.7 | 66.0 | 66.7 | 68.1 | 67.7 | 66.0 | 66.5 | 67.8 | 67.2 | 61.6 | 64.3 |
| 11 | 68.6 | 68.7 | 68.3 | 65.5 | 66.1 | 65.2 | 66.1 | 67.9 | 67.6 | 65.9 | 66.2 | 67.7 | 67.0 | 59.7 | 63.5 |
| 10 | 68.7 | 68.6 | 68.3 | 65.7 | 66.8 | 65.8 | 66.6 | 68.1 | 67.6 | 66.2 | 66.6 | 67.8 | 67.1 | 61.1 | 63.5 |
| 9 | 68.7 | 68.7 | 68.3 | 65.5 | 66.5 | 66.0 | 66.5 | 68.0 | 67.6 | 66.2 | 66.7 | 67.8 | 67.2 | 62.0 | 63.6 |
| 8 | 68.7 | 68.6 | 68.3 | 65.6 | 66.6 | 65.7 | 66.4 | 68.0 | 67.6 | 66.1 | 66.3 | 67.6 | 66.9 | 60.3 | 62.9 |
| 7 | 68.4 | 68.0 | 67.7 | 65.6 | 66.2 | 65.1 | 65.7 | 67.9 | 67.3 | 65.5 | 65.8 | 67.5 | 66.6 | 55.2 | 59.3 |
| 6 | 68.4 | 68.5 | 68.0 | 66.0 | 66.5 | 65.5 | 66.0 | 68.0 | 67.5 | 65.6 | 66.0 | 67.7 | 66.8 | 56.7 | 61.3 |
| 5 | 68.4 | 68.7 | 68.1 | 65.7 | 66.2 | 65.5 | 66.2 | 67.9 | 67.5 | 65.9 | 66.4 | 67.8 | 66.9 | 60.3 | 63.5 |
| 4 | 68.8 | 68.7 | 68.3 | 66.1 | 67.0 | 66.1 | 66.7 | 68.2 | 67.7 | 66.1 | 66.8 | 67.8 | 67.2 | 63.4 | 65.0 |
| 3 | 68.8 | 68.7 | 68.4 | 66.0 | 67.1 | 66.1 | 66.9 | 68.2 | 67.8 | 66.4 | 66.9 | 67.9 | 67.3 | 63.2 | 65.4 |
| 2 | 69.0 | 69.0 | 68.6 | 66.2 | 67.2 | 66.5 | 67.3 | 68.3 | 68.0 | 66.6 | 67.3 | 68.0 | 67.6 | 64.9 | 66.4 |
| 1 | 69.4 | 69.3 | 69.0 | 66.6 | 67.9 | 67.2 | 67.9 | 68.5 | 68.4 | 67.0 | 67.9 | 68.3 | 68.1 | 66.0 | 67.4 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time Period | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 14.8 | 14.6 | 13.2 | 18.3 | 17.9 | 19.5 | 19.3 | 19.0 | 17.6 | 21.9 | 21.9 | 21.5 | 20.4 | 27.7 | 26.6 |
| 11 | 16.4 | 16.2 | 14.5 | 19.8 | 19.7 | 21.6 | 21.2 | 20.6 | 19.0 | 23.5 | 23.3 | 22.7 | 21.5 | 29.9 | 27.9 |
| 10 | 16.0 | 15.8 | 14.2 | 19.2 | 18.9 | 20.5 | 20.3 | 19.9 | 18.4 | 22.8 | 22.7 | 22.1 | 21.2 | 29.0 | 27.9 |
| 9 | 16.0 | 15.7 | 14.1 | 19.4 | 19.1 | 20.7 | 20.5 | 20.0 | 18.4 | 22.6 | 22.4 | 22.0 | 20.9 | 28.2 | 27.4 |
| 8 | 15.7 | 15.5 | 14.1 | 19.5 | 19.1 | 20.8 | 20.7 | 20.3 | 18.8 | 23.3 | 23.4 | 23.0 | 21.9 | 30.0 | 28.7 |
| 7 | 18.6 | 18.5 | 16.6 | 21.7 | 21.5 | 23.6 | 23.3 | 22.5 | 20.9 | 26.0 | 25.9 | 25.1 | 23.9 | 36.0 | 33.2 |
| 6 | 18.7 | 18.4 | 16.4 | 21.1 | 20.9 | 22.9 | 22.8 | 22.1 | 20.4 | 25.6 | 25.5 | 24.8 | 23.6 | 34.1 | 31.3 |
| 5 | 18.2 | 17.7 | 15.8 | 20.8 | 20.6 | 22.3 | 22.1 | 21.4 | 19.7 | 24.3 | 24.0 | 23.3 | 22.3 | 30.4 | 28.6 |
| 4 | 15.6 | 15.3 | 13.8 | 18.4 | 18.1 | 19.7 | 19.4 | 19.0 | 17.6 | 21.9 | 21.7 | 21.2 | 20.1 | 26.3 | 25.6 |
| 3 | 14.8 | 14.6 | 13.1 | 17.6 | 17.3 | 18.9 | 18.6 | 18.2 | 16.7 | 20.6 | 20.4 | 20.0 | 19.1 | 24.9 | 24.0 |
| 2 | 13.6 | 13.3 | 11.9 | 15.7 | 15.4 | 16.6 | 16.4 | 16.1 | 14.8 | 18.3 | 18.0 | 17.6 | 16.6 | 21.2 | 20.5 |
| 1 | 10.8 | 10.6 | 9.6 | 12.7 | 12.4 | 13.4 | 13.3 | 13.0 | 12.0 | 14.7 | 14.5 | 14.2 | 13.3 | 16.7 | 16.3 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > |  |

AVERAGE SPEED DIFFERENCE (mph)
Diff.: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph $\begin{array}{ccccccc}\text { Upper: } & 70 & <65 & <60 & <55 & <50 & <45 \\ \text { Lower: } & 65 & 60 & 55 & 50 & 45 & 0\end{array}$ (Posted Speed-Avg. Speed)

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{lllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0>$
Using HCM 2010 thresholds for informational purposes


Volume (vph): XXXX Difference greater than 400vph (Based on FDOT Traffic Analysis Handbook Calibration Volume $>2,700$ vph

| NORTHBOUND I-75-TIME PLOTS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 67.5 | 66.8 | 67.4 | 67.1 | 66.7 | 64.5 | 67.9 | 66.9 | 66.2 | 65.5 | 68.5 | 66.1 | 67.7 |
| 11 | 67.3 | 66.8 | 67.3 | 66.9 | 66.5 | 64.6 | 67.7 | 66.3 | 65.5 | 65.0 | 68.3 | 66.1 | 67.6 |
| 10 | 67.0 | 66.6 | 67.1 | 66.5 | 65.9 | 64.4 | 67.5 | 66.3 | 65.3 | 64.9 | 68.1 | 65.9 | 67.3 |
| 9 | 66.4 | 64.6 | 66.4 | 66.4 | 65.4 | 63.2 | 67.3 | 65.2 | 64.3 | 61.2 | 68.0 | 66.2 | 67.4 |
| 8 | 66.4 | 66.4 | 66.9 | 66.5 | 65.5 | 63.7 | 67.3 | 65.8 | 64.5 | 63.0 | 68.1 | 66.2 | 67.3 |
| 7 | 66.4 | 66.3 | 66.9 | 66.7 | 65.7 | 63.9 | 67.4 | 66.1 | 64.7 | 64.4 | 68.0 | 66.2 | 67.3 |
| 6 | 66.7 | 66.4 | 67.2 | 66.5 | 65.9 | 64.3 | 67.4 | 65.9 | 64.7 | 64.2 | 68.1 | 66.1 | 67.4 |
| 5 | 66.7 | 66.6 | 67.0 | 66.6 | 65.7 | 64.1 | 67.5 | 66.1 | 64.8 | 64.3 | 68.1 | 66.2 | 67.3 |
| 4 | 66.7 | 66.4 | 66.8 | 66.5 | 65.8 | 64.2 | 67.3 | 66.1 | 65.0 | 64.4 | 68.1 | 66.2 | 67.3 |
| 3 | 66.7 | 66.4 | 67.0 | 66.7 | 66.0 | 64.2 | 67.4 | 66.4 | 65.2 | 64.9 | 68.1 | 66.1 | 67.4 |
| 2 | 67.2 | 66.7 | 67.2 | 66.8 | 66.3 | 64.3 | 67.6 | 66.3 | 65.2 | 64.8 | 68.3 | 66.5 | 67.7 |
| 1 | 67.1 | 66.8 | 67.3 | 66.8 | 66.2 | 64.3 | 67.7 | 66.5 | 65.6 | 65.1 | 68.3 | 66.4 | 67.7 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction | Travel | > | > | > | > | > | > | > | > | > | > | > | > |


| Time | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 22.1 | 22.2 | 17.9 | 19.5 | 19.7 | 20.6 | 16.1 | 17.8 | 18.0 | 18.3 | 12.3 | 16.0 | 15.7 |
| 11 | 23.9 | 24.0 | 19.4 | 20.9 | 21.0 | 21.7 | 17.1 | 19.0 | 19.3 | 19.5 | 13.1 | 16.8 | 16.4 |
| 10 | 25.5 | 25.9 | 21.0 | 22.6 | 22.9 | 23.7 | 18.8 | 20.9 | 21.1 | 21.3 | 14.3 | 18.2 | 17.9 |
| 9 | 29.2 | 30.4 | 23.5 | 24.8 | 25.3 | 26.3 | 20.0 | 22.5 | 22.8 | 24.7 | 15.0 | 18.7 | 18.4 |
| 8 | 29.6 | 29.2 | 23.6 | 25.3 | 25.7 | 26.6 | 20.7 | 22.8 | 23.2 | 24.1 | 15.5 | 19.2 | 18.9 |
| 7 | 29.5 | 29.0 | 23.4 | 24.8 | 25.2 | 26.1 | 20.1 | 22.3 | 22.7 | 22.8 | 15.2 | 19.0 | 18.6 |
| 6 | 27.6 | 27.5 | 22.0 | 23.9 | 24.0 | 24.8 | 19.3 | 21.4 | 21.9 | 22.2 | 14.5 | 18.3 | 17.9 |
| 5 | 28.4 | 28.0 | 22.7 | 24.2 | 24.6 | 25.4 | 19.6 | 21.9 | 22.4 | 22.6 | 14.8 | 18.5 | 18.2 |
| 4 | 28.0 | 27.9 | 22.8 | 24.3 | 24.6 | 25.4 | 20.0 | 22.1 | 22.5 | 22.7 | 15.0 | 18.6 | 18.3 |
| 3 | 27.9 | 27.5 | 22.1 | 23.7 | 23.9 | 24.6 | 19.1 | 20.8 | 21.2 | 21.3 | 14.3 | 17.8 | 17.4 |
| 2 | 25.2 | 25.1 | 20.4 | 22.0 | 22.2 | 23.1 | 17.9 | 19.9 | 20.3 | 20.5 | 13.6 | 16.8 | 16.7 |
| 1 | 25.9 | 25.7 | 20.5 | 22.2 | 22.4 | 23.1 | 17.9 | 19.7 | 20.0 | 20.1 | 13.5 | 16.9 | 16.5 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > |


| Time | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.6 | 68.6 | 68.1 | 65.6 | 66.2 | 65.5 | 66.0 | 67.8 | 67.4 | 66.4 | 66.4 | 67.8 | 67.0 | 60.6 | 62.2 |
| 11 | 68.4 | 68.5 | 67.9 | 65.5 | 66.1 | 65.2 | 65.4 | 67.8 | 67.3 | 66.3 | 66.3 | 67.7 | 66.2 | 50.7 | 57.2 |
| 10 | 68.3 | 68.3 | 67.6 | 65.5 | 65.1 | 65.0 | 65.6 | 67.9 | 67.3 | 65.9 | 65.6 | 67.6 | 59.9 | 35.0 | 52.4 |
| 9 | 67.8 | 68.1 | 67.4 | 65.4 | 64.8 | 63.5 | 63.9 | 67.5 | 67.0 | 65.9 | 65.4 | 67.3 | 56.8 | 28.5 | 50.7 |
| 8 | 67.7 | 67.8 | 67.1 | 65.3 | 64.4 | 63.3 | 63.8 | 67.2 | 66.8 | 65.5 | 64.9 | 66.6 | 59.9 | 29.4 | 51.1 |
| 7 | 67.7 | 68.3 | 67.4 | 65.6 | 65.3 | 63.6 | 63.7 | 67.4 | 66.9 | 65.6 | 65.1 | 67.5 | 63.4 | 36.0 | 52.1 |
| 6 | 68.0 | 67.5 | 67.2 | 65.7 | 65.5 | 64.4 | 64.5 | 67.6 | 67.1 | 65.7 | 65.2 | 67.5 | 63.2 | 36.7 | 51.9 |
| 5 | 67.8 | 67.5 | 67.2 | 65.5 | 65.2 | 63.8 | 63.8 | 67.5 | 67.0 | 65.5 | 64.8 | 67.5 | 63.4 | 37.3 | 51.8 |
| 4 | 67.8 | 67.7 | 67.2 | 65.5 | 65.2 | 64.8 | 65.0 | 67.8 | 67.2 | 65.0 | 65.2 | 67.6 | 65.0 | 40.2 | 53.9 |
| 3 | 67.8 | 68.2 | 67.4 | 65.3 | 64.2 | 64.0 | 64.3 | 67.6 | 67.1 | 65.8 | 65.6 | 67.6 | 66.4 | 51.9 | 58.5 |
| 2 | 68.2 | 68.1 | 67.7 | 65.9 | 66.1 | 64.8 | 65.7 | 67.8 | 67.3 | 65.9 | 66.0 | 67.6 | 66.7 | 57.0 | 60.4 |
| 1 | 68.1 | 68.3 | 67.6 | 65.9 | 66.0 | 64.8 | 65.4 | 67.8 | 67.2 | 66.0 | 65.9 | 67.7 | 66.8 | 59.8 | 61.9 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | ravel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 17.3 | 17.1 | 15.7 | 20.9 | 20.7 | 22.2 | 22.0 | 21.5 | 20.0 | 23.3 | 23.3 | 22.8 | 21.9 | 29.6 | 29.0 |
| 11 | 18.8 | 18.6 | 17.0 | 22.6 | 22.4 | 24.1 | 24.1 | 23.2 | 21.5 | 24.9 | 25.0 | 24.3 | 23.7 | 40.6 | 35.0 |
| 10 | 19.9 | 19.7 | 18.1 | 23.3 | 23.4 | 24.7 | 24.5 | 23.8 | 22.3 | 26.4 | 26.7 | 25.9 | 29.5 | 67.6 | 41.6 |
| 9 | 22.9 | 22.5 | 20.5 | 25.5 | 25.9 | 28.0 | 27.8 | 26.2 | 24.4 | 28.6 | 28.8 | 27.9 | 35.0 | 79.8 | 43.9 |
| 8 | 23.4 | 23.0 | 21.1 | 26.2 | 26.5 | 28.6 | 28.5 | 27.2 | 25.1 | 29.3 | 29.6 | 28.9 | 33.1 | 78.7 | 43.4 |
| 7 | 23.7 | 23.2 | 21.3 | 26.2 | 26.4 | 28.6 | 28.4 | 26.8 | 24.7 | 28.9 | 29.0 | 27.8 | 28.9 | 64.0 | 42.0 |
| 6 | 22.1 | 21.9 | 19.8 | 24.7 | 24.7 | 26.7 | 26.7 | 25.4 | 23.4 | 27.9 | 28.1 | 27.1 | 28.3 | 64.5 | 42.3 |
| 5 | 22.7 | 22.5 | 20.6 | 25.6 | 25.7 | 27.7 | 27.8 | 26.3 | 24.3 | 28.5 | 28.8 | 27.4 | 28.5 | 61.2 | 41.9 |
| 4 | 22.4 | 22.1 | 20.0 | 24.8 | 25.0 | 26.6 | 26.5 | 25.4 | 23.6 | 28.1 | 28.0 | 27.0 | 26.9 | 55.8 | 39.6 |
| 3 | 22.5 | 22.0 | 20.0 | 25.1 | 25.5 | 27.1 | 26.9 | 25.6 | 23.6 | 27.5 | 27.5 | 26.6 | 25.6 | 40.2 | 34.4 |
| 2 | 19.9 | 19.7 | 17.9 | 22.7 | 22.6 | 24.4 | 24.0 | 23.3 | 21.6 | 25.5 | 25.6 | 24.9 | 24.0 | 34.4 | 32.4 |
| 1 | 20.9 | 20.5 | 18.7 | 23.2 | 23.2 | 25.1 | 24.9 | 23.9 | 22.2 | 26.0 | 26.1 | 25.3 | 24.2 | 32.4 | 31.3 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | $>$ | > | > | > | > | > | > | > | > | > | > |

AVERAGE SPEED DIFFERENCE (mph
Diff.: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph Upper: $70<65 \quad<60<55<50<45$ Lower: 65 60

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: $\operatorname{LOSA} \operatorname{LOSB} \operatorname{LOS} C$ LOSD LOSE LOSF
Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
$\begin{array}{lllllll}\text { Upper: } & 10.0 & 18.0 & 26.0 & 35.0 & 45.0 & >\end{array}$
Using HCM 2010 thresholds for informational purposes


Volume (vph): XXXX Difference greater than 400vph (Based on FDOT Traffic Analysis Handbook Calibration Volume> 2,700 vph)

Figure 6-25: SPUI 2045 Speed and Density Time Plots (AM Peak)

NORTHBOUND I-75 - TIME PLOTS

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  |  |  | Average | Speed | mph) |  |  |  |  |  |
| 12 | 66.8 | 66.9 | 66.9 | 66.7 | 66.4 | 68.4 | 67.2 | 66.1 | 64.9 | 65.8 | 67.6 | 66.0 | 66.6 |
| 11 | 66.5 | 66.6 | 66.4 | 66.4 | 65.9 | 68.3 | 67.1 | 66.3 | 65.1 | 65.7 | 67.5 | 65.8 | 66.6 |
| 10 | 65.9 | 65.0 | 65.8 | 66.2 | 65.9 | 68.3 | 67.0 | 65.7 | 65.0 | 65.3 | 67.4 | 65.7 | 66.6 |
| 9 | 63.5 | 61.8 | 66.0 | 66.4 | 66.0 | 68.4 | 67.2 | 65.8 | 64.7 | 65.1 | 67.2 | 65.8 | 66.6 |
| 8 | 60.9 | 58.8 | 64.8 | 66.1 | 65.6 | 68.2 | 67.0 | 65.4 | 64.1 | 64.5 | 67.4 | 65.5 | 66.4 |
| 7 | 60.3 | 53.7 | 63.5 | 63.9 | 64.2 | 68.1 | 67.0 | 65.4 | 63.9 | 65.3 | 67.2 | 65.3 | 66.2 |
| 6 | 63.3 | 58.9 | 65.3 | 66.1 | 65.6 | 68.4 | 67.1 | 64.6 | 63.2 | 64.7 | 67.4 | 65.5 | 66.3 |
| 5 | 65.5 | 66.7 | 66.5 | 66.4 | 65.6 | 68.3 | 67.0 | 64.9 | 64.3 | 65.3 | 67.5 | 65.9 | 66.6 |
| 4 | 66.8 | 67.0 | 66.9 | 66.9 | 66.5 | 68.5 | 67.1 | 66.5 | 65.8 | 65.9 | 67.6 | 66.1 | 66.9 |
| 3 | 66.9 | 66.9 | 66.9 | 67.0 | 66.6 | 68.5 | 67.4 | 66.7 | 66.1 | 66.0 | 67.7 | 66.5 | 67.2 |
| 2 | 67.3 | 67.1 | 67.2 | 67.3 | 67.1 | 68.6 | 67.7 | 67.0 | 66.8 | 66.7 | 68.1 | 66.6 | 67.6 |
| 1 | 67.9 | 67.2 | 67.7 | 67.7 | 67.6 | 68.8 | 68.1 | 67.6 | 67.6 | 67.0 | 68.5 | 67.1 | 68.1 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,702 | 1,502 | 6,475 | 1,502 | 3,033 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | $>$ |


| Time Period | Average Density (veh/mi/nn) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 27.5 | 27.5 | 23.3 | 24.9 | 25.1 | 24.1 | 21.8 | 24.2 | 24.8 | 24.6 | 18.4 | 21.9 | 21.9 |
| 11 | 30.2 | 29.8 | 25.3 | 27.0 | 27.1 | 25.8 | 23.1 | 25.2 | 25.6 | 25.4 | 19.0 | 22.7 | 22.5 |
| 10 | 29.9 | 30.2 | 25.2 | 26.7 | 26.9 | 25.6 | 23.0 | 25.4 | 25.7 | 25.7 | 19.2 | 23.1 | 22.8 |
| 9 | 32.3 | 35.3 | 24.9 | 26.3 | 26.4 | 25.1 | 22.5 | 24.9 | 25.3 | 25.1 | 18.8 | 22.6 | 22.4 |
| 8 | 35.4 | 38.6 | 26.4 | 27.4 | 27.8 | 26.6 | 23.9 | 26.5 | 27.1 | 27.1 | 20.0 | 24.0 | 23.8 |
| 7 | 37.8 | 44.4 | 29.0 | 30.7 | 30.3 | 28.0 | 25.1 | 27.8 | 28.6 | 28.0 | 20.9 | 25.0 | 24.6 |
| 6 | 35.1 | 38.1 | 27.6 | 28.9 | 29.0 | 27.5 | 24.6 | 28.1 | 28.8 | 28.1 | 20.7 | 24.9 | 24.6 |
| 5 | 33.0 | 31.7 | 26.9 | 28.4 | 28.6 | 27.2 | 24.2 | 26.8 | 26.8 | 26.3 | 19.6 | 23.4 | 23.2 |
| 4 | 28.4 | 27.9 | 23.7 | 25.3 | 25.4 | 24.2 | 21.8 | 23.9 | 24.0 | 24.0 | 18.1 | 21.5 | 21.1 |
| 3 | 26.9 | 26.5 | 22.2 | 23.5 | 23.6 | 22.6 | 20.2 | 22.0 | 22.2 | 22.3 | 16.6 | 19.6 | 19.4 |
| 2 | 24.3 | 23.5 | 19.7 | 20.8 | 20.7 | 20.0 | 17.5 | 19.0 | 18.9 | 18.8 | 14.2 | 17.0 | 16.7 |
| 1 | 19.0 | 18.7 | 15.6 | 16.6 | 16.5 | 15.9 | 14.0 | 15.1 | 15.1 | 15.1 | 11.3 | 13.5 | 13.2 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,702 | 1,502 | 6,475 | 1,502 | 3,033 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > |


| SOUTHBOUND I-75-TIME PLOTS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 68.9 | 68.8 | 68.4 | 65.7 | 66.9 | 66.0 | 66.9 | 68.5 | 67.7 | 66.3 | 66.8 | 67.8 | 67.2 | 62.2 | 64.5 |
| 11 | 68.6 | 68.7 | 68.3 | 65.5 | 66.5 | 65.4 | 66.6 | 68.4 | 67.6 | 66.1 | 66.5 | 67.7 | 67.2 | 61.7 | 64.5 |
| 10 | 68.7 | 68.6 | 68.3 | 65.7 | 66.7 | 65.9 | 66.8 | 68.4 | 67.6 | 66.1 | 66.6 | 67.8 | 67.1 | 62.4 | 63.8 |
| 9 | 68.7 | 68.7 | 68.3 | 65.5 | 66.5 | 65.8 | 66.7 | 68.4 | 67.6 | 66.3 | 66.6 | 67.8 | 67.1 | 62.1 | 64.5 |
| 8 | 68.7 | 68.6 | 68.3 | 65.6 | 66.6 | 65.7 | 66.7 | 68.4 | 67.6 | 66.1 | 66.2 | 67.6 | 67.0 | 60.1 | 62.1 |
| 7 | 68.4 | 68.0 | 67.7 | 65.7 | 66.2 | 64.8 | 66.0 | 68.3 | 67.4 | 65.4 | 65.9 | 67.6 | 66.7 | 56.0 | 60.5 |
| 6 | 68.4 | 68.5 | 68.0 | 65.8 | 66.3 | 65.1 | 66.1 | 68.4 | 67.4 | 65.6 | 65.8 | 67.7 | 66.8 | 57.2 | 60.2 |
| 5 | 68.4 | 68.7 | 68.1 | 65.8 | 66.4 | 65.4 | 66.4 | 68.4 | 67.5 | 66.0 | 66.4 | 67.8 | 67.0 | 60.8 | 63.6 |
| 4 | 68.8 | 68.7 | 68.3 | 66.0 | 67.0 | 66.0 | 66.9 | 68.5 | 67.7 | 66.3 | 66.7 | 67.8 | 67.2 | 62.9 | 64.5 |
| 3 | 68.8 | 68.7 | 68.4 | 66.0 | 67.0 | 66.1 | 67.0 | 68.4 | 67.8 | 66.5 | 67.0 | 67.9 | 67.3 | 63.9 | 65.4 |
| 2 | 69.0 | 69.0 | 68.6 | 66.2 | 67.4 | 66.5 | 67.4 | 68.6 | 68.0 | 66.7 | 67.3 | 68.0 | 67.7 | 64.9 | 66.4 |
| 1 | 69.4 | 69.3 | 69.0 | 66.5 | 67.8 | 67.2 | 68.0 | 68.8 | 68.4 | 67.0 | 67.9 | 68.3 | 68.2 | 66.3 | 67.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,666 | 1,499 | 6,918 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 14.8 | 14.6 | 13.2 | 18.3 | 17.9 | 19.5 | 19.2 | 18.8 | 17.7 | 21.7 | 21.8 | 21.4 | 20.4 | 27.4 | 26.4 |
| 11 | 16.4 | 16.2 | 14.5 | 19.7 | 19.4 | 21.4 | 20.8 | 20.3 | 19.0 | 23.2 | 23.2 | 22.8 | 21.5 | 28.8 | 27.4 |
| 10 | 16.0 | 15.8 | 14.2 | 19.4 | 19.1 | 20.6 | 20.2 | 19.8 | 18.6 | 22.8 | 22.8 | 22.3 | 21.3 | 28.4 | 27.8 |
| 9 | 16.0 | 15.7 | 14.1 | 19.3 | 19.0 | 20.7 | 20.2 | 19.8 | 18.4 | 22.4 | 22.4 | 21.8 | 20.9 | 28.1 | 27.0 |
| 8 | 15.7 | 15.5 | 14.1 | 19.5 | 19.1 | 20.8 | 20.5 | 20.0 | 18.8 | 23.0 | 23.4 | 23.0 | 21.7 | 30.1 | 29.2 |
| 7 | 18.6 | 18.5 | 16.6 | 21.7 | 21.5 | 23.7 | 23.0 | 22.3 | 20.9 | 25.9 | 25.9 | 25.1 | 23.9 | 35.1 | 32.2 |
| 6 | 18.7 | 18.4 | 16.4 | 21.3 | 21.1 | 23.1 | 22.7 | 22.0 | 20.6 | 25.5 | 25.6 | 24.9 | 23.7 | 34.4 | 32.3 |
| 5 | 18.2 | 17.7 | 15.8 | 20.7 | 20.4 | 22.3 | 21.8 | 21.2 | 19.7 | 24.1 | 24.0 | 23.3 | 22.3 | 30.0 | 28.5 |
| 4 | 15.6 | 15.3 | 13.8 | 18.6 | 18.2 | 19.8 | 19.4 | 19.0 | 17.7 | 21.7 | 21.7 | 21.2 | 20.1 | 26.5 | 25.8 |
| 3 | 14.8 | 14.6 | 13.1 | 17.6 | 17.3 | 18.8 | 18.4 | 18.0 | 16.8 | 20.4 | 20.4 | 20.0 | 19.1 | 24.6 | 24.0 |
| 2 | 13.6 | 13.3 | 11.9 | 15.7 | 15.4 | 16.7 | 16.2 | 15.9 | 14.8 | 18.1 | 18.0 | 17.6 | 16.7 | 21.2 | 20.6 |
| 1 | 10.8 | 10.6 | 9.6 | 12.7 | 12.4 | 13.4 | 13.1 | 12.9 | 12.0 | 14.6 | 14.4 | 14.2 | 13.3 | 16.7 | 16.3 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,666 | 1,499 | 6,918 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | avel |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## LOS THRESHOLDS (Density in veh/mi/ln)

LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0 \quad>$
Using HCM 2010 thresholds for informational purposes

Figure 6-26: SPUI 2045 Volume Time Plots (AM Peak)

| NORTHBOUND I-75-TIME PLOT |  |  |  |  |  |  |  |  |  |  |  |  |  |  | SOUTHBOUND I-75-TIME PLOT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |  |  |  |  | Time Period | Average Volume (vph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | Processed | 5503 | 5506 | 4670 | 4995 | 5001 | 4952 | 4401 | 4788 | 4819 | 4852 | 3729 | 4339 | 4381 | 12 | Processed | 3060 | 3013 | 2716 | 3604 | 3599 | 3863 | 3851 | 3875 | 3595 | 4307 | 4366 | 4357 | 4106 | 5098 | 5116 |
|  | Demand | 5412 | 5412 | 4544 | 4823 | 4823 | 4823 | 4202 | 4547 | 4547 | 4547 | 3507 | 4111 | 4111 |  | Demand | 3066 | 3066 | 2698 | 3497 | 3497 | 3752 | 3752 | 3752 | 3460 | 4195 | 4195 | 4195 | 3940 | 4849 | 4849 |
|  | Diff. | 91 | 94 | 126 | 172 | 178 | 129 | 199 | 241 | 272 | 305 | 222 | 228 | 270 |  | Diff. | -6 | -53 | 18 | 107 | 102 | 111 | 99 | 123 | 135 | 112 | 171 | 162 | 166 | 249 | 267 |
|  | Processed | 6025 | 5945 | 5034 | 5366 | 5358 | 5295 | 4654 | 5006 | 4991 | 4991 | 3836 | 4493 | 4495 | 11 | Processed | 3383 | 3338 | 2972 | 3862 | 3866 | 4185 | 4159 | 4183 | 3861 | 4610 | 4631 | 4621 | 4328 | 5311 | 5301 |
| 11 | Demand | 6023 | 6023 | 5057 | 5367 | 5367 | 5367 | 4676 | 5061 | 5061 | 5061 | 3903 | 4575 | 4575 |  | Demand | 3412 | 3412 | 3003 | 3891 | 3891 | 4176 | 4176 | 4176 | 3851 | 4669 | 4669 | 4669 | 4385 | 5397 | 5397 |
|  | Diff. | 2 | -78 | -23 | -1 | -9 | -72 | -22 | -55 | -70 | -70 | -67 | -82 | -80 |  | Diff. | -29 | -74 | -31 | -29 | -25 | 9 | -17 | 7 | 10 | -59 | -38 | -48 | -57 | -86 | -96 |
|  | Processed | 5889 | 5873 | 4982 | 5302 | 5309 | 5248 | 4620 | 5005 | 5013 | 5015 | 3875 | 4551 | 4553 | 10 | Processed | 3298 | 3244 | 2900 | 3819 | 3820 | 4080 | 4054 | 4074 | 3763 | 4521 | 4555 | 4531 | 4280 | 5307 | 5313 |
| 10 | Demand | 5849 | 5849 | 4911 | 5212 | 5212 | 5212 | 4541 | 4914 | 4914 | 4914 | 3790 | 4443 | 4443 |  | Demand | 3314 | 3314 | 2916 | 3779 | 3779 | 4055 | 4055 | 4055 | 3739 | 4534 | 4534 | 4534 | 4258 | 5241 | 5241 |
|  | Diff. | 40 | 24 | 71 | 90 | 97 | 36 | 79 | 91 | 99 | 101 | 85 | 108 | 110 |  | Diff. | -16 | -70 | -16 | 40 | 41 | 25 | -1 | 19 | 24 | -13 | 21 | -3 | 22 | 66 | 72 |
|  | Processed | 5907 | 5867 | 4921 | 5227 | 5223 | 5157 | 4539 | 4892 | 4886 | 4889 | 3780 | 4467 | 4468 | 9 | Processed | 3290 | 3232 | 2881 | 3794 | 3795 | 4077 | 4044 | 4064 | 3728 | 4447 | 4470 | 4448 | 4205 | 5213 | 5218 |
| 9 | Demand | 5858 | 5858 | 4918 | 5220 | 5220 | 5220 | 4548 | 4922 | 4922 | 4922 | 3795 | 4449 | 4449 |  | Demand | 3319 | 3319 | 2920 | 3784 | 3784 | 4061 | 4061 | 4061 | 3745 | 4540 | 4540 | 4540 | 4265 | 5249 | 5249 |
|  | Diff. | 49 | 9 | 3 | 7 | 3 | -63 | -9 | -30 | -36 | -33 | -15 | 18 | 19 |  | Diff. | -29 | -87 | -39 | 10 | 11 | 16 | -17 | 3 | -17 | -93 | -70 | -92 | -60 | -36 | -31 |
|  | Processed | 6000 | 6041 | 5115 | 5433 | 5469 | 5437 | 4808 | 5197 | 5198 | 5223 | 4049 | 4730 | 4749 | 8 | Processed | 3238 | 3200 | 2886 | 3821 | 3821 | 4099 | 4094 | 4120 | 3816 | 4569 | 4640 | 4656 | 4362 | 5389 | 5421 |
| 8 | Demand | 5723 | 5723 | 4805 | 5100 | 5100 | 5100 | 4443 | 4809 | 4809 | 4809 | 3708 | 4347 | 4347 |  | Demand | 3242 | 3242 | 2853 | 3698 | 3698 | 3968 | 3968 | 3968 | 3659 | 4436 | 4436 | 4436 | 4167 | 5128 | 5128 |
|  | Diff. | 277 | 318 | 310 | 333 | 369 | 337 | 365 | 388 | 389 | 414 | 341 | 383 | 402 |  | Diff. | -4 | -42 | 33 | 123 | 123 | 131 | 126 | 152 | 157 | 133 | 204 | 220 | 195 | 261 | 293 |
|  | Processed | 6546 | 6438 | 5479 | 5805 | 5798 | 5725 | 5034 | 5447 | 5461 | 5464 | 4206 | 4893 | 4879 | 7 | Processed | 3824 | 3761 | 3373 | 4275 | 4271 | 4597 | 4558 | 4576 | 4217 | 5078 | 5113 | 5092 | 4789 | 5794 | 5811 |
| 7 | Demand | 6782 | 6782 | 5694 | 6044 | 6044 | 6044 | 5265 | 5698 | 5698 | 5698 | 4394 | 5152 | 5152 |  | Demand | 3842 | 3842 | 3381 | 4382 | 4382 | 4702 | 4702 | 4702 | 4336 | 5257 | 5257 | 5257 | 4938 | 6077 | 6077 |
|  | Diff. | -236 | -344 | -215 | -239 | -246 | -319 | -231 | -251 | -237 | -234 | -188 | -259 | -273 |  | Diff. | -18 | -81 | -8 | -107 | -111 | -105 | -144 | -126 | -119 | -179 | -144 | -165 | -149 | -283 | -266 |
|  | Processed | 6606 | 6461 | 5388 | 5728 | 5710 | 5631 | 4961 | 5414 | 5430 | 5439 | 4176 | 4891 | 4901 | 6 | Processed | 3831 | 3779 | 3352 | 4200 | 4197 | 4513 | 4496 | 4510 | 4169 | 5022 | 5061 | 5041 | 4741 | 5773 | 5755 |
| 6 | Demand | 6822 | 6822 | 5728 | 6079 | 6079 | 6079 | 5296 | 5732 | 5732 | 5732 | 4420 | 5182 | 5182 |  | Demand | 3865 | 3865 | 3401 | 4407 | 4407 | 4730 | 4730 | 4730 | 4361 | 5288 | 5288 | 5288 | 4967 | 6113 | 6113 |
|  | Diff. | -216 | -361 | -340 | -351 | -369 | -448 | -335 | -318 | -302 | -293 | -244 | -291 | -281 |  | Diff. | -34 | -86 | -49 | -207 | -210 | -217 | -234 | -220 | -192 | -266 | -227 | -247 | -226 | -340 | -358 |
|  | Processed | 6488 | 6323 | 5362 | 5652 | 5632 | 5566 | 4854 | 5215 | 5169 | 5157 | 3968 | 4629 | 4633 | 5 | Processed | 3739 | 3650 | 3236 | 4078 | 4074 | 4369 | 4335 | 4351 | 3990 | 4768 | 4772 | 4737 | 4482 | 5459 | 5438 |
| 5 | Demand | 6676 | 6676 | 5605 | 5949 | 5949 | 5949 | 5183 | 5609 | 5609 | 5609 | 4326 | 5071 | 5071 |  | Demand | 3782 | 3782 | 3328 | 4313 | 4313 | 4629 | 4629 | 4629 | 4268 | 5175 | 5175 | 5175 | 4861 | 5982 | 5982 |
|  | Diff. | -188 | -353 | -243 | -297 | -317 | -383 | -329 | -394 | -440 | -452 | -358 | -442 | -438 |  | Diff. | -43 | -132 | -92 | -235 | -239 | -260 | -294 | -278 | -278 | -407 | -403 | -438 | -379 | -523 | -544 |
|  | Processed | 5694 | 5603 | 4755 | 5061 | 5061 | 4979 | 4384 | 4750 | 4734 | 4724 | 3660 | 4252 | 4245 | 4 | Processed | 3214 | 3162 | 2827 | 3668 | 3666 | 3924 | 3887 | 3897 | 3592 | 4311 | 4337 | 4314 | 4047 | 4980 | 4993 |
| 4 | Demand | 5761 | 5761 | 4837 | 5133 | 5133 | 5133 | 4472 | 4840 | 4840 | 4840 | 3732 | 4376 | 4376 |  | Demand | 3264 | 3264 | 2872 | 3722 | 3722 | 3994 | 3994 | 3994 | 3683 | 4465 | 4465 | 4465 | 4194 | 5162 | 5162 |
|  | Diff. | -67 | -158 | -82 | -72 | -72 | -154 | -88 | -90 | -106 | -116 | -72 | -124 | -131 |  | Diff. | -50 | -102 | -45 | -54 | -56 | -70 | -107 | -97 | -91 | -154 | -128 | -151 | -147 | -182 | -169 |
|  | Processed | 5404 | 5303 | 4455 | 4721 | 4704 | 4634 | 4075 | 4408 | 4403 | 4402 | 3374 | 3924 | 3916 | 3 | Processed | 3066 | 3015 | 2694 | 3479 | 3474 | 3737 | 3703 | 3708 | 3418 | 4072 | 4098 | 4080 | 3859 | 4711 | 4701 |
| 3 | Demand | 5503 | 5503 | 4620 | 4903 | 4903 | 4903 | 4272 | 4623 | 4623 | 4623 | 3565 | 4180 | 4180 |  | Demand | 3117 | 3117 | 2743 | 3555 | 3555 | 3815 | 3815 | 3815 | 3518 | 4265 | 4265 | 4265 | 4006 | 4930 | 4930 |
|  | Diff. | -99 | -200 | -165 | -182 | -199 | -269 | -197 | -215 | -220 | -221 | -191 | -256 | -264 |  | Diff. | -51 | -102 | -49 | -76 | -81 | -78 | -112 | -107 | -100 | -193 | -167 | -185 | -147 | -219 | -229 |
|  | Processed | 4908 | 4738 | 3981 | 4197 | 4175 | 4109 | 3564 | 3820 | 3780 | 3760 | 2892 | 3402 | 3388 | 2 | Processed | 2818 | 2750 | 2441 | 3111 | 3102 | 3321 | 3283 | 3291 | 3018 | 3628 | 3634 | 3596 | 3380 | 4119 | 4101 |
| 2 | Demand | 5055 | 5055 | 4244 | 4504 | 4504 | 4504 | 3924 | 4247 | 4247 | 4247 | 3275 | 3839 | 3839 |  | Demand | 2864 | 2864 | 2520 | 3266 | 3266 | 3504 | 3504 | 3504 | 3231 | 3918 | 3918 | 3918 | 3680 | 4529 | 4529 |
|  | Diff. | -147 | -317 | -263 | -307 | -329 | -395 | -360 | -427 | -467 | -487 | -383 | -437 | -451 |  | Diff. | -46 | -114 | -79 | -155 | -164 | -183 | -221 | -213 | -213 | -290 | -284 | -322 | -300 | -410 | -428 |
|  | Processed | 3870 | 3769 | 3176 | 3365 | 3343 | 3282 | 2857 | 3072 | 3061 | 3039 | 2327 | 2719 | 2697 | 1 | Processed | 2242 | 2205 | 1979 | 2537 | 2532 | 2710 | 2682 | 2672 | 2472 | 2930 | 2933 | 2909 | 2716 | 3314 | 3305 |
| 1 | Demand | 3980 | 3980 | 3342 | 3547 | 3547 | 3547 | 3090 | 3344 | 3344 | 3344 | 2579 | 3023 | 3023 |  | Demand | 2255 | 2255 | 1984 | 2571 | 2571 | 2759 | 2759 | 2759 | 2545 | 3085 | 3085 | 3085 | 2898 | 3566 | 3566 |
|  | Diff. | -110 | -211 | -166 | -182 | -204 | -265 | -233 | -272 | -283 | -305 | -252 | -304 | -326 |  | Diff. | -13 | -50 | -5 | -34 | -39 | -49 | -77 | -87 | -73 | -155 | -152 | -176 | -182 | -252 | -261 |
| Type |  | Basic | Diverge Basic Merge |  |  | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Type |  | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Interchange |  | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | I-75 | Interchange |  | I-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | I-75 | US 27 Interchange |  |  | 1-75 |
| Direction of Travel |  | > | > | $>$ | > |  | > | > | > |  | > | > | > | > | Direction of Travel |  | > | $>$ | > | > | > | > | > | > | > | > | > | > | > | > | > |

Volume (vph): XXXX Difference greater than 400vph (Based on FDOT Traffic Analysis Handbook Calibration Volume> 2,700 vph)

Figure 6-27: SPUI 2045 Speed and Density Time Plots (PM Peak)

NORTHBOUND I-75 - TIME PLOTS

|  |  |  |  | NORT | BOU | I-75 | IME | PLOTS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  |  |  | Average | Speed | mph) |  |  |  |  |  |
| 12 | 67.5 | 66.8 | 67.4 | 67.2 | 67.2 | 68.6 | 67.8 | 66.9 | 66.7 | 66.0 | 68.4 | 66.1 | 67.6 |
| 11 | 67.3 | 66.8 | 67.3 | 67.1 | 67.0 | 68.3 | 67.7 | 66.5 | 66.2 | 65.6 | 68.3 | 66.2 | 67.5 |
| 10 | 67.0 | 66.6 | 67.1 | 66.8 | 66.6 | 68.5 | 67.6 | 66.5 | 65.9 | 65.2 | 68.0 | 65.9 | 67.2 |
| 9 | 66.4 | 66.4 | 67.0 | 66.9 | 66.3 | 68.3 | 67.4 | 66.1 | 65.5 | 63.0 | 67.9 | 66.0 | 67.3 |
| 8 | 66.4 | 66.4 | 66.9 | 66.4 | 66.1 | 68.4 | 67.4 | 66.2 | 65.1 | 63.3 | 67.9 | 65.8 | 67.1 |
| 7 | 66.4 | 66.3 | 66.9 | 67.0 | 66.3 | 68.3 | 67.4 | 66.1 | 65.5 | 65.4 | 68.1 | 66.1 | 67.3 |
| 6 | 66.7 | 66.4 | 67.2 | 66.9 | 66.6 | 68.5 | 67.5 | 66.2 | 65.5 | 64.3 | 68.1 | 66.2 | 67.4 |
| 5 | 66.7 | 66.6 | 67.0 | 67.0 | 66.5 | 68.4 | 67.5 | 66.2 | 65.5 | 64.4 | 68.0 | 66.1 | 67.3 |
| 4 | 66.7 | 66.3 | 66.7 | 66.8 | 66.5 | 68.4 | 67.3 | 66.2 | 65.4 | 64.6 | 68.0 | 66.2 | 67.3 |
| 3 | 66.7 | 66.4 | 67.0 | 66.6 | 66.6 | 68.3 | 67.5 | 66.7 | 66.0 | 65.3 | 68.1 | 66.2 | 67.4 |
| 2 | 67.2 | 66.7 | 67.2 | 67.0 | 66.8 | 68.3 | 67.6 | 66.6 | 66.2 | 65.4 | 68.2 | 66.3 | 67.5 |
| 1 | 67.1 | 66.8 | 67.3 | 66.9 | 66.8 | 68.4 | 67.6 | 66.7 | 66.1 | 65.1 | 68.2 | 66.2 | 67.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,702 | 1,502 | 6,475 | 1,502 | 3,033 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | $>$ | > | > | > | > |


| Time Period | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 22.1 | 22.2 | 17.9 | 19.4 | 19.6 | 19.2 | 16.1 | 17.7 | 17.8 | 18.1 | 12.3 | 15.8 | 15.6 |
| 11 | 23.9 | 24.0 | 19.4 | 20.9 | 20.8 | 20.2 | 17.1 | 19.0 | 19.1 | 19.3 | 13.1 | 16.7 | 16.4 |
| 10 | 25.5 | 25.9 | 21.0 | 22.6 | 22.8 | 22.0 | 18.7 | 20.6 | 20.9 | 21.2 | 14.3 | 18.1 | 17.9 |
| 9 | 29.2 | 29.0 | 23.2 | 24.7 | 24.9 | 23.9 | 20.0 | 22.1 | 22.4 | 23.8 | 15.1 | 18.9 | 18.5 |
| 8 | 29.6 | 29.2 | 23.6 | 25.3 | 25.5 | 24.3 | 20.6 | 22.7 | 23.1 | 24.2 | 15.5 | 19.2 | 19.0 |
| 7 | 29.5 | 29.0 | 23.4 | 24.8 | 25.0 | 24.0 | 20.1 | 22.3 | 22.4 | 22.4 | 15.2 | 19.0 | 18.6 |
| 6 | 27.6 | 27.6 | 22.0 | 23.7 | 23.8 | 22.8 | 19.3 | 21.3 | 21.6 | 22.2 | 14.5 | 18.3 | 18.0 |
| 5 | 28.4 | 28.0 | 22.7 | 24.1 | 24.3 | 23.3 | 19.6 | 21.8 | 22.0 | 22.5 | 14.8 | 18.6 | 18.2 |
| 4 | 28.0 | 27.9 | 22.8 | 24.2 | 24.3 | 23.5 | 20.1 | 22.1 | 22.3 | 22.7 | 15.1 | 18.6 | 18.3 |
| 3 | 27.9 | 27.6 | 22.1 | 23.7 | 23.5 | 22.6 | 19.0 | 20.8 | 20.9 | 21.2 | 14.3 | 17.8 | 17.5 |
| 2 | 25.2 | 25.1 | 20.4 | 22.0 | 22.1 | 21.4 | 17.9 | 19.8 | 19.9 | 20.3 | 13.7 | 16.9 | 16.7 |
| 1 | 25.9 | 25.7 | 20.5 | 22.2 | 22.1 | 21.4 | 17.9 | 19.6 | 19.8 | 20.2 | 13.5 | 16.9 | 16.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,702 | 1,502 | 6,475 | 1,502 | 3,033 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > |


| Time | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.6 | 68.6 | 68.1 | 65.8 | 66.4 | 65.4 | 66.3 | 68.3 | 67.5 | 66.9 | 66.6 | 67.8 | 66.9 | 60.7 | 63.2 |
| 11 | 68.4 | 68.5 | 67.9 | 65.8 | 66.3 | 65.6 | 66.1 | 68.3 | 67.3 | 66.7 | 66.3 | 67.8 | 66.4 | 50.3 | 57.3 |
| 10 | 68.3 | 68.3 | 67.6 | 65.6 | 65.7 | 64.8 | 65.5 | 68.3 | 67.2 | 65.6 | 65.5 | 67.6 | 61.1 | 29.6 | 50.7 |
| 9 | 67.8 | 68.1 | 67.4 | 65.4 | 63.1 | 63.2 | 64.5 | 68.1 | 67.0 | 65.4 | 65.3 | 66.8 | 55.9 | 27.7 | 50.1 |
| 8 | 67.7 | 67.8 | 67.1 | 65.0 | 63.6 | 63.7 | 64.3 | 68.0 | 66.9 | 65.8 | 64.8 | 67.0 | 56.2 | 27.1 | 49.8 |
| 7 | 67.7 | 68.3 | 67.4 | 65.3 | 63.9 | 63.4 | 64.4 | 68.1 | 67.0 | 65.5 | 64.8 | 67.5 | 64.1 | 33.9 | 51.4 |
| 6 | 68.0 | 67.5 | 67.2 | 65.5 | 65.1 | 64.0 | 64.6 | 68.1 | 67.1 | 65.9 | 65.4 | 67.5 | 65.2 | 37.0 | 51.8 |
| 5 | 67.8 | 67.5 | 67.2 | 65.4 | 64.8 | 63.9 | 64.3 | 68.0 | 67.0 | 65.4 | 65.0 | 67.4 | 65.5 | 42.9 | 54.0 |
| 4 | 67.8 | 67.7 | 67.2 | 65.8 | 65.7 | 64.4 | 65.3 | 68.2 | 67.1 | 65.8 | 65.5 | 67.6 | 65.5 | 44.8 | 54.1 |
| 3 | 67.8 | 68.2 | 67.4 | 65.8 | 65.1 | 64.5 | 65.1 | 68.2 | 67.1 | 65.6 | 65.0 | 67.5 | 65.9 | 54.8 | 60.0 |
| 2 | 68.2 | 68.1 | 67.7 | 65.9 | 66.2 | 65.3 | 66.1 | 68.3 | 67.3 | 66.3 | 66.1 | 67.7 | 66.6 | 57.7 | 59.8 |
| 1 | 68.1 | 68.3 | 67.6 | 65.8 | 65.7 | 65.0 | 65.9 | 68.3 | 67.2 | 66.3 | 66.1 | 67.7 | 66.7 | 59.8 | 60.4 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,666 | 1,499 | 6,918 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | $>$ | > | $>$ | > | $>$ | $>$ | $>$ | $>$ | > | > | > | > | > |


| Time | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 17.3 | 17.1 | 15.7 | 20.6 | 20.5 | 22.0 | 21.6 | 21.0 | 19.8 | 22.7 | 23.0 | 22.6 | 21.7 | 29.3 | 28.3 |
| 11 | 18.8 | 18.6 | 17.0 | 22.3 | 22.1 | 23.6 | 23.4 | 22.8 | 21.4 | 24.3 | 24.8 | 24.3 | 23.5 | 40.7 | 34.8 |
| 10 | 19.9 | 19.7 | 18.1 | 23.3 | 23.3 | 25.0 | 24.6 | 23.7 | 22.5 | 26.5 | 26.7 | 25.9 | 28.9 | 73.7 | 43.2 |
| 9 | 22.9 | 22.5 | 20.5 | 25.6 | 26.7 | 28.2 | 27.4 | 26.1 | 24.6 | 28.7 | 28.9 | 28.2 | 36.5 | 82.1 | 44.6 |
| 8 | 23.4 | 23.0 | 21.1 | 26.3 | 26.9 | 28.5 | 28.0 | 26.6 | 25.0 | 28.9 | 29.6 | 28.6 | 36.9 | 83.9 | 44.9 |
| 7 | 23.7 | 23.2 | 21.3 | 26.3 | 26.9 | 28.6 | 27.9 | 26.4 | 24.8 | 28.7 | 29.2 | 27.9 | 28.1 | 65.5 | 42.9 |
| 6 | 22.1 | 21.9 | 19.8 | 25.0 | 25.1 | 27.1 | 26.7 | 25.4 | 23.8 | 27.8 | 28.3 | 27.3 | 26.8 | 60.6 | 42.1 |
| 5 | 22.7 | 22.5 | 20.6 | 25.6 | 25.8 | 27.8 | 27.5 | 26.0 | 24.3 | 28.4 | 28.7 | 27.5 | 26.9 | 52.4 | 40.0 |
| 4 | 22.4 | 22.1 | 20.0 | 24.8 | 24.9 | 26.8 | 26.2 | 25.2 | 23.7 | 27.6 | 27.8 | 27.0 | 26.6 | 50.2 | 39.8 |
| 3 | 22.5 | 22.0 | 20.0 | 24.9 | 25.1 | 26.9 | 26.4 | 25.3 | 23.7 | 27.4 | 27.8 | 26.5 | 25.8 | 37.6 | 33.4 |
| 2 | 19.9 | 19.7 | 17.9 | 22.6 | 22.6 | 24.2 | 23.7 | 23.1 | 21.7 | 25.2 | 25.5 | 24.9 | 24.0 | 33.9 | 32.7 |
| 1 | 20.9 | 20.5 | 18.7 | 23.3 | 23.3 | 25.0 | 24.6 | 23.7 | 22.3 | 25.7 | 26.0 | 25.3 | 24.3 | 32.7 | 32.4 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | -75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,666 | 1,499 | 6,918 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0 \quad>$
Using HCM 2010 thresholds for informational purposes

Figure 6-28: SPUI 2045 Volume Time Plots (PM Peak)


NORTHBOUND I-75 - TIME PLOTS

|  |  |  |  |  |  |  | -75 | IME | OTS |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  |  |  |  | Averag | Speed | ph) |  |  |  |  |  |  |
| 12 | 66.8 | 66.9 | 66.9 | 66.6 | 66.4 | 67.0 | 67.1 | 67.9 | 66.4 | 66.8 | 65.3 | 65.8 | 67.6 | 65.9 | 66.6 |
| 11 | 66.5 | 66.6 | 66.4 | 66.5 | 65.9 | 66.6 | 66.8 | 67.7 | 66.1 | 66.7 | 65.3 | 65.9 | 67.5 | 65.7 | 66.5 |
| 10 | 66.6 | 65.5 | 66.1 | 66.3 | 65.7 | 66.8 | 66.9 | 67.8 | 66.2 | 66.7 | 65.1 | 65.7 | 67.5 | 65.7 | 66.6 |
| 9 | 66.6 | 65.8 | 66.4 | 66.1 | 65.9 | 66.9 | 67.1 | 67.9 | 66.3 | 66.9 | 65.3 | 65.9 | 67.5 | 65.7 | 66.6 |
| 8 | 63.7 | 62.6 | 65.7 | 66.1 | 65.4 | 66.3 | 66.8 | 67.7 | 66.0 | 65.6 | 63.5 | 64.7 | 67.4 | 65.7 | 66.4 |
| 7 | 61.8 | 59.3 | 65.4 | 64.6 | 64.6 | 65.9 | 66.6 | 67.6 | 65.9 | 65.1 | 62.7 | 64.4 | 67.1 | 65.7 | 66.3 |
| 6 | 63.4 | 62.9 | 66.2 | 66.1 | 65.4 | 66.5 | 66.8 | 67.7 | 65.9 | 65.9 | 64.2 | 64.7 | 67.2 | 65.6 | 66.3 |
| 5 | 65.5 | 66.7 | 66.5 | 65.4 | 65.1 | 66.6 | 66.9 | 67.7 | 66.1 | 66.4 | 64.6 | 65.4 | 67.5 | 65.9 | 66.5 |
| 4 | 66.8 | 67.0 | 66.9 | 67.0 | 66.4 | 67.1 | 67.1 | 67.9 | 66.4 | 67.1 | 65.8 | 66.1 | 67.7 | 66.1 | 66.9 |
| 3 | 66.9 | 66.9 | 66.9 | 67.1 | 66.5 | 67.0 | 67.3 | 67.9 | 66.5 | 67.3 | 66.3 | 66.3 | 67.8 | 66.4 | 67.2 |
| 2 | 67.3 | 67.1 | 67.2 | 67.2 | 67.0 | 67.2 | 67.6 | 68.2 | 67.1 | 67.7 | 67.0 | 66.7 | 68.1 | 66.5 | 67.6 |
| 1 | 67.9 | 67.2 | 67.7 | 67.7 | 67.6 | 67.6 | 68.1 | 68.5 | 67.7 | 68.1 | 67.6 | 67.1 | 68.5 | 67.2 | 68.1 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 3,535 | 1,501 | 1,911 | 1,501 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time Period | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 27.5 | 27.5 | 23.3 | 25.0 | 25.1 | 24.6 | 21.8 | 22.6 | 23.1 | 23.8 | 24.6 | 24.6 | 18.4 | 22.0 | 22.0 |
| 11 | 30.2 | 29.8 | 25.3 | 26.9 | 27.1 | 26.5 | 23.3 | 23.9 | 24.4 | 24.9 | 25.5 | 25.3 | 18.9 | 22.8 | 22.6 |
| 10 | 29.4 | 29.6 | 24.9 | 26.3 | 26.6 | 25.8 | 22.7 | 23.4 | 24.0 | 24.6 | 25.3 | 25.2 | 18.9 | 22.7 | 22.4 |
| 9 | 29.4 | 29.7 | 24.4 | 26.1 | 26.1 | 25.3 | 22.3 | 23.0 | 23.5 | 24.1 | 24.9 | 24.7 | 18.6 | 22.7 | 22.4 |
| 8 | 32.1 | 34.6 | 26.3 | 27.8 | 28.2 | 27.6 | 24.3 | 25.1 | 25.7 | 26.7 | 27.7 | 27.2 | 20.2 | 24.1 | 23.9 |
| 7 | 36.3 | 38.3 | 28.0 | 30.4 | 30.1 | 29.0 | 25.2 | 25.9 | 26.6 | 28.0 | 29.3 | 28.6 | 21.0 | 25.1 | 24.9 |
| 6 | 35.0 | 35.0 | 27.4 | 29.1 | 29.3 | 28.5 | 25.0 | 25.8 | 26.4 | 27.5 | 28.3 | 28.1 | 20.7 | 24.8 | 24.5 |
| 5 | 33.0 | 31.7 | 26.9 | 28.8 | 28.9 | 27.8 | 24.3 | 24.9 | 25.4 | 26.0 | 26.7 | 26.5 | 19.6 | 23.4 | 23.2 |
| 4 | 28.4 | 27.9 | 23.7 | 25.2 | 25.4 | 24.7 | 21.8 | 22.4 | 22.9 | 23.5 | 24.0 | 23.8 | 18.0 | 21.4 | 21.1 |
| 3 | 26.9 | 26.5 | 22.2 | 23.5 | 23.6 | 23.0 | 20.2 | 21.0 | 21.4 | 21.7 | 22.1 | 22.2 | 16.6 | 19.7 | 19.4 |
| 2 | 24.3 | 23.5 | 19.7 | 20.9 | 20.8 | 20.4 | 17.7 | 18.2 | 18.3 | 18.7 | 18.8 | 18.8 | 14.1 | 17.0 | 16.7 |
| 1 | 19.0 | 18.7 | 15.6 | 16.6 | 16.5 | 16.2 | 14.1 | 14.5 | 14.6 | 15.0 | 15.1 | 15.1 | 11.3 | 13.5 | 13.2 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | I-75 | NW 49 ST Interchange |  |  |  |  | I-75 | SR 326 Interchange |  |  | I-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 3,535 | 1,501 | 1,911 | 1,501 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | ravel | > | > | > | > |  | > | > | > | > |  | > | > |  |  |

## SOUTHBOUND I-75 - TIME PLOTS

| Time |  |  |  |  |  |  | Aver | Spee | (mph) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.9 | 68.8 | 68.4 | 65.6 | 66.6 | 65.7 | 66.5 | 68.1 | 67.7 | 66.1 | 66.6 | 67.8 | 67.1 | 62.6 | 64.5 |
| 11 | 68.6 | 68.7 | 68.3 | 65.6 | 66.5 | 65.3 | 66.2 | 67.9 | 67.6 | 66.0 | 66.5 | 67.7 | 67.1 | 60.0 | 62.5 |
| 10 | 68.7 | 68.6 | 68.3 | 65.7 | 66.7 | 66.0 | 66.7 | 68.1 | 67.6 | 66.2 | 66.7 | 67.8 | 67.1 | 59.9 | 62.5 |
| 9 | 68.7 | 68.7 | 68.3 | 65.5 | 66.4 | 65.6 | 66.4 | 68.0 | 67.7 | 66.3 | 66.7 | 67.8 | 67.1 | 61.5 | 63.5 |
| 8 | 68.7 | 68.6 | 68.3 | 65.6 | 66.7 | 65.8 | 66.5 | 68.0 | 67.6 | 66.2 | 66.3 | 67.7 | 66.9 | 59.1 | 61.8 |
| 7 | 68.4 | 68.0 | 67.7 | 65.4 | 65.9 | 65.1 | 65.7 | 67.9 | 67.4 | 65.2 | 65.7 | 67.6 | 66.5 | 55.3 | 59.7 |
| 6 | 68.4 | 68.5 | 68.0 | 65.8 | 66.4 | 65.3 | 66.0 | 67.9 | 67.4 | 65.1 | 65.8 | 67.6 | 66.6 | 57.8 | 61.2 |
| 5 | 68.4 | 68.7 | 68.1 | 65.7 | 66.4 | 65.6 | 66.3 | 68.0 | 67.5 | 65.9 | 66.2 | 67.8 | 66.8 | 59.1 | 62.8 |
| 4 | 68.8 | 68.7 | 68.3 | 66.1 | 67.0 | 66.0 | 66.7 | 68.2 | 67.6 | 66.2 | 66.7 | 67.8 | 67.2 | 63.6 | 65.3 |
| 3 | 68.8 | 68.7 | 68.4 | 65.9 | 67.0 | 66.0 | 66.8 | 68.1 | 67.7 | 66.2 | 66.9 | 67.9 | 67.3 | 64.1 | 65.5 |
| 2 | 69.0 | 69.0 | 68.6 | 66.2 | 67.4 | 66.4 | 67.3 | 68.3 | 68.0 | 66.7 | 67.3 | 68.0 | 67.6 | 65.0 | 66.6 |
| 1 | 69.4 | 69.3 | 69.0 | 66.5 | 67.9 | 67.2 | 67.9 | 68.6 | 68.4 | 67.1 | 67.9 | 68.2 | 68.1 | 66.1 | 67.5 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 14.8 | 14.6 | 13.2 | 18.4 | 18.1 | 19.7 | 19.5 | 19.1 | 17.8 | 22.1 | 22.0 | 21.5 | 20.5 | 27.4 | 26.6 |
| 11 | 16.4 | 16.2 | 14.5 | 19.8 | 19.5 | 21.5 | 21.2 | 20.6 | 19.0 | 23.4 | 23.3 | 22.8 | 21.5 | 29.7 | 28.5 |
| 10 | 16.0 | 15.8 | 14.2 | 19.3 | 18.9 | 20.4 | 20.2 | 19.9 | 18.3 | 22.9 | 22.6 | 22.1 | 21.1 | 29.5 | 28.2 |
| 9 | 16.0 | 15.7 | 14.1 | 19.5 | 19.2 | 20.9 | 20.5 | 20.0 | 18.4 | 22.5 | 22.4 | 21.9 | 20.9 | 28.5 | 27.5 |
| 8 | 15.7 | 15.5 | 14.1 | 19.3 | 19.0 | 20.7 | 20.6 | 20.2 | 18.7 | 23.3 | 23.4 | 23.1 | 21.9 | 30.6 | 29.3 |
| 7 | 18.6 | 18.5 | 16.6 | 21.9 | 21.7 | 23.7 | 23.4 | 22.6 | 20.9 | 26.2 | 25.9 | 25.1 | 24.0 | 36.2 | 33.1 |
| 6 | 18.7 | 18.4 | 16.4 | 21.2 | 21.0 | 22.9 | 22.7 | 22.0 | 20.3 | 25.8 | 25.6 | 24.8 | 23.6 | 33.5 | 31.3 |
| 5 | 18.2 | 17.7 | 15.8 | 20.7 | 20.5 | 22.3 | 22.0 | 21.3 | 19.6 | 24.2 | 24.0 | 23.3 | 22.3 | 31.2 | 28.9 |
| 4 | 15.6 | 15.3 | 13.8 | 18.4 | 18.1 | 19.7 | 19.4 | 19.0 | 17.6 | 21.8 | 21.7 | 21.2 | 20.0 | 26.0 | 25.4 |
| 3 | 14.8 | 14.6 | 13.1 | 17.7 | 17.3 | 18.9 | 18.7 | 18.2 | 16.8 | 20.6 | 20.4 | 20.0 | 19.2 | 24.6 | 24.0 |
| 2 | 13.6 | 13.3 | 11.9 | 15.7 | 15.3 | 16.7 | 16.3 | 16.0 | 14.7 | 18.2 | 18.0 | 17.6 | 16.6 | 21.1 | 20.4 |
| 1 | 10.8 | 10.6 | 9.6 | 12.7 | 12.4 | 13.4 | 13.3 | 13.0 | 12.0 | 14.7 | 14.4 | 14.2 | 13.3 | 16.7 | 16.3 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
$\begin{array}{lllllll}\text { Upper: } & 10.0 & 18.0 & 26.0 & 35.0 & 45.0 & >\end{array}$
Using HCM 2010 thresholds for informational purposes


## NORTHBOUND I-75-TIME PLOTS

| Time Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 67.5 | 66.8 | 67.4 | 67.2 | 67.1 | 66.9 | 67.8 | 67.3 | 67.7 | 67.5 | 66.8 | 65.9 | 68.4 | 66.2 | 67.6 |
| 11 | 67.3 | 66.8 | 67.3 | 67.1 | 66.9 | 66.8 | 67.6 | 67.2 | 67.6 | 67.4 | 66.4 | 65.5 | 68.2 | 65.9 | 67.4 |
| 10 | 67.0 | 66.6 | 67.1 | 66.7 | 66.5 | 66.7 | 67.5 | 67.1 | 67.5 | 66.9 | 65.8 | 64.4 | 67.9 | 66.2 | 67.3 |
| 9 | 66.4 | 65.2 | 66.8 | 66.7 | 66.3 | 66.6 | 67.4 | 66.8 | 67.3 | 66.8 | 65.4 | 60.0 | 67.9 | 66.0 | 67.3 |
| 8 | 66.4 | 66.3 | 66.7 | 66.7 | 66.3 | 66.5 | 67.3 | 66.8 | 67.3 | 66.6 | 65.0 | 63.6 | 67.9 | 66.0 | 67.2 |
| 7 | 66.4 | 66.2 | 66.9 | 66.8 | 66.3 | 66.5 | 67.5 | 66.7 | 67.3 | 67.0 | 65.6 | 65.1 | 68.1 | 66.2 | 67.2 |
| 6 | 66.7 | 66.4 | 67.2 | 66.9 | 66.5 | 66.7 | 67.5 | 66.9 | 67.4 | 67.3 | 65.8 | 64.4 | 68.0 | 66.1 | 67.4 |
| 5 | 66.7 | 66.6 | 67.0 | 66.6 | 66.4 | 66.7 | 67.4 | 66.8 | 67.3 | 67.1 | 65.7 | 64.7 | 68.0 | 65.9 | 67.3 |
| 4 | 66.7 | 66.3 | 66.8 | 66.7 | 66.3 | 66.7 | 67.4 | 66.8 | 67.3 | 67.0 | 65.6 | 65.1 | 68.1 | 66.2 | 67.3 |
| 3 | 66.7 | 66.4 | 67.0 | 66.9 | 66.6 | 66.8 | 67.5 | 67.0 | 67.5 | 67.3 | 66.1 | 65.4 | 68.1 | 66.2 | 67.4 |
| 2 | 67.2 | 66.7 | 67.2 | 67.0 | 66.7 | 66.7 | 67.6 | 67.1 | 67.6 | 67.3 | 66.2 | 65.6 | 68.2 | 66.5 | 67.6 |
| 1 | 67.1 | 66.8 | 67.3 | 66.8 | 66.7 | 66.7 | 67.6 | 67.1 | 67.6 | 67.4 | 66.2 | 65.6 | 68.3 | 66.4 | 67.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  |  |  | I-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 3,535 | 1,501 | 1,911 | 1,502 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time Period |  |  |  |  |  |  | ge D | sity (v | /mi/ln |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 22.1 | 22.2 | 17.9 | 19.5 | 19.7 | 19.6 | 16.2 | 17.1 | 16.9 | 17.5 | 17.8 | 18.1 | 12.3 | 15.9 | 15.7 |
| 11 | 23.9 | 24.0 | 19.4 | 20.9 | 20.8 | 20.6 | 17.1 | 18.1 | 18.0 | 18.6 | 19.0 | 19.4 | 13.1 | 16.8 | 16.5 |
| 10 | 25.5 | 25.9 | 21.0 | 22.6 | 22.8 | 22.6 | 18.7 | 19.7 | 19.6 | 20.4 | 20.9 | 21.6 | 14.4 | 18.0 | 17.8 |
| 9 | 29.2 | 29.7 | 23.3 | 24.8 | 24.9 | 24.4 | 19.9 | 21.1 | 21.0 | 21.8 | 22.4 | 25.6 | 15.0 | 18.8 | 18.5 |
| 8 | 29.6 | 29.3 | 23.7 | 25.3 | 25.4 | 25.0 | 20.7 | 21.7 | 21.5 | 22.5 | 23.1 | 24.0 | 15.5 | 19.2 | 19.0 |
| 7 | 29.5 | 29.1 | 23.4 | 24.8 | 24.9 | 24.6 | 20.0 | 21.1 | 21.0 | 21.9 | 22.3 | 22.5 | 15.2 | 18.9 | 18.5 |
| 6 | 27.6 | 27.6 | 22.0 | 23.7 | 23.8 | 23.4 | 19.3 | 20.4 | 20.2 | 20.9 | 21.5 | 22.2 | 14.5 | 18.3 | 18.0 |
| 5 | 28.4 | 28.0 | 22.7 | 24.3 | 24.4 | 23.9 | 19.7 | 20.7 | 20.6 | 21.4 | 22.0 | 22.5 | 14.9 | 18.6 | 18.2 |
| 4 | 28.0 | 27.9 | 22.8 | 24.2 | 24.4 | 24.0 | 20.0 | 21.1 | 20.9 | 21.7 | 22.3 | 22.6 | 15.0 | 18.6 | 18.3 |
| 3 | 27.9 | 27.6 | 22.1 | 23.7 | 23.6 | 23.0 | 19.0 | 20.0 | 19.8 | 20.5 | 20.9 | 21.1 | 14.3 | 17.8 | 17.4 |
| 2 | 25.2 | 25.1 | 20.4 | 22.0 | 22.1 | 21.9 | 17.9 | 18.8 | 18.7 | 19.4 | 19.9 | 20.2 | 13.7 | 16.8 | 16.7 |
| 1 | 25.9 | 25.7 | 20.5 | 22.2 | 22.2 | 21.9 | 17.9 | 18.9 | 18.7 | 19.4 | 19.8 | 20.0 | 13.4 | 16.9 | 16.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | I-75 | NW 49 ST Interchange |  |  |  |  | I-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 3,535 | 1,501 | 1,911 | 1,502 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > | > | > |



> AVERAGE SPEED DIFFERENCE (mph)
> Diff.: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph
> Upper: $70<65 \quad<60 \quad<55 \quad<50 \quad<45$
> Lower: 65 60

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
$\begin{array}{lllllll}\text { Upper: } & 10.0 & 18.0 & 26.0 & 35.0 & 45.0 & >\end{array}$
Using HCM 2010 thresholds for informational purposes

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multicolumn{16}{|c|}{NORTHBOUND I-75-TIME PLOTS} \& \multicolumn{17}{|c|}{SOUTHBOUND I-75-TIME PLOTS} \\
\hline Time Period \& \multicolumn{15}{|c|}{Average Volume (vph)} \& Time Peri \& \multicolumn{16}{|c|}{Average Volume (vph)} \\
\hline \(12 \quad\)\begin{tabular}{c|c|}
\hline \begin{tabular}{c} 
Processed \\
Demand \\
Diff.
\end{tabular} \\
\hline
\end{tabular} \& \[
\begin{array}{|c|}
\hline 4480 \\
4417 \\
63 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4444 \\
4417 \\
27 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3628 \\
3571 \\
57 \\
\hline
\end{array}
\] \& \[
\begin{array}{c|}
\hline 3928 \\
3834 \\
94 \\
\hline
\end{array}
\] \& \[
\begin{array}{|c|}
\hline 3959 \\
3834 \\
125 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
3940 \\
3834 \\
106
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3292 \\
3162 \\
130
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3443 \\
3305 \\
138 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3426 \\
3305 \\
121 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3541 \\
3429 \\
112 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 3567 \\
3429 \\
138
\end{array}
\] \& \[
\begin{gathered}
\hline 3573 \\
3429 \\
144
\end{gathered}
\] \& \[
\begin{gathered}
2519 \\
2408 \\
111
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3162 \\
2947 \\
215 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|r|}
\hline 3179 \\
2947 \\
232 \\
\hline
\end{array}
\] \& 12 \& \[
\begin{array}{|c}
\text { Processed } \\
\text { Demand } \\
\text { Diff. }
\end{array}
\] \& \[
\begin{array}{|c|}
\hline 3563 \\
3574 \\
-11 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 3519 \\
3574 \\
-55 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3204 \\
3188 \\
16 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4103 \\
3925 \\
178 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4100 \\
3925 \\
175 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4349 \\
4153 \\
196 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 4339 \\
4153 \\
186 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4350 \\
4153 \\
197 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4033 \\
3837 \\
196
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4628 \\
4405 \\
223 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 4643 \\
4405 \\
238
\end{array}
\] \& \[
\begin{gathered}
4631 \\
4405 \\
226
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4399 \\
4154 \\
245
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5364 \\
5049 \\
315 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 5383 \\
5049 \\
334 \\
\hline
\end{array}
\] \\
\hline \(11 \quad\)\begin{tabular}{c|c|} 
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 4831 \\
4803 \\
28 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4797 \\
4803 \\
-6 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3912 \\
3883 \\
29 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 4197 \\
4170 \\
27 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4176 \\
4170 \\
6
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4117 \\
4170 \\
-53 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3465 \\
3438 \\
27 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3652 \\
3594 \\
58 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 3653 \\
3594 \\
59 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 3763 \\
3729 \\
34 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3783 \\
3729 \\
54 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3800 \\
3729 \\
71
\end{gathered}
\] \& \[
\begin{gathered}
\hline 2678 \\
2619 \\
59 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3326 \\
3204 \\
122 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3333 \\
3204 \\
129 \\
\hline
\end{array}
\] \& 11 \& \[
\begin{gathered}
\text { Processed } \\
\text { Demand } \\
\text { Diff. }
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3867 \\
3886 \\
-19 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 3819 \\
3886 \\
-67 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3457 \\
3467 \\
-10 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 4444 \\
4269 \\
175 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4436 \\
4269 \\
167 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 4693 \\
4516 \\
177 \\
\hline
\end{array}
\] \& \[
\begin{array}{|c}
\hline 4712 \\
4516 \\
196 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 4725 \\
\& 4516 \\
\& 209 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
\hline 4333 \\
4172 \\
161 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4930 \\
4791 \\
139 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 4946 \\
4791 \\
155 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4941 \\
4791 \\
150 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 4680 \\
4517 \\
163 \\
\hline
\end{array}
\] \& \[
\begin{array}{c|}
\hline 5719 \\
5491 \\
228 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5795 \\
5491 \\
304 \\
\hline
\end{gathered}
\] \\
\hline \(10 \quad\)\begin{tabular}{c|c|c} 
Processed \\
Demand \\
Diff.
\end{tabular}\(~\) \& \[
\begin{array}{|c|}
\hline 5136 \\
5061 \\
75 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5167 \\
5061 \\
106 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4236 \\
4092 \\
144 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4520 \\
4394 \\
126 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 4546 \\
4394 \\
152 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4514 \\
4394 \\
120 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3793 \\
3623 \\
170
\end{gathered}
\] \& \[
\begin{gathered}
3962 \\
3787 \\
175 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{r}
3969 \\
3787 \\
182 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4103 \\
3929 \\
174 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4130 \\
3929 \\
201 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4146 \\
3929 \\
217 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
2923 \\
2759 \\
164 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{r}
3583 \\
3377 \\
206 \\
\hline
\end{array}
\] \& \[
\begin{array}{|r|}
\hline 3601 \\
3377 \\
224 \\
\hline
\end{array}
\] \& 10 \& \[
\begin{array}{c|}
\hline \text { Processed } \\
\text { Demand } \\
\text { Diff. }
\end{array}
\] \& \[
\begin{gathered}
4077 \\
4095 \\
-18 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4030 \\
4095 \\
-65 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3674 \\
3654 \\
20 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 4569 \\
4498 \\
71 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4572 \\
4498 \\
74 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4832 \\
4759 \\
73 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 4836 \\
4759 \\
77 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4852 \\
4759 \\
93 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4497 \\
4397 \\
100
\end{gathered}
\] \& \[
\begin{gathered}
5215 \\
5048 \\
167
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 5248 \\
5048 \\
200 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5239 \\
5048 \\
191 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|r|}
\hline 4986 \\
4760 \\
226 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 6119 \\
5786 \\
333 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
6171 \\
5786 \\
385 \\
\hline
\end{gathered}
\] \\
\hline \(9 \quad\)\begin{tabular}{c|c|} 
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 5825 \\
5783 \\
42 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 5769 \\
5783 \\
-14 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4664 \\
4675 \\
-11 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4949 \\
5020 \\
-71 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4941 \\
5020 \\
-79 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& 4871 \\
\& 5020 \\
\& -149
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4027 \\
\& 4140 \\
\& -113 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
4229 \\
4327 \\
-98 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4230 \\
4327 \\
-97 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 4367 \\
\& 4490 \\
\& -123 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 4390 \\
4490 \\
-100 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4398 \\
4490 \\
-92 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3063 \\
3153 \\
-90 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3724 \\
3858 \\
-134 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3730 \\
3858 \\
-128 \\
\hline
\end{array}
\] \& 9 \& \[
\begin{gathered}
\text { Processed } \\
\text { Demand } \\
\text { Diff. }
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 4655 \\
4679 \\
-24 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4592 \\
4679 \\
-87 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4145 \\
4174 \\
-29 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|l|}
\hline 5020 \\
5139 \\
-119 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 5029 \\
5139 \\
-110 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 5324 \\
5438 \\
-114 \\
\hline
\end{array}
\] \& \[
\begin{array}{|l|}
\hline 5320 \\
5438 \\
-118 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 5332 \\
\& 5438 \\
\& -106 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
\hline 4926 \\
5023 \\
-97 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 5664 \\
5768 \\
-104 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 5654 \\
5768 \\
-114
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 5635 \\
\& 5768 \\
\& -133 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5305 \\
\& 5439 \\
\& -134 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 6285 \\
\& 6611 \\
\& -326 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 6292 \\
6611 \\
-319 \\
\hline
\end{array}
\] \\
\hline \(\left.8 \quad\)\begin{tabular}{c|c|} 
Processed \\
Demand \\
Diff.
\end{tabular} \right\rvert\, \& \[
\begin{array}{|c|}
\hline 5884 \\
5873 \\
11 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5821 \\
5873 \\
-52 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4738 \\
4749 \\
-11 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5049 \\
5099 \\
\hline-50 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 5054 \\
5099 \\
-45 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4985 \\
5099 \\
-114 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4173 \\
4204 \\
-31 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4356 \\
4395 \\
-39 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4342 \\
4395 \\
-53 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4496 \\
4560 \\
-64 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 4509 \\
4560 \\
-51 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4517 \\
4560 \\
-43 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3164 \\
3202 \\
-38 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 3803 \\
\& 3919 \\
\& -116 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|c|}
\hline 3821 \\
3919 \\
-98 \\
\hline
\end{array}
\] \& 8 \& \[
\begin{gathered}
\text { Processed } \\
\text { Demand } \\
\text { Diff. } \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4745 \\
4753 \\
-8 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4681 \\
4753 \\
-72 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4239 \\
4240 \\
-1 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 5114 \\
\& 5220 \\
\& -106 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{r}
\hline 5110 \\
5220 \\
-110 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 5419 \\
\& 5523 \\
\& -104 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|c}
\hline 5431 \\
5523 \\
-92 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5438 \\
5523 \\
-85 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4997 \\
5102 \\
-105 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 5735 \\
5858 \\
-123 \\
\hline
\end{array}
\] \& \[
\begin{array}{|c}
\hline 5739 \\
5858 \\
-119 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 5736 \\
\& 5858 \\
\& -122 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
5423 \\
5524 \\
-101 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 6306 \\
\& 6714 \\
\& -408 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|l}
\hline 6283 \\
6714 \\
-431 \\
\hline
\end{array}
\] \\
\hline 7 \begin{tabular}{c|c|}
\hline Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 5874 \\
5967 \\
-93 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 5774 \\
5967 \\
-193 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 4700 \\
\& 4825 \\
\& -125
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4967 \\
\& 5181 \\
\& -214 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4964 \\
\& 5181 \\
\& -217
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4903 \\
\& 5181 \\
\& -278 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 4055 \\
\& 4272 \\
\& -217 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 4231 \\
\& 4465 \\
\& -234 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4234 \\
\& 4465 \\
\& -231 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4391 \\
\& 4633 \\
\& -242 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l}
\hline 4387 \\
4633 \\
-246 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 4374 \\
\& 4633 \\
\& -259 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 3101 \\
\& 3253 \\
\& -152
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 3756 \\
\& 3981 \\
\& -225 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 3737 \\
3981 \\
-244 \\
\hline
\end{array}
\] \& 7 \& \[
\begin{gathered}
\text { Processed } \\
\text { Demand } \\
\text { Diff. }
\end{gathered}
\] \& \[
\begin{gathered}
4814 \\
4829 \\
-15 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4743 \\
4829 \\
-86 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4300 \\
4308 \\
-8 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 5138 \\
\& 5303 \\
\& -165 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5128 \\
\& 5303 \\
\& -175
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5417 \\
\& 5611 \\
\& -194
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 5403 \\
5611 \\
-208 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 5396 \\
\& 5611 \\
\& -215 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4943 \\
\& 5184 \\
\& -241 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5667 \\
\& 5952 \\
\& -285 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|c|}
\hline 5665 \\
5952 \\
-287 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 5618 \\
\& 5952 \\
\& -334 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5308 \\
\& 5612 \\
\& -304 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 6288 \\
\& 6822 \\
\& -534 \\
\& \hline
\end{aligned}
\] \& \begin{tabular}{|c|c|}
6290 \\
6822 \\
-532 \\
\hline 2
\end{tabular} \\
\hline \(6 \quad\)\begin{tabular}{c|c} 
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 5533 \\
5588 \\
-55 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5484 \\
5588 \\
-104
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 4435 \\
4518 \\
-83 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4751 \\
4851 \\
-100 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& 4745 \\
\& 4851 \\
\& -106
\end{aligned}
\] \& \[
\begin{aligned}
\& 4673 \\
\& 4851 \\
\& -178
\end{aligned}
\] \& \[
\begin{gathered}
3910 \\
4000 \\
-90
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4095 \\
4181 \\
-86 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4086 \\
4181 \\
-95
\end{gathered}
\] \& \[
\begin{array}{r}
\hline 4214 \\
4338 \\
-124 \\
\hline
\end{array}
\] \& \[
\begin{array}{|c}
\hline 4241 \\
4338 \\
-97 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4256 \\
4338 \\
-82 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
2962 \\
3047 \\
-85 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3630 \\
3728 \\
-98 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3646 \\
3728 \\
-82 \\
\hline
\end{array}
\] \& 6 \& \begin{tabular}{l}
Processed \\
Demand Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 4502 \\
4522 \\
-20 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4432 \\
4522 \\
-90 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3997 \\
4034 \\
-37
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 4894 \\
4966 \\
-72 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4895 \\
4966 \\
-71
\end{gathered}
\] \& \[
\begin{gathered}
5181 \\
5254 \\
-73 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 5183 \\
5254 \\
-71
\end{array}
\] \& \[
\begin{gathered}
5191 \\
5254 \\
-63 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4764 \\
4854 \\
-90 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
5517 \\
5573 \\
-56
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 5521 \\
5573 \\
-52 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5510 \\
5573 \\
-63 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
5173 \\
5255 \\
-82 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 6224 \\
\& 6388 \\
\& -164 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|c}
\hline 6230 \\
6388 \\
-158
\end{array}
\] \\
\hline 58 \begin{tabular}{c|c} 
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 5677 \\
5755 \\
-78 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 5590 \\
\& 5755 \\
\& -165 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
4557 \\
4653 \\
-96 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 4842 \\
\& 4997 \\
\& -155 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4851 \\
\& 4997 \\
\& -146 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4786 \\
\& 4997 \\
\& -211 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 3978 \\
\& 4120 \\
\& -142 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 4153 \\
\& 4307 \\
\& -154 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 4150 \\
4307 \\
-157 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4311 \\
4468 \\
-157 \\
\hline
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 4327 \\
\& 4468 \\
\& -141
\end{aligned}
\] \& \[
\begin{gathered}
\hline 4336 \\
4468 \\
-132 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3033 \\
3138 \\
-105 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3689 \\
3840 \\
-151 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3683 \\
3840 \\
-157 \\
\hline
\end{array}
\] \& 5 \& \[
\begin{array}{|c|}
\hline \text { Processed } \\
\text { Demand } \\
\text { Diff. }
\end{array}
\] \& \[
\begin{array}{|c|}
\hline 4617 \\
4657 \\
-40 \\
\hline
\end{array}
\] \& 4552
4657
-105 \& \[
\begin{gathered}
\hline 4160 \\
4155 \\
5 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 5018 \\
5115 \\
-97 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 5015 \\
\& 5115 \\
\& -100 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5312 \\
\& 5412 \\
\& -100 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
\hline 5321 \\
5412 \\
-91 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5324 \\
5412 \\
-88 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4883 \\
5000 \\
-117 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5589 \\
5740 \\
-151 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 5600 \\
5740 \\
-140 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 5573 \\
\& 5740 \\
\& -167 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5270 \\
\& 5413 \\
\& -143 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 6227 \\
\& 6580 \\
\& -353 \\
\& \hline
\end{aligned}
\] \& \begin{tabular}{|c|}
\hline 6218 \\
6580 \\
-362 \\
\hline 6
\end{tabular} \\
\hline \(4 \quad\)\begin{tabular}{c|c} 
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 5609 \\
5646 \\
-37 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5547 \\
5646 \\
-99
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4556 \\
4565 \\
-9 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4847 \\
4902 \\
-55 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4849 \\
4902 \\
-53 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4794 \\
4902 \\
-108 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4039 \\
4042 \\
-3 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4221 \\
4225 \\
-4 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4216 \\
4225 \\
-9 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 4360 \\
4384 \\
-24 \\
\hline
\end{array}
\] \& \[
\begin{array}{|c}
\hline 4381 \\
4384 \\
-3 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4387 \\
4384 \\
3 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3067 \\
3078 \\
-11 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3694 \\
3767 \\
-73 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3704 \\
3767 \\
-63 \\
\hline
\end{array}
\] \& 4 \& \[
\begin{gathered}
\text { Processed } \\
\text { Demand } \\
\text { Diff. }
\end{gathered}
\] \& \[
\begin{gathered}
4552 \\
4569 \\
-17 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4487 \\
4569 \\
-82 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4030 \\
4076 \\
-46 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|l|}
\hline 4904 \\
5018 \\
-114 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 4908 \\
\& 5018 \\
\& -110 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 5172 \\
\& 5309 \\
\& -137
\end{aligned}
\] \& \[
\begin{array}{|l}
\hline 5157 \\
5309 \\
-152 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
5155 \\
5309 \\
-154 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 4743 \\
\& 4905 \\
\& -162 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
5469 \\
5631 \\
-162 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|l|}
\hline 5466 \\
5631 \\
-165 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
5451 \\
5631 \\
-180 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5183 \\
5310 \\
-127
\end{gathered}
\] \& \[
\begin{aligned}
\& \hline 6213 \\
\& 6454 \\
\& -241 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 6204 \\
6454 \\
-250 \\
\hline
\end{array}
\] \\
\hline \(3 \mathrm{c|c|}\)\begin{tabular}{c} 
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|l|}
\hline 5595 \\
5702 \\
-107 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
5483 \\
5702 \\
-219 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
4447 \\
4610 \\
-163 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
4740 \\
4951 \\
-211 \\
\hline
\end{array}
\] \& \[
\begin{array}{|l|}
\hline 4706 \\
4951 \\
-245 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
4614 \\
4951 \\
-337 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 3851 \\
\& 4082 \\
\& -231 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 4018 \\
\& 4267 \\
\& -249 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{r}
4013 \\
4267 \\
-254 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 4136 \\
\& 4427 \\
\& -291 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 4131 \\
4427 \\
-296 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 4129 \\
\& 4427 \\
\& -298 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{r}
2919 \\
3109 \\
-190 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 3541 \\
\& 3805 \\
\& -264 \\
\& \hline
\end{aligned}
\] \& \[
\begin{gathered}
\hline 3529 \\
3805 \\
-276 \\
\hline
\end{gathered}
\] \& 3 \& \begin{tabular}{l}
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c}
4579 \\
4614 \\
-35
\end{array}
\] \& \[
\begin{array}{r}
4505 \\
4614 \\
-109 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4054 \\
4116 \\
-62 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{r}
4912 \\
5068 \\
-156 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
4901 \\
5068 \\
-167 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
5201 \\
5362 \\
-161 \\
\hline
\end{array}
\] \& \[
\begin{array}{|l}
5195 \\
5362 \\
-167 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
5197 \\
5362 \\
-165 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 4751 \\
\& 4954 \\
\& -203 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 5411 \\
\& 5688 \\
\& -277 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l|}
\hline 5406 \\
5688 \\
-282 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 5376 \\
\& 5688 \\
\& -312 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 5074 \\
\& 5363 \\
\& -289 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& 5994 \\
\& 6519 \\
\& -525 \\
\& \hline
\end{aligned}
\] \& \begin{tabular}{|c|}
5939 \\
6519 \\
-580 \\
\hline
\end{tabular} \\
\hline \begin{tabular}{l}
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 5069 \\
5085 \\
-16 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
5021 \\
5085 \\
-64
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4117 \\
4111 \\
6 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4412 \\
4415 \\
-3
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4422 \\
4415 \\
7 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4372 \\
4415 \\
-43 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3628 \\
3640 \\
-12 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3793 \\
3805 \\
-12
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 3788 \\
3805 \\
-17 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
3932 \\
3948 \\
-16 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3951 \\
3948 \\
3 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
3965 \\
3948 \\
17 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 2797 \\
2772 \\
25 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 3358 \\
3393 \\
-35 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{|c|}
\hline 3376 \\
3393 \\
-17 \\
\hline
\end{array}
\] \& 2 \& \begin{tabular}{c} 
Processed \\
\begin{tabular}{c} 
Demand \\
Diff.
\end{tabular} \\
\hline
\end{tabular} \& \begin{tabular}{|c|}
\hline 4073 \\
4115 \\
-42 \\
\hline
\end{tabular} \& \begin{tabular}{c}
4017 \\
4115 \\
-98 \\
\hline
\end{tabular} \& \[
\begin{gathered}
\hline 3640 \\
3671 \\
-31 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4463 \\
4519 \\
-56 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4461 \\
4519 \\
-58 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{c|}
\hline 4721 \\
4782 \\
-61 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
\hline 4712 \\
4782 \\
-70 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4726 \\
4782 \\
-56 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
4362 \\
4417 \\
-55
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5064 \\
5072 \\
-8 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5073 \\
5072 \\
1 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
5055 \\
5072 \\
-17
\end{gathered}
\] \& \[
\begin{gathered}
4800 \\
4782 \\
18
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5792 \\
5813 \\
-21 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5802 \\
5813 \\
-11 \\
\hline
\end{gathered}
\] \\
\hline \begin{tabular}{l}
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{array}{|c|}
\hline 5206 \\
5268 \\
-62 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 5140 \\
\& 5268 \\
\& -128
\end{aligned}
\] \& \[
\begin{array}{r}
\hline 4143 \\
4259 \\
-116 \\
\hline \hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 4452 \\
\& 4574 \\
\& -122 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{|l}
\hline 4439 \\
4574 \\
-135 \\
\hline \hline
\end{array}
\] \& \[
\begin{aligned}
\& 4373 \\
\& 4574 \\
\& -201
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 3636 \\
\& 3771 \\
\& -135 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 3802 \\
\& 3942 \\
\& -140 \\
\& \hline \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 3797 \\
\& 3942 \\
\& -145 \\
\& \hline
\end{aligned}
\] \& \[
\begin{array}{r}
\hline 3912 \\
4090 \\
-178 \\
\hline \hline
\end{array}
\] \& \[
\begin{array}{|l}
\hline 3928 \\
4090 \\
-162 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& 3927 \\
\& 4090 \\
\& -163
\end{aligned}
\] \& \[
\begin{gathered}
2751 \\
2872 \\
-121 \\
\hline
\end{gathered}
\] \& \[
\begin{array}{r}
\hline 3358 \\
3515 \\
-157 \\
\hline \hline
\end{array}
\] \& \[
\begin{array}{|l|}
\hline 3361 \\
3515 \\
-154 \\
\hline \hline
\end{array}
\] \& 1 \& \begin{tabular}{l}
Processed \\
Demand \\
Diff.
\end{tabular} \& \[
\begin{gathered}
4274 \\
4263 \\
11 \\
\hline \hline
\end{gathered}
\] \& 4206
4263
-57 \& \[
\begin{gathered}
\hline 3790 \\
3803 \\
-13 \\
\hline \hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4594 \\
4682 \\
-88 \\
\hline \hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4595 \\
4682 \\
-87 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4885 \\
4954 \\
-69 \\
\hline \hline
\end{gathered}
\] \& \[
\begin{array}{|c}
\hline 4892 \\
4954 \\
-62 \\
\hline
\end{array}
\] \& \[
\begin{gathered}
4871 \\
4954 \\
-83 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 4483 \\
4576 \\
-93 \\
\hline
\end{gathered}
\] \& \[
\begin{gathered}
\hline 5143 \\
5254 \\
-111 \\
\hline \hline
\end{gathered}
\] \& \[
\begin{array}{|l|}
\hline 5148 \\
5254 \\
-106 \\
\hline
\end{array}
\] \& \[
\begin{array}{r}
\hline 5141 \\
5254 \\
-113 \\
\hline
\end{array}
\] \& \[
\begin{aligned}
\& \hline 4855 \\
\& 4955 \\
\& -100 \\
\& \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5809 \\
\& 6022 \\
\& -213 \\
\& \hline \hline
\end{aligned}
\] \& \[
\begin{aligned}
\& \hline 5793 \\
\& 6022 \\
\& -229 \\
\& \hline
\end{aligned}
\] \\
\hline Type \& Basic \& \multicolumn{3}{|l|}{\multirow[t]{2}{*}{Diverge Basic Merge US 27 Interchange}} \& Basic \& \multicolumn{5}{|l|}{\multirow[t]{2}{*}{Diverge Basic Merge Basic Merge NW 49 ST Interchange}} \& Basic \& \multicolumn{3}{|l|}{\multirow[t]{2}{*}{\[
\begin{array}{|c|c|}
\hline \text { c } \& \text { Diverge Basic Merge } \\
\hline \text { SR } 326 \text { Interchange }
\end{array}
\]}} \& \multirow[t]{3}{*}{\[
\begin{array}{|c|}
\hline \text { Basic } \\
\hline 1-75 \\
\hline> \\
\hline
\end{array}
\]} \& \multicolumn{2}{|l|}{Type} \& ic \& \multicolumn{5}{|l|}{\multirow[t]{2}{*}{\begin{tabular}{|c|} 
Diverge Basic Merge Basic Merge \\
SR 326 Interchange
\end{tabular}}} \& Basic \& \multicolumn{3}{|l|}{\multirow[t]{2}{*}{Diverge Basic Merge NW 49 ST Interchange}} \& \multirow[t]{2}{*}{\[
\begin{array}{|l|l}
\text { Basic } \\
\hline \& 1-75
\end{array}
\]} \& Diverge B \& \multicolumn{2}{|l|}{Basic Merge} \& Basic \\
\hline Interchange \& I-75 \& \& \& \& 1-75 \& \& \& \& \& \& 1-75 \& \& \& \& \& \multicolumn{2}{|l|}{\multirow[t]{2}{*}{Interchange Direction of Travel}} \& 1-75 \& \& \& \& \& \& \multirow[t]{2}{*}{\[
1-75
\]} \& \& \& \& \& \multicolumn{3}{|l|}{US 27 Interchange} \& 75 \\
\hline Direction of Travel \& > \& > \& > \& > \& > \& > \& > \& > \& > \& > \& > \& > \& > \& > \& \& \& \& > \& \multicolumn{5}{|c|}{SR 326 Interchange} \& \& NW 49 S

$>$ \& \multicolumn{2}{|l|}{ST Interchange} \& > \& > \& > \& > \& > <br>
\hline
\end{tabular}

NORTHBOUND I-75 - TIME PLOTS

| Time Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 66.8 | 66.9 | 66.9 | 66.7 | 66.4 | 67.7 | 66.7 | 68.6 | 66.9 | 66.5 | 65.3 | 65.9 | 67.7 | 66.1 | 66.7 |
| 11 | 66.5 | 66.6 | 66.4 | 66.6 | 66.0 | 67.6 | 66.5 | 68.5 | 66.9 | 66.3 | 65.2 | 65.7 | 67.5 | 66.0 | 66.7 |
| 10 | 65.5 | 64.9 | 65.7 | 66.5 | 65.9 | 67.6 | 66.5 | 68.5 | 66.7 | 66.2 | 64.9 | 65.7 | 67.5 | 65.9 | 66.6 |
| 9 | 64.1 | 63.3 | 65.9 | 66.5 | 66.1 | 67.5 | 66.6 | 68.6 | 66.9 | 65.5 | 64.7 | 65.8 | 67.6 | 65.6 | 66.7 |
| 8 | 62.2 | 58.3 | 65.1 | 66.3 | 65.5 | 67.3 | 66.3 | 68.5 | 66.8 | 66.1 | 64.5 | 65.3 | 67.5 | 65.6 | 66.5 |
| 7 | 62.4 | 59.2 | 65.6 | 65.6 | 65.2 | 67.0 | 65.7 | 68.4 | 66.7 | 64.8 | 62.7 | 62.8 | 67.2 | 65.5 | 66.3 |
| 6 | 63.7 | 65.9 | 66.6 | 66.4 | 65.4 | 67.0 | 65.6 | 68.4 | 66.7 | 64.5 | 63.1 | 63.6 | 67.3 | 65.3 | 66.3 |
| 5 | 65.5 | 66.5 | 66.5 | 66.5 | 65.5 | 67.5 | 66.3 | 68.5 | 66.8 | 65.0 | 64.0 | 65.5 | 67.5 | 65.8 | 66.6 |
| 4 | 66.8 | 67.0 | 66.9 | 67.1 | 66.4 | 67.7 | 66.6 | 68.6 | 66.9 | 66.7 | 65.7 | 66.0 | 67.7 | 66.1 | 66.8 |
| 3 | 66.9 | 66.9 | 66.9 | 67.1 | 66.7 | 67.8 | 66.9 | 68.6 | 67.1 | 66.9 | 66.1 | 66.2 | 67.7 | 66.5 | 67.2 |
| 2 | 67.3 | 67.1 | 67.2 | 67.4 | 67.1 | 67.9 | 67.2 | 68.7 | 67.5 | 67.2 | 66.8 | 66.6 | 68.0 | 66.6 | 67.6 |
| 1 | 67.9 | 67.2 | 67.7 | 67.8 | 67.6 | 68.2 | 67.8 | 69.0 | 68.0 | 67.8 | 67.6 | 67.0 | 68.5 | 67.2 | 68.1 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 | Interch | nge | I-75 |  | NW 4 | ST Interc | ange |  | I-75 | SR 32 | Interc | nge | I-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 2,750 | 1,501 | 2,690 | 1,502 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time Period | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 27.5 | 27.5 | 23.3 | 25.0 | 25.1 | 24.3 | 23.8 | 23.2 | 22.0 | 23.9 | 24.6 | 24.6 | 18.3 | 21.9 | 21.9 |
| 11 | 30.2 | 29.8 | 25.3 | 26.9 | 27.1 | 26.0 | 25.4 | 24.5 | 23.1 | 25.1 | 25.6 | 25.5 | 19.0 | 22.7 | 22.5 |
| 10 | 30.2 | 30.4 | 25.3 | 26.6 | 26.8 | 25.7 | 25.1 | 24.4 | 23.1 | 25.1 | 25.6 | 25.3 | 19.0 | 22.8 | 22.6 |
| 9 | 31.7 | 32.9 | 24.8 | 26.0 | 26.2 | 25.3 | 24.8 | 23.9 | 22.5 | 24.7 | 25.1 | 24.7 | 18.6 | 22.6 | 22.3 |
| 8 | 33.7 | 37.9 | 26.1 | 27.3 | 27.6 | 26.6 | 26.0 | 25.1 | 23.9 | 26.0 | 26.9 | 26.6 | 19.9 | 23.9 | 23.7 |
| 7 | 35.7 | 39.0 | 27.8 | 29.4 | 29.6 | 28.5 | 27.9 | 26.8 | 25.3 | 28.1 | 29.3 | 30.6 | 21.1 | 25.1 | 24.9 |
| 6 | 34.9 | 33.1 | 27.4 | 29.2 | 29.6 | 28.5 | 27.9 | 26.6 | 25.1 | 28.2 | 28.9 | 28.9 | 20.7 | 25.1 | 24.7 |
| 5 | 33.0 | 31.7 | 26.9 | 28.4 | 28.6 | 27.4 | 26.7 | 25.6 | 24.1 | 26.7 | 27.0 | 26.4 | 19.7 | 23.4 | 23.1 |
| 4 | 28.4 | 27.9 | 23.7 | 25.2 | 25.4 | 24.5 | 23.8 | 23.0 | 21.8 | 23.6 | 24.0 | 23.9 | 18.0 | 21.4 | 21.2 |
| 3 | 26.9 | 26.5 | 22.2 | 23.5 | 23.5 | 22.8 | 22.1 | 21.6 | 20.3 | 21.8 | 22.2 | 22.2 | 16.6 | 19.6 | 19.4 |
| 2 | 24.3 | 23.5 | 19.7 | 20.8 | 20.7 | 20.2 | 19.4 | 18.8 | 17.5 | 18.8 | 18.8 | 18.8 | 14.2 | 17.0 | 16.7 |
| 1 | 19.0 | 18.7 | 15.6 | 16.5 | 16.5 | 16.0 | 15.4 | 14.9 | 13.9 | 15.0 | 15.1 | 15.1 | 11.3 | 13.5 | 13.2 |
| Type | Basic | Diverge |  | Merge | Basic | Diverge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  |  |  | I-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 2,750 | 1,501 | 2,690 | 1,502 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | ravel |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

SOUTHBOUND I-75 - TIME PLOTS

| Time Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.6 | 68.7 | 68.3 | 65.7 | 66.6 | 65.6 | 66.3 | 68.0 | 67.7 | 66.1 | 66.7 | 67.8 | 67.2 | 62.1 | 64.4 |
| 11 | 68.7 | 68.6 | 68.3 | 65.8 | 66.7 | 65.8 | 66.6 | 68.1 | 67.6 | 66.2 | 66.5 | 67.7 | 67.1 | 62.0 | 64.1 |
| 10 | 68.7 | 68.7 | 68.3 | 65.4 | 66.4 | 65.6 | 66.4 | 68.2 | 67.7 | 66.0 | 66.5 | 67.8 | 67.0 | 60.2 | 62.9 |
| 9 | 68.7 | 68.6 | 68.3 | 65.6 | 66.6 | 65.6 | 66.4 | 68.0 | 67.7 | 66.2 | 66.7 | 67.8 | 67.1 | 61.3 | 64.1 |
| 8 | 68.4 | 68.0 | 67.7 | 65.7 | 66.2 | 65.3 | 66.3 | 67.9 | 67.6 | 65.9 | 66.3 | 67.6 | 66.8 | 59.2 | 61.5 |
| 7 | 68.4 | 68.5 | 68.0 | 65.7 | 66.3 | 65.1 | 65.9 | 67.8 | 67.4 | 64.9 | 65.3 | 67.5 | 66.7 | 54.4 | 58.4 |
| 6 | 68.4 | 68.7 | 68.1 | 65.9 | 66.3 | 65.3 | 65.9 | 67.9 | 67.4 | 65.5 | 66.1 | 67.7 | 66.8 | 58.0 | 60.8 |
| 5 | 68.8 | 68.7 | 68.3 | 65.9 | 66.3 | 65.3 | 66.1 | 68.0 | 67.5 | 65.7 | 66.4 | 67.8 | 67.0 | 60.0 | 62.7 |
| 4 | 68.8 | 68.7 | 68.4 | 66.0 | 67.0 | 66.2 | 66.9 | 68.2 | 67.7 | 66.1 | 66.7 | 67.8 | 67.2 | 63.7 | 65.4 |
| 3 | 69.0 | 69.0 | 68.4 | 65.9 | 67.1 | 66.1 | 66.8 | 68.1 | 67.8 | 66.4 | 67.0 | 67.9 | 67.3 | 64.5 | 65.8 |
| 2 | 69.4 | 69.0 | 68.6 | 66.2 | 67.4 | 66.4 | 67.3 | 68.4 | 68.0 | 66.7 | 67.4 | 68.0 | 67.6 | 64.7 | 66.4 |
| 1 | 69.4 | 69.3 | 69.0 | 66.5 | 67.8 | 67.2 | 68.0 | 68.6 | 68.4 | 67.1 | 67.8 | 68.2 | 68.1 | 66.2 | 67.4 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 |  | SR 32 | Interch | ange |  | l-75 | NW 49 | T Inte | hange | I-75 | US 27 | Interch | nge | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


|  | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 16.4 | 16.2 | 14.5 | 19.5 | 19.3 | 21.2 | 20.9 | 20.4 | 17.7 | 22.0 | 21.9 | 21.6 | 20.4 | 27.5 | 26.5 |
| 11 | 16.0 | 15.8 | 14.2 | 19.1 | 18.8 | 20.4 | 20.2 | 20.0 | 18.8 | 23.2 | 23.0 | 22.6 | 21.3 | 28.5 | 27.5 |
| 10 | 16.0 | 15.7 | 14.1 | 19.4 | 19.2 | 20.8 | 20.5 | 19.7 | 18.2 | 22.8 | 22.7 | 22.2 | 21.2 | 29.4 | 28.1 |
| 9 | 15.7 | 15.5 | 14.1 | 19.5 | 19.2 | 20.8 | 20.5 | 20.0 | 18.4 | 22.6 | 22.4 | 21.9 | 21.0 | 28.7 | 27.3 |
| 8 | 18.6 | 18.5 | 16.6 | 21.8 | 21.6 | 22.1 | 20.7 | 20.3 | 18.7 | 23.3 | 23.3 | 23.0 | 21.8 | 30.5 | 29.7 |
| 7 | 18.7 | 18.4 | 16.4 | 21.4 | 21.2 | 23.6 | 23.3 | 22.6 | 20.9 | 26.4 | 26.2 | 25.2 | 24.0 | 36.5 | 33.7 |
| 6 | 18.2 | 17.7 | 15.8 | 20.6 | 21.2 | 23.2 | 23.0 | 22.3 | 20.6 | 25.8 | 25.6 | 25.0 | 23.7 | 33.4 | 31.9 |
| 5 | 15.6 | 15.3 | 13.8 | 19.0 | 20.5 | 22.3 | 22.0 | 21.3 | 19.6 | 24.3 | 24.0 | 23.3 | 22.3 | 30.6 | 28.9 |
| 4 | 14.8 | 14.6 | 13.1 | 18.5 | 18.2 | 19.7 | 19.4 | 19.1 | 17.6 | 21.9 | 21.7 | 21.2 | 20.1 | 26.1 | 25.4 |
| 3 | 13.6 | 13.3 | 13.1 | 17.7 | 17.3 | 18.8 | 18.6 | 18.2 | 16.7 | 20.6 | 20.4 | 20.0 | 19.1 | 24.4 | 23.9 |
| 2 | 10.8 | 13.3 | 11.9 | 15.7 | 15.3 | 16.7 | 16.4 | 16.0 | 14.7 | 18.2 | 17.9 | 17.6 | 16.6 | 21.3 | 20.6 |
| 1 | 10.8 | 10.6 | 9.6 | 12.7 | 12.5 | 13.4 | 13.2 | 13.0 | 12.0 | 14.7 | 14.5 | 14.2 | 13.3 | 16.7 | 16.3 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > |  |

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: $\operatorname{LOS} A$ LOSB $\operatorname{LOS} C$ LOSD LOSE LOSF
Lower: $\begin{array}{lllllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0>$
Using HCM 2010 thresholds for informational purposes


NORTHBOUND I-75 - TIME PLOTS

|  |  |  |  |  | NOR | BOU | D I-75 | TIME | LOTS |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  |  |  |  | Averag | Speed ( | ph) |  |  |  |  |  |  |
| 12 | 67.5 | 66.8 | 67.4 | 67.3 | 67.1 | 67.7 | 67.3 | 68.7 | 67.7 | 67.2 | 66.7 | 65.7 | 68.3 | 66.1 | 67.7 |
| 11 | 67.3 | 66.8 | 67.3 | 67.2 | 67.0 | 67.7 | 67.2 | 68.6 | 67.5 | 67.1 | 66.4 | 65.4 | 68.2 | 66.1 | 67.5 |
| 10 | 67.0 | 66.6 | 67.1 | 67.0 | 66.5 | 67.5 | 66.9 | 66.9 | 66.8 | 66.3 | 65.8 | 65.1 | 68.1 | 66.0 | 67.2 |
| 9 | 66.4 | 66.3 | 67.0 | 66.6 | 66.2 | 67.5 | 66.7 | 66.6 | 66.9 | 65.9 | 65.2 | 61.5 | 67.9 | 66.2 | 67.3 |
| 8 | 66.4 | 66.4 | 66.9 | 66.8 | 66.3 | 67.4 | 66.7 | 68.4 | 67.2 | 65.8 | 64.9 | 62.6 | 67.8 | 66.0 | 67.2 |
| 7 | 66.4 | 66.3 | 66.9 | 66.9 | 66.4 | 67.5 | 66.9 | 68.5 | 67.2 | 66.2 | 65.1 | 64.8 | 68.1 | 66.1 | 67.3 |
| 6 | 66.7 | 66.4 | 67.2 | 67.0 | 66.6 | 67.5 | 66.8 | 68.6 | 67.3 | 66.5 | 65.7 | 64.2 | 68.1 | 66.2 | 67.4 |
| 5 | 66.7 | 66.6 | 67.0 | 66.9 | 66.5 | 67.5 | 66.9 | 68.6 | 67.2 | 66.4 | 65.5 | 64.6 | 68.0 | 66.0 | 67.4 |
| 4 | 66.7 | 66.4 | 66.7 | 66.7 | 66.3 | 67.5 | 66.9 | 68.6 | 67.2 | 66.3 | 65.8 | 64.9 | 68.0 | 66.1 | 67.3 |
| 3 | 66.7 | 66.4 | 67.0 | 66.8 | 66.6 | 67.6 | 67.0 | 68.6 | 67.3 | 66.7 | 66.2 | 65.5 | 68.1 | 66.2 | 67.4 |
| 2 | 67.2 | 66.7 | 67.2 | 67.2 | 66.8 | 67.5 | 66.9 | 68.6 | 67.4 | 66.9 | 66.3 | 65.5 | 68.2 | 66.4 | 67.7 |
| 1 | 67.1 | 66.8 | 67.3 | 67.0 | 66.8 | 67.6 | 67.1 | 68.6 | 67.4 | 67.0 | 66.3 | 65.6 | 68.2 | 66.4 | 67.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | I-75 | NW 49 ST Interchange |  |  |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 2,750 | 1,501 | 2,690 | 1,502 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > | > | $>$ |


| Time Period | Average Density (veh/mi/n) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 22.1 | 22.2 | 17.9 | 19.4 | 19.6 | 19.4 | 18.4 | 17.9 | 16.1 | 17.5 | 17.8 | 18.2 | 12.3 | 15.9 | 15.6 |
| 11 | 23.9 | 24.0 | 19.4 | 20.9 | 20.9 | 20.3 | 19.4 | 19.1 | 17.3 | 18.8 | 19.0 | 19.5 | 13.1 | 16.8 | 16.5 |
| 10 | 25.5 | 25.9 | 21.0 | 22.5 | 22.7 | 22.2 | 21.2 | 22.4 | 19.0 | 20.6 | 20.9 | 21.3 | 14.3 | 18.2 | 17.9 |
| 9 | 29.2 | 29.0 | 23.2 | 24.8 | 24.9 | 24.1 | 22.8 | 23.9 | 20.1 | 22.1 | 22.5 | 24.5 | 15.0 | 18.7 | 18.4 |
| 8 | 29.6 | 29.2 | 23.6 | 25.2 | 25.4 | 24.6 | 23.5 | 22.8 | 20.7 | 23.0 | 23.3 | 24.6 | 15.5 | 19.2 | 19.0 |
| 7 | 29.5 | 29.0 | 23.4 | 24.8 | 25.0 | 24.2 | 22.9 | 22.1 | 20.0 | 22.2 | 22.5 | 22.6 | 15.2 | 19.0 | 18.7 |
| 6 | 27.6 | 27.6 | 22.0 | 23.7 | 23.7 | 23.1 | 22.0 | 21.4 | 19.3 | 21.1 | 21.5 | 22.2 | 14.5 | 18.3 | 18.0 |
| 5 | 28.4 | 28.0 | 22.7 | 24.1 | 24.3 | 23.6 | 22.4 | 21.8 | 19.8 | 21.7 | 22.0 | 22.4 | 14.9 | 18.6 | 18.2 |
| 4 | 28.0 | 27.9 | 22.8 | 24.2 | 24.4 | 23.6 | 22.5 | 21.9 | 20.0 | 21.9 | 22.2 | 22.6 | 15.0 | 18.7 | 18.4 |
| 3 | 27.9 | 27.6 | 22.1 | 23.7 | 23.6 | 22.8 | 21.5 | 20.9 | 19.0 | 20.7 | 20.8 | 21.1 | 14.3 | 17.9 | 17.4 |
| 2 | 25.2 | 25.1 | 20.4 | 21.9 | 22.1 | 21.6 | 20.4 | 19.8 | 17.9 | 19.6 | 19.9 | 20.2 | 13.7 | 16.9 | 16.7 |
| 1 | 25.9 | 25.7 | 20.5 | 22.2 | 22.1 | 21.5 | 20.4 | 19.9 | 18.0 | 19.5 | 19.8 | 20.0 | 13.4 | 16.9 | 16.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 3,345 | 1,502 | 2,750 | 1,501 | 2,690 | 1,502 | 3,019 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | $>$ | > | > | > | > | > | > | > | > | > | > | > | > |

## SOUTHBOUND I-75 - TIME PLOTS

| Tim | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 68.4 | 68.5 | 67.9 | 65.5 | 66.0 | 65.0 | 65.7 | 67.9 | 67.5 | 66.7 | 66.5 | 67.6 | 66.7 | 59.4 | 62.8 |
| 11 | 68.3 | 68.3 | 67.6 | 65.5 | 65.3 | 64.8 | 65.5 | 67.8 | 67.4 | 66.2 | 66.1 | 67.6 | 66.2 | 49.1 | 57.3 |
| 10 | 67.8 | 68.1 | 67.4 | 65.7 | 65.1 | 63.5 | 63.8 | 67.7 | 67.2 | 65.7 | 65.7 | 67.7 | 61.4 | 33.8 | 51.4 |
| 9 | 67.7 | 67.8 | 67.1 | 65.5 | 65.0 | 63.6 | 63.8 | 67.4 | 67.0 | 64.1 | 63.9 | 67.0 | 55.9 | 29.4 | 50.9 |
| 8 | 67.7 | 68.3 | 67.4 | 65.4 | 64.2 | 63.7 | 64.1 | 67.4 | 66.9 | 65.3 | 64.7 | 67.5 | 55.7 | 28.1 | 50.2 |
| 7 | 68.0 | 67.5 | 67.2 | 65.5 | 65.4 | 63.7 | 64.0 | 67.5 | 67.0 | 65.9 | 65.4 | 66.9 | 61.5 | 31.2 | 50.9 |
| 6 | 67.8 | 67.5 | 67.2 | 65.6 | 65.4 | 64.4 | 64.7 | 67.6 | 67.0 | 65.4 | 65.0 | 67.5 | 63.7 | 32.3 | 51.1 |
| 5 | 67.8 | 67.7 | 67.2 | 65.4 | 64.6 | 64.1 | 64.4 | 67.6 | 67.1 | 65.8 | 65.3 | 67.5 | 64.2 | 36.2 | 52.8 |
| 4 | 67.8 | 68.2 | 67.4 | 65.3 | 65.1 | 64.2 | 64.7 | 67.7 | 67.2 | 65.7 | 65.0 | 67.6 | 65.5 | 41.9 | 53.6 |
| 3 | 68.2 | 68.1 | 67.4 | 65.5 | 64.3 | 64.0 | 64.6 | 67.7 | 67.1 | 66.0 | 65.4 | 67.6 | 65.9 | 53.2 | 59.4 |
| 2 | 68.1 | 68.1 | 67.7 | 65.9 | 66.1 | 65.3 | 65.6 | 67.7 | 67.3 | 65.9 | 65.9 | 67.6 | 66.6 | 56.3 | 60.3 |
| 1 | 68.1 | 68.3 | 67.6 | 66.0 | 66.1 | 65.0 | 65.5 | 67.5 | 67.2 | 66.3 | 66.0 | 67.7 | 66.8 | 59.4 | 61.8 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time Period | Average Density (veh/mi/nn) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 18.8 | 18.6 | 17.0 | 22.6 | 22.4 | 24.0 | 23.8 | 23.1 | 19.8 | 23.0 | 23.1 | 22.7 | 21.8 | 30.2 | 28.4 |
| 11 | 19.9 | 19.7 | 18.1 | 23.4 | 23.5 | 25.0 | 24.8 | 23.7 | 21.4 | 24.8 | 25.0 | 24.4 | 23.6 | 41.7 | 35.2 |
| 10 | 22.9 | 22.5 | 20.5 | 25.5 | 25.8 | 28.1 | 28.0 | 24.1 | 22.4 | 26.6 | 26.6 | 25.8 | 28.5 | 67.9 | 42.4 |
| 9 | 23.4 | 23.0 | 21.1 | 26.1 | 26.2 | 28.6 | 28.0 | 26.5 | 24.5 | 29.6 | 29.7 | 28.2 | 36.4 | 79.8 | 43.6 |
| 8 | 23.7 | 23.2 | 21.3 | 26.4 | 26.9 | 28.6 | 28.3 | 26.9 | 25.0 | 29.5 | 29.7 | 28.4 | 37.5 | 82.6 | 44.3 |
| 7 | 22.1 | 21.9 | 19.8 | 25.0 | 25.0 | 28.6 | 28.4 | 26.8 | 24.8 | 28.9 | 29.1 | 28.3 | 29.9 | 71.7 | 43.6 |
| 6 | 22.7 | 22.5 | 20.6 | 25.5 | 25.0 | 26.9 | 26.8 | 25.7 | 23.8 | 28.2 | 28.4 | 27.2 | 27.6 | 69.9 | 43.1 |
| 5 | 22.4 | 22.1 | 20.0 | 25.2 | 25.9 | 27.7 | 27.5 | 26.1 | 24.2 | 28.3 | 28.6 | 27.5 | 27.8 | 63.9 | 40.8 |
| 4 | 22.5 | 22.0 | 20.0 | 25.1 | 25.2 | 27.0 | 26.8 | 25.5 | 23.6 | 27.9 | 28.2 | 27.0 | 26.5 | 54.1 | 40.2 |
| 3 | 19.9 | 19.7 | 20.0 | 25.0 | 25.4 | 27.1 | 26.7 | 25.5 | 23.6 | 27.4 | 27.6 | 26.6 | 25.7 | 39.4 | 33.9 |
| 2 | 20.9 | 19.7 | 17.9 | 22.7 | 22.7 | 24.4 | 24.1 | 23.4 | 21.7 | 25.6 | 25.7 | 25.0 | 24.1 | 35.3 | 32.6 |
| 1 | 20.9 | 20.5 | 18.7 | 23.2 | 23.2 | 25.0 | 24.9 | 24.1 | 22.2 | 25.9 | 26.0 | 25.2 | 24.2 | 32.7 | 31.3 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > | > | > |

AVERAGE SPEED DIFFERENCE (mph)
Diff.: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph Upper: $70<65 \quad<60 \quad<55 \quad<50<45$ $\begin{array}{lllllll}\text { Lower: } & 65 & 60 & 55 & 50 & 45 & 0\end{array}$ (Posted Speed -Avg. Speed)

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{llllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
$\begin{array}{lllllll}\text { Upper: } & 10.0 & 18.0 & 26.0 & 35.0 & 45.0 & >\end{array}$
Using HCM 2010 thresholds for informational purposes


Figure 6-37: DDI 2045 Speed and Density Time Plots (AM Peak)

| NORTHBOUND I-75-TIME PLOTS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 66.8 | 66.9 | 66.9 | 66.4 | 65.4 | 64.8 | 67.1 | 65.5 | 64.4 | 65.0 | 67.5 | 65.9 | 66.6 |
| 11 | 66.4 | 66.6 | 66.4 | 65.9 | 64.1 | 64.0 | 66.6 | 64.0 | 62.6 | 64.5 | 67.4 | 65.8 | 66.5 |
| 10 | 64.9 | 63.9 | 65.7 | 65.5 | 64.2 | 63.7 | 66.8 | 64.0 | 63.4 | 64.9 | 67.5 | 65.6 | 66.6 |
| 9 | 64.0 | 62.1 | 65.8 | 66.0 | 64.7 | 63.9 | 67.0 | 65.3 | 64.1 | 65.3 | 67.6 | 65.7 | 66.7 |
| 8 | 61.5 | 58.4 | 65.4 | 65.9 | 64.9 | 64.3 | 66.7 | 62.6 | 61.0 | 64.0 | 67.2 | 65.6 | 66.5 |
| 7 | 61.7 | 58.8 | 65.2 | 65.7 | 63.3 | 63.5 | 66.6 | 64.6 | 63.0 | 64.2 | 67.4 | 65.8 | 66.3 |
| 6 | 63.7 | 64.8 | 66.5 | 66.3 | 64.4 | 63.3 | 66.6 | 63.8 | 61.0 | 63.6 | 67.3 | 65.3 | 66.3 |
| 5 | 65.5 | 66.7 | 66.5 | 65.6 | 64.1 | 63.5 | 66.5 | 64.3 | 63.0 | 64.8 | 67.5 | 65.9 | 66.7 |
| 4 | 66.8 | 67.0 | 66.9 | 66.8 | 65.5 | 64.7 | 67.0 | 65.7 | 65.1 | 65.5 | 67.6 | 66.1 | 66.9 |
| 3 | 66.9 | 66.9 | 66.9 | 66.8 | 66.1 | 64.9 | 67.2 | 65.8 | 65.3 | 65.6 | 67.8 | 66.6 | 67.2 |
| 2 | 67.3 | 67.1 | 67.2 | 67.3 | 66.7 | 65.0 | 67.6 | 66.3 | 66.4 | 66.4 | 68.2 | 66.5 | 67.6 |
| 1 | 67.9 | 67.2 | 67.7 | 67.6 | 67.3 | 66.0 | 68.1 | 66.8 | 67.2 | 66.9 | 68.5 | 67.2 | 68.0 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 | Interch |  | 1-75 | NW 49 | T Inter | hange | 1-75 | SR 32 | Interc | nge | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | $>$ | > | > | > | > | > | > |


|  |  |  |  |  |  | BO | D- | TIM | PLO |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  |  |  |  | Aver | e Speed | (mph) |  |  |  |  |  |  |
| 12 | 68.9 | 68.8 | 68.4 | 65.7 | 66.9 | 66.0 | 66.7 | 68.1 | 67.7 | 64.6 | 66.5 | 67.8 | 67.1 | 61.7 | 64.2 |
| 11 | 68.6 | 68.7 | 68.3 | 65.6 | 66.5 | 65.3 | 66.2 | 68.0 | 67.6 | 64.7 | 66.3 | 67.7 | 67.1 | 61.0 | 63.6 |
| 10 | 68.7 | 68.6 | 68.3 | 65.7 | 66.8 | 65.9 | 66.8 | 68.1 | 67.7 | 64.8 | 66.6 | 67.8 | 67.1 | 61.4 | 63.5 |
| 9 | 68.7 | 68.7 | 68.3 | 65.6 | 66.7 | 65.7 | 66.5 | 68.0 | 67.7 | 65.0 | 66.7 | 67.8 | 67.2 | 61.4 | 64.0 |
| 8 | 68.7 | 68.6 | 68.3 | 65.7 | 66.7 | 65.8 | 66.4 | 68.0 | 67.6 | 64.8 | 66.3 | 67.6 | 67.0 | 60.1 | 62.4 |
| 7 | 68.4 | 68.0 | 67.7 | 65.6 | 66.2 | 65.0 | 65.8 | 67.9 | 67.4 | 63.7 | 65.4 | 67.5 | 66.7 | 56.5 | 60.4 |
| 6 | 68.4 | 68.5 | 68.0 | 65.8 | 66.3 | 65.3 | 65.9 | 67.9 | 67.4 | 64.2 | 65.7 | 67.2 | 66.7 | 57.1 | 59.8 |
| 5 | 68.4 | 68.7 | 68.1 | 65.9 | 66.5 | 65.4 | 66.2 | 68.0 | 67.5 | 64.4 | 66.3 | 67.8 | 66.9 | 61.2 | 63.5 |
| 4 | 68.8 | 68.7 | 68.3 | 66.0 | 67.1 | 66.2 | 66.9 | 68.2 | 67.7 | 65.1 | 66.8 | 67.8 | 67.2 | 63.2 | 65.0 |
| 3 | 68.8 | 68.7 | 68.4 | 66.0 | 67.0 | 66.1 | 66.9 | 68.1 | 67.8 | 65.1 | 66.8 | 67.9 | 67.3 | 63.5 | 65.4 |
| 2 | 69.0 | 69.0 | 68.6 | 66.2 | 67.3 | 66.6 | 67.3 | 68.4 | 68.0 | 65.4 | 67.2 | 68.1 | 67.6 | 64.9 | 66.4 |
| 1 | 69.4 | 69.3 | 69.0 | 66.5 | 67.9 | 67.2 | 67.9 | 68.6 | 68.4 | 66.0 | 67.9 | 68.3 | 68.1 | 66.2 | 67.5 |
| Type | Basic | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | I-75 | NW 49 ST Interchange |  |  | I-75 | US 27 Interchange |  |  | I-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > | > | > |


| Time Period |  |  |  |  |  | rage D | sity (v | /mi/ln |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 27.5 | 27.5 | 23.3 | 25.1 | 25.5 | 25.8 | 21.9 | 24.5 | 25.1 | 25.0 | 18.5 | 22.0 | 22.0 |
| 11 | 30.2 | 29.9 | 25.3 | 27.2 | 28.0 | 28.3 | 23.4 | 26.3 | 26.9 | 26.1 | 19.1 | 22.9 | 22.6 |
| 10 | 30.9 | 31.0 | 25.4 | 27.2 | 27.7 | 27.9 | 23.0 | 26.2 | 26.3 | 25.6 | 19.0 | 23.1 | 22.7 |
| 9 | 32.2 | 34.2 | 24.7 | 26.1 | 26.7 | 27.2 | 22.4 | 24.8 | 25.3 | 24.9 | 18.6 | 22.5 | 22.2 |
| 8 | 34.2 | 40.5 | 26.1 | 27.5 | 27.9 | 28.5 | 23.9 | 27.8 | 28.6 | 27.2 | 19.9 | 23.8 | 23.5 |
| 7 | 36.3 | 39.6 | 28.0 | 29.4 | 30.6 | 30.5 | 25.2 | 28.2 | 29.0 | 28.5 | 20.9 | 25.0 | 24.9 |
| 6 | 34.9 | 33.7 | 27.3 | 29.1 | 30.0 | 30.7 | 25.2 | 28.7 | 30.1 | 28.8 | 20.8 | 25.1 | 24.7 |
| 5 | 33.0 | 31.7 | 26.9 | 28.7 | 29.4 | 29.7 | 24.4 | 27.0 | 27.4 | 26.6 | 19.6 | 23.4 | 23.1 |
| 4 | 28.4 | 27.9 | 23.7 | 25.3 | 25.8 | 26.2 | 21.9 | 24.0 | 24.2 | 24.0 | 18.1 | 21.4 | 21.1 |
| 3 | 26.9 | 26.5 | 22.2 | 23.6 | 23.8 | 24.3 | 20.2 | 22.3 | 22.5 | 22.4 | 16.6 | 19.6 | 19.4 |
| 2 | 24.3 | 23.5 | 19.7 | 20.8 | 20.9 | 21.5 | 17.6 | 19.1 | 18.9 | 18.9 | 14.1 | 17.0 | 16.7 |
| 1 | 19.0 | 18.7 | 15.6 | 16.6 | 16.6 | 16.9 | 14.0 | 15.3 | 15.1 | 15.1 | 11.3 | 13.5 | 13.2 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | I-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of Travel |  | > | > | > | > | > | > | > | > | > | > | > | > |

[^7]| Time Period | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 14.8 | 14.6 | 13.2 | 18.3 | 17.9 | 19.5 | 19.3 | 19.0 | 17.6 | 22.3 | 21.9 | 21.5 | 20.4 | 27.7 | 26.6 |
| 11 | 16.4 | 16.2 | 14.5 | 19.6 | 19.4 | 21.3 | 21.1 | 20.5 | 19.0 | 23.8 | 23.3 | 22.8 | 21.5 | 29.2 | 27.9 |
| 10 | 16.0 | 15.8 | 14.2 | 19.4 | 19.1 | 20.6 | 20.3 | 19.9 | 18.4 | 23.1 | 22.6 | 22.2 | 21.1 | 28.8 | 27.8 |
| 9 | 16.0 | 15.7 | 14.1 | 19.2 | 18.9 | 20.6 | 20.3 | 19.9 | 18.3 | 22.9 | 22.5 | 21.8 | 20.9 | 28.5 | 27.2 |
| 8 | 15.7 | 15.5 | 14.1 | 19.4 | 19.0 | 20.6 | 20.6 | 20.2 | 18.7 | 23.5 | 23.3 | 23.0 | 21.8 | 30.1 | 29.1 |
| 7 | 18.6 | 18.5 | 16.6 | 21.7 | 21.6 | 23.7 | 23.3 | 22.5 | 20.8 | 26.6 | 26.1 | 25.1 | 23.9 | 34.9 | 32.3 |
| 6 | 18.7 | 18.4 | 16.4 | 21.3 | 21.2 | 23.2 | 23.0 | 22.3 | 20.6 | 26.2 | 25.8 | 25.1 | 23.8 | 34.2 | 32.7 |
| 5 | 18.2 | 17.7 | 15.8 | 20.6 | 20.4 | 22.2 | 21.9 | 21.2 | 19.6 | 24.7 | 24.0 | 23.2 | 22.2 | 29.7 | 28.5 |
| 4 | 15.6 | 15.3 | 13.8 | 18.5 | 18.2 | 19.7 | 19.4 | 19.0 | 17.6 | 22.1 | 21.6 | 21.3 | 20.2 | 26.4 | 25.6 |
| 3 | 14.8 | 14.6 | 13.1 | 17.6 | 17.3 | 18.9 | 18.6 | 18.2 | 16.7 | 20.9 | 20.4 | 20.0 | 19.1 | 24.7 | 24.0 |
| 2 | 13.6 | 13.3 | 11.9 | 15.7 | 15.3 | 16.7 | 16.4 | 16.1 | 14.7 | 18.5 | 18.0 | 17.6 | 16.6 | 21.2 | 20.5 |
| 1 | 10.8 | 10.6 | 9.6 | 12.7 | 12.4 | 13.4 | 13.3 | 13.0 | 12.0 | 14.8 | 14.4 | 14.2 | 13.3 | 16.7 | 16.4 |
| Type | Bas | Diverge | Basic | Merge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | SR 326 Interchange |  |  |  |  | 1-75 | NW 49 ST Interchange |  |  | I-75 | US 27 Interchange |  |  | 1-75 |
| Length (ft) | 3001 | 1,503 | 2,225 | 1,499 | 272 | 1,500 | 2,017 | 1,500 | 7,580 | 1,496 | 3,494 | 1,500 | 3,388 | 1,500 | 2,489 |
| Direction of | Travel | > | > | > | $>$ | > | > | > | > | > | > | > | > | > | > |

LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $\begin{array}{lllllll}0.0 & >10.0 & >18.0 & >26.0 & >35.0 & >45.0\end{array}$
Upper: $10.0 \quad 18.0 \quad 26.0 \quad 35.0 \quad 45.0 \quad>$
Using HCM 2010 thresholds for informational purposes


Figure 6-39: DDI 2045 Speed and Density Time Plots (PM Peak)

| NORTHBOUND I-75-TIME PLOTS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | Average Speed (mph) |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 67.5 | 66.9 | 67.5 | 67.6 | 66.8 | 66.8 | 67.8 | 66.5 | 66.2 | 65.8 | 68.3 | 66.3 | 67.6 |
| 11 | 67.3 | 67.0 | 67.3 | 67.4 | 66.4 | 66.7 | 67.7 | 66.1 | 65.4 | 65.3 | 68.3 | 66.3 | 67.5 |
| 10 | 67.0 | 66.9 | 67.1 | 67.2 | 66.0 | 66.3 | 67.5 | 65.7 | 64.8 | 64.9 | 68.2 | 66.2 | 67.2 |
| 9 | 66.5 | 66.5 | 67.0 | 67.3 | 65.8 | 66.2 | 67.4 | 63.9 | 63.7 | 63.1 | 68.0 | 66.4 | 67.3 |
| 8 | 66.4 | 66.7 | 66.9 | 67.1 | 65.4 | 65.8 | 67.2 | 65.0 | 63.7 | 63.4 | 67.9 | 66.4 | 67.2 |
| 7 | 66.4 | 66.5 | 66.9 | 67.3 | 65.8 | 66.1 | 67.4 | 65.0 | 64.1 | 64.7 | 68.1 | 66.5 | 67.3 |
| 6 | 66.7 | 66.6 | 67.2 | 67.2 | 66.0 | 66.3 | 67.4 | 65.6 | 65.0 | 64.8 | 68.2 | 66.3 | 67.4 |
| 5 | 66.7 | 66.8 | 67.0 | 67.3 | 65.9 | 66.2 | 67.4 | 65.4 | 64.4 | 64.7 | 68.1 | 66.2 | 67.3 |
| 4 | 66.8 | 66.6 | 66.8 | 67.3 | 66.0 | 66.4 | 67.4 | 65.5 | 64.4 | 64.6 | 68.0 | 66.5 | 67.4 |
| 3 | 66.8 | 66.6 | 67.0 | 67.3 | 66.0 | 66.2 | 67.4 | 65.6 | 65.2 | 65.3 | 68.2 | 66.6 | 67.5 |
| 2 | 67.2 | 66.9 | 67.2 | 67.4 | 66.3 | 66.4 | 67.6 | 66.1 | 65.3 | 65.1 | 68.1 | 66.7 | 67.5 |
| 1 | 67.1 | 66.9 | 67.3 | 67.4 | 66.2 | 66.4 | 67.6 | 66.2 | 65.5 | 65.4 | 68.2 | 66.5 | 67.6 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | 1-75 | US 27 Interchange |  |  | 1-75 | NW 49 ST Interchange |  |  | 1-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction o | Travel | > | > | > | > | > | > | > | > | > | > | > | $>$ |


| Time Period | Average Density (veh/mi/ln) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 22.1 | 22.2 | 17.9 | 19.3 | 19.7 | 19.8 | 16.1 | 17.9 | 18.0 | 18.3 | 12.3 | 16.0 | 15.6 |
| 11 | 23.9 | 24.0 | 19.4 | 20.9 | 21.1 | 21.0 | 17.1 | 19.2 | 19.4 | 19.7 | 13.0 | 16.8 | 16.6 |
| 10 | 25.5 | 25.9 | 21.0 | 22.5 | 22.9 | 23.0 | 18.7 | 21.1 | 21.3 | 21.6 | 14.3 | 18.2 | 17.9 |
| 9 | 29.2 | 29.0 | 23.2 | 24.6 | 25.1 | 25.0 | 20.0 | 23.2 | 23.1 | 24.4 | 15.0 | 18.7 | 18.4 |
| 8 | 29.6 | 29.2 | 23.6 | 25.1 | 25.8 | 25.7 | 20.7 | 23.4 | 23.7 | 24.6 | 15.5 | 19.3 | 19.0 |
| 7 | 29.5 | 29.0 | 23.4 | 24.6 | 25.1 | 25.1 | 20.0 | 22.7 | 22.9 | 22.9 | 15.2 | 18.9 | 18.5 |
| 6 | 27.6 | 27.6 | 22.0 | 23.7 | 24.0 | 24.0 | 19.4 | 21.7 | 21.8 | 22.2 | 14.5 | 18.2 | 17.9 |
| 5 | 28.4 | 28.0 | 22.7 | 24.0 | 24.6 | 24.5 | 19.7 | 22.2 | 22.5 | 22.6 | 14.8 | 18.6 | 18.3 |
| 4 | 28.0 | 27.9 | 22.8 | 24.1 | 24.5 | 24.5 | 20.0 | 22.4 | 22.8 | 23.0 | 15.0 | 18.6 | 18.3 |
| 3 | 27.9 | 27.6 | 22.1 | 23.5 | 23.9 | 23.8 | 19.1 | 21.1 | 21.1 | 21.3 | 14.3 | 17.7 | 17.4 |
| 2 | 25.2 | 25.1 | 20.4 | 21.9 | 22.2 | 22.4 | 17.9 | 20.1 | 20.3 | 20.6 | 13.7 | 16.9 | 16.7 |
| 1 | 25.9 | 25.7 | 20.5 | 22.1 | 22.4 | 22.3 | 18.0 | 19.9 | 20.0 | 20.2 | 13.5 | 16.9 | 16.5 |
| Type | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic | Diverge | Basic | Merge | Basic |
| Int. | I-75 | US 27 Interchange |  |  | I-75 | NW 49 ST Interchange |  |  | I-75 | SR 326 Interchange |  |  | 1-75 |
| Length (ft) | 15,034 | 1,479 | 3,075 | 1,501 | 1,443 | 1,497 | 8,860 | 1,500 | 1,606 | 1,500 | 3,094 | 1,495 | 3,759 |
| Direction of | Travel | > | > | > | > | > | > | > | > | > | > | > | > |

[^8]LOS THRESHOLDS (Density in veh/mi/ln)
LOS: LOSA LOSB LOSC LOSD LOSE LOSF
Lower: $0.0 \quad>10.0 \quad>18.0 \quad>26.0 \quad>35.0 \quad>45.0$
$\begin{array}{llllll} & 26.0 & 35.0\end{array}$


### 6.2.4.5 Vissim Analysis Results -Network Performance

Tables 6-11 and 6-12 summarize the network performance. During the AM Peak, all network performance measures are improved under the Build alternatives when compared to the No Build. During the PM Peak, all network performance measures are also improved under the Build alternatives when compared to the No Build except for latent delay and latent demand under the Diamond alternative. It should be noted that all other measures for the Diamond alternative outperform No Build including an increase in Vehicles arrived and VMT. Overall, the Build alternatives demonstrate improved operations with substantial reductions in total delay and total stops during both the AM and PM peak hours while processing more vehicles.

Overall, the benefits of the build alternatives are visibly higher during the AM peak period. During the PM peak period, the benefits are not as significant due to the higher demand volumes. This results in higher congestion on I-75 southbound at the US 27 interchange as previously presented in Figure 6-39 (DDI speed /density for PM peak) compared to Figure 6-19 (No-Build speed /density for PM peak).

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Table 6-11 2045 Vissim Network Performance Summary - AM Peak

| 15-min <br> Period | No Build |  |  |  |  |  |  | Diamond |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total Delay (Hours) | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | VehicleMiles Traveled | Latent Delay (Hours) | Latent Demand (Vehicles) | $\begin{aligned} & \hline \text { Total } \\ & \text { Delay } \\ & \text { (Hours) } \\ & \hline \end{aligned}$ | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | Vehicle- <br> Miles <br> Traveled | Latent Delay (Hours) | Latent Demand (Vehicles) |
| 1 | 21 | 1,980 | 58 | 2,854 | 13,513 | 0 | 0 | 23 | 2,097 | 57 | 2,875 | 14,269 | 0 | 0 |
| 2 | 33 | 3,034 | 56 | 3,558 | 16,829 | 0 | 0 | 35 | 3,104 | 55 | 3,570 | 17,812 | 0 | 0 |
| 3 | 43 | 3,981 | 55 | 4,048 | 18,965 | 0 | 1 | 45 | 3,941 | 55 | 4,080 | 20,020 | 0 | 1 |
| 4 | 53 | 5,095 | 54 | 4,283 | 20,027 | 0 | 1 | 52 | 4,621 | 54 | 4,354 | 21,245 | 0 | 1 |
| 5 | 93 | 9,964 | 50 | 4,667 | 22,275 | 0 | 3 | 81 | 7,584 | 51 | 4,760 | 23,709 | 1 | 5 |
| 6 | 165 | 18,817 | 44 | 4,878 | 22,897 | 9 | 97 | 129 | 13,349 | 47 | 5,056 | 24,556 | 3 | 20 |
| 7 | 215 | 24,529 | 40 | 4,832 | 22,799 | 47 | 293 | 167 | 17,912 | 44 | 5,051 | 24,588 | 15 | 115 |
| 8 | 211 | 23,218 | 39 | 4,694 | 21,326 | 75 | 326 | 155 | 16,927 | 44 | 4,807 | 22,821 | 24 | 88 |
| 9 | 187 | 20,770 | 40 | 4,496 | 20,691 | 84 | 347 | 123 | 13,453 | 46 | 4,624 | 22,084 | 22 | 88 |
| 10 | 182 | 20,154 | 41 | 4,507 | 20,757 | 91 | 382 | 111 | 11,769 | 48 | 4,618 | 22,152 | 20 | 74 |
| 11 | 178 | 19,332 | 42 | 4,574 | 21,335 | 100 | 403 | 108 | 10,972 | 48 | 4,668 | 22,631 | 18 | 70 |
| 12 | 176 | 20,012 | 41 | 4,393 | 19,981 | 97 | 357 | 91 | 8,952 | 49 | 4,514 | 21,201 | 15 | 53 |
| Total ${ }^{1}$ | 1,557 | 170,886 | 46 | 51,784 | 241,395 | 503 | 2,210 | 1,120 | 114,681 | 49 | 52,977 | 257,088 | 118 | 515 |
|  | SPUI |  |  |  |  |  |  | ParClo SE |  |  |  |  |  |  |
| 1 | 23 | 2090 | 57 | 2875 | 14264 | 0 | 0 | 23 | 2125 | 57 | 2875 | 14328 | 0 | 0 |
| 2 | 34 | 3009 | 56 | 3577 | 17820 | 0 | 0 | 35 | 3096 | 56 | 3566 | 17880 | 0 | 0 |
| 3 | 44 | 3874 | 55 | 4082 | 20014 | 0 | 1 | 44 | 3874 | 55 | 4083 | 20114 | 0 | 1 |
| 4 | 50 | 4375 | 55 | 4357 | 21246 | 0 | 1 | 52 | 4658 | 54 | 4353 | 21321 | 0 | 1 |
| 5 | 78 | 7312 | 52 | 4769 | 23710 | 1 | 5 | 81 | 7714 | 51 | 4752 | 23805 | 1 | 5 |
| 6 | 128 | 13727 | 47 | 5029 | 24487 | 3 | 21 | 132 | 14051 | 47 | 5039 | 24579 | 3 | 23 |
| 7 | 175 | 19060 | 43 | 5017 | 24465 | 15 | 114 | 169 | 18212 | 44 | 5051 | 24692 | 19 | 140 |
| 8 | 165 | 18556 | 43 | 4809 | 22753 | 24 | 90 | 154 | 17284 | 44 | 4827 | 22958 | 28 | 99 |
| 9 | 134 | 14537 | 46 | 4631 | 22123 | 21 | 94 | 123 | 13474 | 46 | 4624 | 22178 | 23 | 82 |
| 10 | 113 | 12118 | 48 | 4646 | 22307 | 21 | 78 | 115 | 12508 | 47 | 4598 | 22233 | 20 | 76 |
| 11 | 106 | 10799 | 48 | 4670 | 22612 | 21 | 87 | 111 | 11598 | 48 | 4670 | 22731 | 19 | 83 |
| 12 | 89 | 9148 | 50 | 4498 | 21178 | 19 | 69 | 89 | 8780 | 50 | 4523 | 21322 | 19 | 73 |
| Total ${ }^{1}$ | 1,139 | 118,605 | 49 | 52,960 | 256,979 | 125 | 560 | 1,128 | 117,374 | 49 | 52,961 | 258,141 | 132 | 583 |
|  | ParClo NE |  |  |  |  |  |  | DDI |  |  |  |  |  |  |
| 1 | 23 | 2128 | 57 | 2878 | 14362 | 0 | 0 | 24 | 2,152 | 56 | 2,874 | 14,262 | 0 | 0 |
| 2 | 34 | 3092 | 56 | 3572 | 17922 | 0 | 0 | 36 | 3,142 | 55 | 3,565 | 17,796 | 0 | 0 |
| 3 | 43 | 3876 | 55 | 4085 | 20147 | 0 | 1 | 46 | 4,026 | 54 | 4,081 | 19,997 | 0 | 1 |
| 4 | 49 | 4399 | 55 | 4351 | 21375 | 0 | 1 | 53 | 4,666 | 54 | 4,359 | 21,230 | 0 | 1 |
| 5 | 80 | 7908 | 52 | 4742 | 23842 | 1 | 5 | 83 | 7,802 | 51 | 4,746 | 23,652 | 1 | 5 |
| 6 | 127 | 13403 | 47 | 5065 | 24763 | 3 | 22 | 127 | 13,118 | 47 | 5,087 | 24,632 | 3 | 19 |
| 7 | 166 | 18412 | 44 | 5035 | 24708 | 17 | 126 | 166 | 17,774 | 44 | 5,032 | 24,507 | 14 | 109 |
| 8 | 157 | 17602 | 44 | 4813 | 22849 | 27 | 99 | 160 | 17,568 | 43 | 4,797 | 22,682 | 22 | 89 |
| 9 | 125 | 13910 | 46 | 4620 | 22255 | 24 | 88 | 133 | 14,654 | 45 | 4,602 | 22,012 | 21 | 79 |
| 10 | 112 | 11879 | 48 | 4628 | 22364 | 20 | 69 | 116 | 12,211 | 47 | 4,630 | 22,262 | 19 | 74 |
| 11 | 110 | 11361 | 48 | 4657 | 22704 | 18 | 79 | 106 | 10,502 | 48 | 4,692 | 22,650 | 19 | 76 |
| 12 | 91 | 9359 | 49 | 4514 | 21334 | 18 | 68 | 89 | 8,646 | 49 | 4,507 | 21,177 | 17 | 60 |
| Total ${ }^{1}$ | 1,117 | 117,329 | 50 | 52,960 | 258,625 | 128 | 558 | 1,139 | 116,261 | 49 | 52,972 | 256,859 | 116 | 513 |

Table 6-12 2045 Vissim Network Performance Summary - PM Peak

| 15-min <br> Period | No Build |  |  |  |  |  |  | Diamond |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total Delay (Hours) | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | VehicleMiles Traveled | Latent Delay (Hours) | Latent Demand (Vehicles) | $\begin{aligned} & \hline \text { Total } \\ & \text { Delay } \\ & \text { (Hours) } \\ & \hline \end{aligned}$ | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | $\begin{aligned} & \hline \text { Vehicle- } \\ & \text { Miles } \\ & \text { Traveled } \end{aligned}$ | $\begin{gathered} \text { Latent } \\ \text { Delay } \\ \text { (Hours) } \end{gathered}$ | Latent Demand (Vehicles) |
| 1 | 78 | 6,781 | 51 | 4,465 | 20,171 | 0 | 2 | 82 | 6,530 | 50 | 4,551 | 21,439 | 1 | 10 |
| 2 | 88 | 7,486 | 49 | 4,428 | 19,854 | 4 | 20 | 89 | 6,757 | 49 | 4,544 | 21,083 | 8 | 39 |
| 3 | 113 | 9,992 | 47 | 4,572 | 21,238 | 12 | 73 | 105 | 8,117 | 48 | 4,670 | 22,647 | 25 | 143 |
| 4 | 137 | 12,609 | 45 | 4,739 | 21,598 | 37 | 183 | 121 | 10,180 | 47 | 4,877 | 23,030 | 54 | 258 |
| 5 | 158 | 16,407 | 43 | 4,748 | 21,700 | 67 | 330 | 135 | 11,765 | 46 | 4,866 | 23,204 | 85 | 396 |
| 6 | 175 | 17,801 | 42 | 4,724 | 21,355 | 105 | 474 | 150 | 14,701 | 44 | 4,889 | 22,816 | 117 | 507 |
| 7 | 198 | 20,597 | 41 | 4,759 | 22,182 | 151 | 717 | 165 | 16,415 | 43 | 4,931 | 23,729 | 154 | 698 |
| 8 | 221 | 24,377 | 39 | 4,839 | 22,198 | 217 | 971 | 192 | 20,928 | 42 | 4,973 | 23,908 | 205 | 905 |
| 9 | 236 | 26,684 | 38 | 4,797 | 21,984 | 275 | 1,199 | 210 | 23,349 | 40 | 4,943 | 23,465 | 259 | 1,144 |
| 10 | 222 | 25,246 | 38 | 4,620 | 20,428 | 316 | 1,282 | 191 | 21,469 | 40 | 4,745 | 21,660 | 304 | 1,247 |
| 11 | 176 | 19,134 | 40 | 4,429 | 19,423 | 327 | 1,310 | 145 | 14,996 | 43 | 4,480 | 20,533 | 316 | 1,259 |
| 12 | 134 | 13,881 | 43 | 4,152 | 18,122 | 326 | 1,255 | 112 | 10,827 | 46 | 4,208 | 19,186 | 319 | 1,252 |
| Total ${ }^{1}$ | 1,936 | 200,995 | 43 | 55,272 | 250,253 | 1,837 | 7,816 | 1,697 | 166,034 | 45 | 56,677 | 266,700 | 1,847 | 7,858 |
|  | SPUI |  |  |  |  |  |  | Parclo SE |  |  |  |  |  |  |
| 1 | 80 | 6363 | 51 | 4550 | 21447 | 1 | 9 | 84 | 6471 | 50 | 4535 | 21540 | 1 | 7 |
| 2 | 85 | 6354 | 50 | 4536 | 21070 | 8 | 38 | 90 | 6940 | 49 | 4545 | 21164 | 7 | 35 |
| 3 | 102 | 7967 | 49 | 4688 | 22644 | 24 | 136 | 109 | 8666 | 48 | 4671 | 22738 | 23 | 131 |
| 4 | 118 | 9661 | 47 | 4883 | 23027 | 52 | 251 | 125 | 10183 | 47 | 4890 | 23133 | 50 | 245 |
| 5 | 126 | 11043 | 47 | 4883 | 23212 | 84 | 394 | 135 | 11887 | 46 | 4878 | 23340 | 81 | 377 |
| 6 | 139 | 12811 | 45 | 4885 | 22880 | 116 | 504 | 145 | 13330 | 45 | 4893 | 22963 | 113 | 492 |
| 7 | 156 | 14962 | 44 | 4927 | 23713 | 153 | 699 | 162 | 15662 | 44 | 4933 | 23809 | 151 | 687 |
| 8 | 182 | 18744 | 42 | 4977 | 23906 | 204 | 896 | 188 | 19686 | 42 | 4992 | 24011 | 200 | 876 |
| 9 | 200 | 23347 | 41 | 4963 | 23548 | 251 | 1096 | 203 | 22833 | 41 | 4960 | 23613 | 250 | 1102 |
| 10 | 184 | 21624 | 41 | 4768 | 21689 | 291 | 1177 | 185 | 21061 | 41 | 4764 | 21767 | 292 | 1186 |
| 11 | 139 | 14410 | 44 | 4467 | 20437 | 303 | 1213 | 139 | 14054 | 44 | 4463 | 20587 | 306 | 1215 |
| Total ${ }^{1}$ | 103 | 9905 | 47 | 4193 | 19083 | 309 | 1218 | 105 | 10108 | 47 | 4198 | 19249 | 307 | 1211 |
|  | 1,614 | 157,191 | 46 | 56,720 | 266,656 | 1,796 | 7,631 | 1,670 | 160,881 | 45 | 56,722 | 267,914 | 1,781 | 7,564 |
|  | Parclo Ne |  |  |  |  |  |  | DDI |  |  |  |  |  |  |
| 1 | 81 | 6789 | 50 | 4546 | 21597 | 1 | 8 | 85 | 6,904 | 50 | 4,545 | 21,429 | 1 | 9 |
| 2 | 87 | 7077 | 50 | 4553 | 21271 | 5 | 26 | 89 | 6,701 | 49 | 4,553 | 21,113 | 7 | 29 |
| 3 | 104 | 8561 | 49 | 4686 | 22800 | 20 | 130 | 108 | 8,479 | 48 | 4,672 | 22,600 | 21 | 127 |
| 4 | 118 | 10310 | 47 | 4878 | 23208 | 49 | 240 | 123 | 9,860 | 47 | 4,892 | 23,030 | 50 | 239 |
| 5 | 133 | 12710 | 46 | 4853 | 23375 | 80 | 368 | 135 | 11,555 | 46 | 4,870 | 23,210 | 79 | 374 |
| 6 | 146 | 14281 | 45 | 4912 | 23050 | 112 | 496 | 146 | 13,453 | 44 | 4,901 | 22,797 | 112 | 499 |
| 7 | 157 | 15501 | 44 | 4937 | 23943 | 150 | 676 | 160 | 15,527 | 44 | 4,911 | 23,637 | 153 | 702 |
| 8 | 189 | 21688 | 42 | 4961 | 24092 | 196 | 858 | 184 | 19,593 | 42 | 4,985 | 23,932 | 206 | 902 |
| 9 | 214 | 25921 | 40 | 4951 | 23671 | 242 | 1075 | 211 | 23,172 | 40 | 4,912 | 23,441 | 255 | 1,110 |
| 10 | 195 | 23974 | 40 | 4763 | 21840 | 285 | 1162 | 191 | 21,240 | 40 | 4,794 | 21,733 | 293 | 1,190 |
| 11 | 145 | 16518 | 43 | 4508 | 20685 | 299 | 1188 | 144 | 14,620 | 43 | 4,504 | 20,576 | 302 | 1,201 |
| 12 | 105 | 10299 | 47 | 4201 | 19252 | 305 | 1205 | 106 | 9,755 | 46 | 4,199 | 19,142 | 307 | 1,217 |
| Total ${ }^{1}$ | 1,674 | 173,629 | 45 | 56,749 | 268,784 | 1,744 | 7,432 | 1,682 | 160,859 | 45 | 56,738 | 266,640 | 1,786 | 7,599 |

### 6.3 Queue Analysis

Suggested turn lane lengths were developed for the proposed interchange ramp terminal intersections using the Synchro 10 queue output and Vissim Max Queue results from the 2045 Design Year analysis. Queue lengths measured from Vissim are based on actual queue lengths generated by the simulation. Synchro 10 queue length measurements are based on the Synchro Percentile Delay Method which is defined as:

$$
Q=\frac{v}{3600} *(R-6) *\left[1+\frac{1}{\frac{s}{v}-1}\right] * \frac{L}{n * f L U}=\text { Queue Length }(\text { feet })
$$

Where:
$R=$ Red time (sec)
$s=$ Saturation Flow Rate (vph)
$v$ = Arrival Rate (vph)
$L=$ Length of vehicles including space between (ft)
$n=$ Number of Lanes
fLU = Lane Utilization Factor

Based on the Diamond, SPUI, Parclo-SE, Parclo-NE, and DDI build alternatives geometry previously provided, the recommended turn lane storage lengths are provided in Table 6-13. It should be noted that recommended storage lengths do not include deceleration and taper lengths. Additional storage is also suggested to accommodate the heavy truck traffic that is anticipated at the proposed interchange to support the industrial/commercial Ocala 489 commerce park. A notable difference in queue lengths are reported between Synchro and Vissim for the southbound right turn movement at the northbound I-75 ramp intersection under the ParClo NE alternative. The southbound right turn movement is the northeast quadrant loop ramp terminus with NW 49 ${ }^{\text {th }}$ Street which is modeled as a stop condition. The Vissim analysis suggests that this movement under the ParClo NE alternative would likely require signalization in order to provide adequate gaps in NW 49 ${ }^{\text {th }}$ Street traffic flow and reduce the observed queue length.

Table 6-13: 2045 Recommended Turn Lane Storage Lengths

| Interchange | Ramps | Movement | Turn Bay Length ${ }^{1}$ (ft) | 95th Percentile Queue Length ${ }^{2}$ (ft) |  | Vissim Max Queue Lengths (ft) |  | Recommended Storage Length ${ }^{3}$ (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM | PM | AM | PM |  |
| Diamond | I-75 NB | EBL | 300 | 0 | 96 | 2 | 8 | 100 |
|  |  | NBL/R | 300 | 62 | 126 | 215 | 230 | 250 |
|  |  | WBR | 400 | 0 | 0 | 3 | 3 | 25 |
|  | I-75 SB | WBL | 300 | 118 | 102 | 167 | 96 | 175 |
|  |  | SBL/R | - | 51 | 90 | 185 | 215 | 225 |
|  |  | EBR | 450 | 27 | m8 | 132 | 77 | 150 |
| SPUI | I-75 NB | EBL | 275 | m98 | m119 | 151 | 132 | 175 |
|  |  | NBL/R | 300 | 75 | \#189 | 221 | 251 | 275 |
|  |  | WBR | 700 | 40 | 26 | 29 | 16 | 50 |
|  |  | WBL | 390 | 153 | 129 | 177 | 146 | 200 |
|  | I-75 SB | SBL/R | 450 | 69 | 76 | 149 | 170 | 175 |
|  |  | EBR | 640 | m144 | m133 | 94 | 56 | 100 |
| Parclo-SE | I-75 NB | EBR (FF) | 560 | 0 | 0 | 13 | 7 | 25 |
|  |  | WBR (FF) | 300 | 0 | 0 | 39 | 44 | 50 |
|  |  | NBL/R | 83 | 62 | 169 | 216 | 238 | 250 |
|  | I-75 SB | WBL | 300 | 120 | 117 | 264 | 323 | 325 |
|  |  | SBL/R | 550 | 65 | 90 | 175 | 212 | 225 |
|  |  | EBR | 375 | m32 | m7 | 143 | 93 | 150 |
| Parclo-NE | I-75 NB | EBL | 600 | 14 | 5 | 126 | 56 | 150 |
|  |  | NBR | - | 40 | 56 | 203 | 254 | 275 |
|  |  | SBR | - | 122 | 165 | 409 | 942 | 950 |
|  |  | WBL | 300 | 142 | 138 | 150 | 147 | 150 |
|  | I-75 SB | SBL/R | 550 | 65 | 99 | 189 | 248 | 250 |
|  |  | EBR | 375 | m32 | 0 | 114 | 89 | 125 |
| DDI | I-75 NB | WBR | 250 | 40 | 37 | 4 | 0 | 50 |
|  |  | NBL | - | 0 | 0 | 228 | 256 | 275 |
|  |  | EBR | 300 | 24 | 13 | 201 | 265 | 275 |
|  | -75 SB | SBL | - | 0 | 0 | 166 | 207 | 225 |

${ }^{1}$ Turn Bay Length used in traffic analysis; Turn Bay Length = Storage + Deceleration + Taper Lengths
${ }^{2}$ Queue length from Synchro Analysis
${ }^{3}$ Recommended Storage Length does not include Deceleration+ Taper Lengths. Min. of 25 feet recommended
${ }^{4}$ m-Volume for $95^{t} h$ percentile queue is metered by upstream signal
${ }^{5}$ \#-95th percentile volume exceeds capacity, queue may be longer

## 7 Future Conditions Safety

In accordance with the approved MLOU, a safety analysis was conducted for future conditions utilizing the predictive methods set forth in the HSM Parts C and D. HSM Part C provides an outline for applying Safety Performance Functions (SPFs) to predict crash frequency and severity according to roadway geometry, intersection geometry, and traffic conditions. HSM Part D provides an outline for applying Crash Modification Factors (CMFs) to the forecasted crash frequencies and severities to account for deviations from the base conditions of the Part C predictions.

Consistent with the existing conditions safety analysis, the AOI includes the I-75 mainline between US 27 and SR 326 (broken into two segments to account for the new interchange at NW 49 ${ }^{\text {th }}$ Street), the I-75 interchanges at US 27 and at SR 326, as well as the following adjacent segments and intersections:

- Intersection of US 27 and NW 44 ${ }^{\text {th }}$ Avenue
- Intersection of US 27 and NW 35 ${ }^{\text {th }}$ Avenue Road
- Segment of US 27 from NW $44^{\text {th }}$ Avenue to I-75 southbound ramps
- Segment of US 27 from I-75 northbound ramps to NW 35 ${ }^{\text {th }}$ Avenue Road
- Segment of SR 326 one-half mile west of I-75 southbound off-ramp
- Segment of SR 326 one-half mile east of I-75 northbound ramps
- Segment of NW $44^{\text {th }}$ Avenue from US 27 to SR 326
- Intersection of NW 49 ${ }^{\text {th }}$ Street and NW 44 ${ }^{\text {th }}$ Avenue

For the five Build alternatives (Diamond, SPUI, Parclo-SE, Parclo-NE and DDI), the Build scenario analyses include the following segments and intersections due to the addition of the NW 49 ${ }^{\text {th }}$ Street Interchange:

- I-75 interchange with NW 49 ${ }^{\text {th }}$ Street (varies by Build scenario)
- Intersection of NW 49 ${ }^{\text {th }}$ Street and NW 44 ${ }^{\text {th }}$ Avenue
- Segment of NW 49 ${ }^{\text {th }}$ Street from NW 44 ${ }^{\text {th }}$ Avenue to I-75 southbound ramps
- Segment of NW $49^{\text {th }}$ Street one-half mile east of I-75 northbound ramps

The following sections illustrate some of the factors that contributed to forecasted crash rates and severities in different portions of the future roadway network and the resulting predictions. The HSM Worksheets used to calculate the anticipated future crash rates are provided in Appendix K.

### 7.1 Predicted Crashes

### 7.1.1 I-75 Mainline

The I-75 mainline within this project's AOI remains the same in the future conditions analysis as the existing conditions analysis, aside from the addition of on- and off-ramps at the proposed NW 49 ${ }^{\text {th }}$ Street interchange for the Build scenarios. The traffic volumes summarized in Table 71 were utilized for the crash predictions for the I-75 mainline.

## Table 7-1: I-75 Mainline 2045 AADT

| From |  | 2045 AADT |  |
| :--- | :--- | ---: | ---: |
|  | To | No Build | Build |
|  | SR 326 Interchange | 94,200 | 93,800 |
| SR 326 Interchange | Proposed Interchange | 107,100 | 109,300 |
| Proposed Interchange | US 27 Interchange | 107,100 | 118,900 |
| US 27 Interchange | S of US 27 Interchange | 131,300 | 137,300 |

The HSM worksheets were utilized to predict the number of annual crashes expected in year 2045. The HSM prediction method is based on the projected 2045 AADT volumes and geometric properties of the I-75 mainline (horizontal curves, lane widths, shoulder widths, presence of median barriers, and presence of rumble strips). Figure 7-1 provides the segmentation for the HSM analysis.

The predicted number of annual crashes ranges from approximately 132 crashes per year for the Parclo-SE scenario to approximately 143 crashes per year for the No Build scenario. Table 7-2 summarizes the predicted number of annual crashes on the I-75 mainline for the No Build and Build scenarios.

Table 7-2: Predicted 2045 Annual Crashes I-75 Mainline (S of US 27 to N of SR 326)

| Alternative | Fatal/Injury | PDO* | Total |
| :--- | ---: | ---: | ---: |
| No Build | 40.3 | 102.8 | $\mathbf{1 4 3 . 1}$ |
| Build Diamond | 38.7 | 99.4 | $\mathbf{1 3 8 . 1}$ |
| Build SPUI | 39.1 | 100.9 | $\mathbf{1 4 0 . 0}$ |
| Build Parclo SE | 36.9 | 95.2 | $\mathbf{1 3 2 . 1}$ |
| Build Parclo NE | 37.9 | 97.8 | $\mathbf{1 3 5 . 7}$ |
| Build DDI | 38.7 | 99.4 | $\mathbf{1 3 8 . 1}$ |

[^9]Figure 7-1: I-75 HSM Segmentation






### 7.1.2 Interchanges

## I-75 and US 27 Interchange and I-75 and SR 326 Interchange

No improvements are planned to the two interchanges adjacent to the proposed NW 49 ${ }^{\text {th }}$ Street interchange in conjunction with the proposed interchange construction. The introduction of the NW 49 ${ }^{\text {th }}$ Street interchange will alter travel patterns at the adjacent interchanges in the Build scenario. As a result, the number of annual crashes expected at the US 27 and SR 326 interchanges vary between the No Build scenario and the Build scenarios. The future traffic volumes at the adjacent interchanges are consistent between the five Build scenarios. Therefore, the projected number of crashes does not differ between the Build scenarios and a single value is reported.

The number of predicted crashes calculated for the interchanges includes the merge areas, diverge areas, ramp segments, and ramp terminals. A summary of the predicted number of annual crashes at the adjacent interchanges is provided in Table 7-3 for the No Build and Build scenarios.

Table 7-3: Predicted 2045 Annual Crashes I-75 Interchanges (US 27 and SR 326)

| I-75 and US 27 Interchange |  |  |  |
| :--- | :---: | :---: | :---: |
| Alternative | Fatal/Injury | PDO | Total |
| No Build | 28.2 | 39.9 | $\mathbf{6 8 . 1}$ |
| Build Diamond/SPUI/Parclos/DDI | 27.1 | 38.4 | $\mathbf{6 5 . 5}$ |
| I-75 and SR 326 Interchange |  |  |  |
| Alternative | Fatal/Injury | PDO | Total |
| No Build | 41.2 | 76.6 | $\mathbf{1 1 7 . 8}$ |
| Build Diamond/SPUI/Parclos/DDI | 40.2 | 77.4 | $\mathbf{1 1 7 . 6}$ |

## I-75 and NW 49 ${ }^{\text {th }}$ Street Interchange

The primary difference in predicted number of annual crashes between the No Build and Build scenarios is the differing geometry for the five NW 49 ${ }^{\text {th }}$ Street interchange Build alternatives. There is no difference in projected traffic volume for the five Build scenarios and the difference in predicted number of crashes is directly related to the geometric characteristics. The number of predicted crashes reported for the interchange includes the merge areas, diverge areas, ramp segments, and ramp terminal intersections. The HSM does not provide CMFs for a DDI. However, there are sources that provide CMFs for the conversion of a Diamond Interchange to DDI; reference information provided in Appendix K. The average of two applicable "diamond to

DDI conversion" CMFs (average of CMF ID 8278 and CMF ID 8258) was used to determine the DDI ramp terminals predicted crashes. In addition, there are also methodology limitations for the analysis of the SPUI. CMF results for a Diamond Conversion to SPUI were not consistent; decreases and increases in crashes were both concluded. Therefore, a conversion factor was not applied and the SPUI ramp terminal intersection was evaluated as a four-leg intersection. Diamond Conversion to SPUI reference information is provided in Appendix K.

A summary of the predicted number of annual crashes at the proposed interchange is provided in Table 7-4 for the five Build alternatives. The No Build scenario does not include an interchange at I-75 at NW 49 ${ }^{\text {th }}$ Street, so it is excluded from the table.

Table 7-4: Predicted 2045 Annual Crashes I-75 at NW 49 ${ }^{\text {th }}$ Street Interchange

| Alternative | Fatal/Injury | PDO | Total |
| :--- | :---: | :---: | :---: |
| Build Diamond | 11.9 | 25.3 | $\mathbf{3 7 . 2}$ |
| Build SPUI | 8.0 | 22.2 | $\mathbf{3 0 . 2}$ |
| Build Parclo-SE | 12.9 | 26.6 | $\mathbf{3 9 . 5}$ |
| Build Parclo-NE | 10.2 | 19.2 | $\mathbf{2 9 . 4}$ |
| Build DDI | 8.0 | 17.5 | $\mathbf{2 5 . 5}$ |

Based on the proposed geometry and traffic controls of the respective alternatives, the DDI interchange configuration results in the fewest predicted annual crashes, followed by the ParCloNE, SPUI, Parclo-SE, and Diamond build alternatives.

Treatment and volume of left turn movements are a defining factor between interchange types. The Diamond, ParClo-SE, and ParClo-NE alternatives treat the southbound ramp movements similarly through the provision of a signalized intersections. The SPUI combines movements with the northbound ramps and the DDI crossover intersections allow for the treatment of left turn movements similarly to a typical right turn movement, therefore reducing conflict points. In addition, the Diamond alternative provides for left turns at two separate intersections; introducing a second intersection increases the potential of additional crashes. Both Parclo alternatives also have a second signalized intersection. The loop ramps reduce the left turn volumes at the second intersection, with the Parclo-NE loop serving the highest of all four left-turn movements; reducing the potential of left turn crashes at the ramp terminus.

### 7.1.3 Arterial Segments

No improvements are planned for the US 27 and SR 326 arterials with the proposed NW $49^{\text {th }}$ Street interchange construction. Therefore, the geometric CMF's are consistent between the No Build and Build scenarios. For the HSM Analysis for the arterial segments and intersections, the
segmentation of US 27, NW 49 ${ }^{\text {th }}$ Street (No Build) and SR 326 are provided on Figure 7-2; and provided on Figure 7-3 for NW 49 ${ }^{\text {th }}$ Street under Build scenarios. There is a minor variation in projected AADT volumes between the No Build and Build scenarios that results in different projected numbers of annual crashes. For example, traffic growth on NW $44^{\text {th }}$ Avenue is projected to be greater in the No Build scenario than in the Build scenarios, leading to a higher predicted number of crashes in the No Build scenario.

In the No Build scenario, NW 49 ${ }^{\text {th }}$ Street would be constructed across I-75 via an overpass without an interchange with I-75. The traffic volume on NW 49 ${ }^{\text {th }}$ Street east and west of the proposed interchange is projected to be less in the No Build scenario than in the Build scenarios, resulting in fewer predicted crashes. A summary of the predicted number of annual crashes on the arterial segments is provided in Table 7-5 for the No Build and Build scenarios.

Table 7-5: Predicted 2045 Annual Crashes Arterial Segments

| Roadway From | To | Scenario | Fatal/ Injury | PDO | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
| US 27 |  | No Build | 6.6 | 17.0 | 23.6 |
| NW 44 ${ }^{\text {th }}$ Avenue | NW 35 ${ }^{\text {th }}$ Avenue Road | Build | 6.4 | 16.3 | 22.7 |
| SR 326 |  | No Build | 4.7 | 12.0 | 16.7 |
| $1 / 2$-mile west of NW $44^{\text {th }}$ Avenue | 1⁄2-mile E of I-75 NB ramps | Build | 4.6 | 11.8 | 16.4 |
| NW 44 ${ }^{\text {th }}$ Avenue |  | No Build | 3.0 | 8.0 | 11.0 |
| US 27 | SR 326 | Build | 2.0 | 5.4 | 7.4 |
| NW 49 ${ }^{\text {th }}$ Street |  | No Build | 0.2 | 0.7 | 0.9 |
| NW 44 ${ }^{\text {th }}$ Avenue | 1⁄2-mile E of I-75 NB ramps | Build | 0.3 | 0.7 | 1.0 |

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Figure 7-2: US 27, NW 49 ${ }^{\text {th }}$ Street (No Build) and SR 326 HSM Segmentation


Figure 7-3: NW 49th ${ }^{\text {th }}$ Street Build Conditions HSM Segmentation

### 7.1.4 Intersections

In addition to the ramp terminal intersections evaluated as part of the interchanges, three other intersections within the AOI were evaluated to predict year 2045 annual crashes: US 27 at NW $44^{\text {th }}$ Avenue, US 27 at NW $35^{\text {th }}$ Avenue Road, and NW $44^{\text {th }}$ Avenue at NW 49 ${ }^{\text {th }}$ Street. A summary of the predicted number of annual crashes at the adjacent intersections is provided in Table 7-6 for the No Build and Build scenarios.

Table 7-6: Predicted 2045 Annual Crashes Intersections

| Intersection | Scenario | Fatal/ <br> Injury | PDO | Total |
| :--- | :--- | :---: | :---: | :---: |
| US 27 at | No Build | 3.0 | 5.1 | $\mathbf{8 . 1}$ |
| NW 44 ${ }^{\text {th }}$ Avenue | Build Diamond/SPUI/Parclos/DDI | 2.8 | 4.6 | $\mathbf{7 . 4}$ |
| US 27 at | No Build | 3.8 | 6.3 | $\mathbf{1 0 . 1}$ |
| NW 35 ${ }^{\text {th }}$ Avenue Road | Build Diamond/SPUI/Parclo/DDI | 3.6 | 6.0 | $\mathbf{9 . 6}$ |
| NW 49 ${ }^{\text {th }}$ Street at | No Build | 0.8 | 1.6 | $\mathbf{2 . 4}$ |
| NW 44 ${ }^{\text {th }}$ Avenue | Build Diamond/SPUI/Parclos/DDI | 0.7 | 1.3 | $\mathbf{2 . 0}$ |

### 7.2 Future Predicted Safety Evaluation Summary

The cumulative results of the HSM predictive crash analyses for year 2045 are summarized in Tables 7-7 and 7-8.

Table 7-7: AOI Cumulative Predicted 2045 Annual Crash Summary

| Location | FI | PDO | $\begin{gathered} \text { NO } \\ \text { BUILD } \end{gathered}$ | FI | PDO | BUILD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I-75 (S of US 27-N Ramps \& S Ramps-N of SR 326) | 18.5 | 48.1 | 66.6 | 19.4 | 51.0 | 70.3 |
| I-75 \& US 27 Interchange ${ }^{1}$ | 28.2 | 39.9 | 68.0 | 27.1 | 38.4 | 65.5 |
| I-75 \& SR 326 Interchange ${ }^{1}$ | 41.2 | 76.6 | 117.7 | 40.2 | 77.4 | 117.7 |
| US 27 (Arterial \& Intersections) | 13.5 | 28.4 | 41.8 | 12.8 | 27.0 | 39.8 |
| SR 326 (Arterial \& Intersections) | 4.7 | 12.0 | 16.7 | 4.6 | 11.8 | 16.4 |
| NW 44 ${ }^{\text {th }}$ Avenue AOI ( N \& S of NW 49 ${ }^{\text {th }}$ St) | 3.0 | 8.0 | 11.0 | 2.0 | 5.4 | 7.4 |
| TOTALS | 109.0 | 212.9 | 321.9 | 106.1 | 211.0 | 317.2 |

${ }^{1}$ Merge/Diverge/Ramps/Ramp Termini

## Table 7-8: Project Site Predicted 2045 Annual Crashes

| Location | DIAMOND |  |  | SPUI |  |  | ParClo SE |  |  | ParClo NE |  |  | DDI |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total |
| I-75 (N of US 27 to NW 49 ${ }^{\text {th }}$ Street to $S$ of SR 326) | 19.4 | 48.5 | 67.8 | 19.8 | 49.9 | 69.7 | 17.6 | 44.3 | 61.8 | 18.5 | 46.8 | 65.3 | 19.4 | 48.5 | 67.8 |
| I-75 \& NW 49 ${ }^{\text {th }}$ Street Interchange ${ }^{1}$ | 11.9 | 25.3 | 37.2 | 8.0 | 22.2 | 30.1 | 12.9 | 26.6 | 39.5 | 10.2 | 19.2 | 29.4 | 8.0 | 17.5 | 25.5 |
| NW 49 ${ }^{\text {th }}$ Street, NW 44 ${ }^{\text {th }}$ Avenue to I-75 | 0.1 | 0.2 | 0.3 | 0.1 | 0.3 | 0.4 | 0.1 | 0.2 | 0.3 | 0.1 | 0.2 | 0.3 | 0.1 | 0.2 | 0.3 |
| NW 49 ${ }^{\text {th }}$ Street, East of 1-75 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 |
| NW 44 ${ }^{\text {th }}$ Avenue at NW 49 ${ }^{\text {th }}$ Street | 0.7 | 1.3 | 2.0 | 0.7 | 1.3 | 2.0 | 0.7 | 1.3 | 2.0 | 0.6 | 1.3 | 1.9 | 0.7 | 1.3 | 2.0 |
| TOTALS | 32.2 | 75.8 | 108.0 | 28.7 | 74.2 | 102.9 | 31.4 | 72.9 | 104.3 | 29.6 | 68.1 | 97.7 | 28.3 | 68.0 | 96.3 |

${ }^{1}$ Merge/Diverge/Ramps/Ramp Termini
Based on the predicted number of crashes, the project AOI shows a reduction in total crashes from 321.9 crashes under No Build to 317.2 crashes under Build conditions. A comparison of the number of predicted crashes under the five Build alternatives for the project site shows that the DDI alternative results in the lowest number of predicted crashes ( 96.3 crashes). The ParCloNE alternative is the second-best performing alternative with a total of 97.7 predicted crashes. The Diamond alternative results in the highest number of predicted crashes (108.0 crashes).

The Build condition is expected to decrease the number of predicted crashes. However, there are several locations with existing safety concerns; they are reflected on the district high crash locations list and/or have average crash rates higher than the statewide average. These safety deficiencies may still be present and require additional improvements. One such location is US 27 at NW 44 ${ }^{\text {th }}$ Avenue; under Build conditions, crashes are predicted to decrease. However, the predicted reduction in crashes may not be sufficient to offset existing safety conditions. The actual crash rate is higher than the statewide average crash rate; and it is a districtwide high crash location. Future operational analysis show significant delays eastbound during AM and westbound in PM. Since both volumes and delays decrease to/from NW $44^{\text {th }}$ Avenue, it reflects a capacity issue with US 27. Based on the operational analysis, congested conditions contribute to these safety issues. Capacity improvements, reduction of conflict points and other major improvements are likely required.

## 8 Environmental Impacts

This section describes existing environmental conditions and assesses the potential for environmental "fatal flaws" or issues that might influence or impact the acceptance of a recommended alternative. At this time there are no known environmental fatal flaws or resources of significant concern within the proposed project footprint. A PD\&E study is ongoing and will document the baseline conditions and potential impacts to the social, natural, and physical environments.

This environmental analysis used Geographic Information System (GIS) data as well as data from the Florida Department of Environmental Protection (FDEP), St. John's River Water Management District (SJRWMD), Southwest Florida Water Management District (SWFWMD), U.S. Fish and Wildlife Service (USFWS) and other sources described in each resource section below. The summary report from the FDOT Efficient Transportation Decision Making (ETDM) process was also consulted in evaluating potential impacts to each resource. The majority of the project area was also inspected in the field by an environmental scientist.

### 8.1 Project Area Description

The project is located along I-75, northwest of the City of Ocala in Marion County. The project area is bisected by I-75. On the west side of I-75, NW $44^{\text {th }}$ Avenue parallels I-75 and provides a north-south route between the nearest adjacent interstate exit/entrance ramps. To the west of NW $44^{\text {th }}$ Avenue and immediately south of NW 49 ${ }^{\text {th }}$ Street is a small residential area. Several businesses and complexes of warehouses, some currently unused, are located between NW $44^{\text {th }}$ Avenue and I-75. These include Barracuda Boat and RV Storage, Hickory Springs Manufacturing Company, Quality Bedding, Scorpion Performance Anodize Inc., Just in Time Machining, and All-In Removal waste disposal.

To the east of I-75, most the project area is under agricultural use and owned by the Baldwin Angus Ranch. Southeast of the project is the Magnum Materials limestone mine. The project will require right-of-way from both the Baldwin Angus Ranch and a small area in the northeast corner of the mine. South of the mine, and east of I-75, is a recently developed regional shipping hub. This area currently includes major distribution centers for Federal Express, Chewy, and Auto Zone. Land use cover descriptions provided for both uplands and wetlands are classified utilizing the Florida Land Use Cover and Forms Classifications System (FLUCCS) designation. Existing land use in the project area was initially determined utilizing U.S. Geological Survey (USGS)
maps, historical images, aerial photographs, and land use mapping from the SJRWMD (2012). Land use categories reported by SJRWMD were verified in the field. The predominant land use types in the project area west of I-75 are Other Light Industrial (FLUCCS 1550), Rural Land in Transition (FLUCCS 7410), Field Crops (FLUCCS 2150), and Improved Pastures (FLUCCS 2110). East of I-75, the predominant land types are Improved Pastures (FLUCCS 2110) with a smaller area of Field Crops (FLUCCS 2150), both of which are part of the Baldwin Angus Ranch. The Magnum Materials mine in the southeastern part of the project area is mapped as Reclaimed Lands (FLUCCS 1650) and Limerock or Dolomite (FLUCCS 1632) Elevations in the project area range from approximately 65 to approximately 120 feet above sea level.

### 8.2 Historic or Archaeological Sites

No historic or archaeological resources were identified that might act as fatal flaws or strongly impact acceptance of the recommended alternative. The summary degree of effect in the ETDM for Historic and Archaeological Sites was rated None by the SWFWMD, Minimal by the FHWA, and Moderate by the Florida Department of State. A review of the Florida Master Site File revealed one historic structure (8MR01660) and six archaeological sites that were determined ineligible for listing on the National Register of Historic Places (NRHP). The review also yielded one historic linear resource, the Seaboard Coast Line Railroad (8MR03621), which is considered eligible for listing on the NRHP and is located within one mile of the project. The historic Mt. Tabor Cemetery is located nearby and has not yet been evaluated by the State Historic Preservation Officer (SHPO). A Cultural Resources Assessment Survey is being developed as part of the PD\&E study and will involve additional research and field investigations to determine potential impacts to historic or archaeological resources.

### 8.3 Wetlands

There are no wetlands in the project area, so there are no anticipated short-term or long-term adverse impacts to wetlands. OSWs in the project area are limited to small roadside ditches and swales that are part of the manmade drainage system. Several stormwater ponds and detention ponds occur on the mine property but are outside the project area. A Natural Resources Evaluation Report is being prepared as part of the PD\&E study and will contain additional detail.

### 8.4 Threatened and Endangered Species and Habitats

Potential habitat for federally and state listed species was identified in the project area. No federally listed species were observed in the project area during field investigations. The
southeastern American kestrel (Falco sparverius paulus) was the only state listed species observed in the project area. The project is outside the core foraging areas of all known wood stork (Mycteria Americana) colonies. Suitable elevations and soils for sand skinks (Neoseps reynoldsi) occur in the project area; however, coordination with U.S. Fish and Wildlife Service concluded that habitat was highly isolated and relatively poor quality, so no cover-board surveys for sand skinks were necessary. A Natural Resources Evaluation Report is being prepared as part of the PD\&E study and will contain additional detail.

### 8.5 Public Lands and Recreational Section 4(F) Resources

There are no significant public lands or recreational Section 4(f) resources in the project area, so no impacts are anticipated.

### 8.6 Contamination

Information on contamination was obtained through interviews, observations during on-site visits and database information from the Florida Department of Environmental Protection (FDEP) and the United States Environmental Protection Agency. A total of ten sites were identified and reviewed for potential contamination risk. One site was assigned a risk rating of High, four sites were assigned a risk rating of Medium, and five sites were assigned a risk rating of Low. Level II Contamination Assessment investigations are recommended for any areas that have proposed dewatering or subsurface work activities occurring at or adjacent to any High- or Medium-Risk sites. A Contamination Screening Evaluation Report is being prepared as part of the PD\&E study and will have additional information.

### 8.7 Noise Sensitive Sites

Relatively few sensitive noise receptors are located in or around the project area. Multiple residences occur in a neighborhood immediately south of NW 49 ${ }^{\text {th }}$ Street. These houses are at least 1,200 feet from I-75. Some rural residences are located east of I-75 and the Baldwin Ranch occasionally hosts weddings on their property east of I-75. The FHWA assigned a summary degree of effect of Minimal regarding noise during the ETDM screening. No significant noise impacts are anticipated, and no fatal flaws have been identified.

### 8.8 Air Quality

Marion County is currently in attainment for all National Ambient Air Quality Standards and an such, no screening analysis or technical memorandum was conducted. No significant impacts are anticipated.

### 8.9 Farmland Soils

Approximately one quarter of the proposed project footprint occurs on Farmland Soils of Local Importance that are under active agricultural use. During the PD\&E study FDOT will coordinate with the Natural Resources Conservation Service to complete the USDA Farmland Conversion Impact Rating form (Form AD-1006) so that impacts can be scored, and alternatives developed as needed. No fatal flaws or significant impacts to farmland soils are anticipated.

### 8.10 Neighborhoods

Relatively few residences occur within the project area and one subdivision is located immediately south of NW 49 ${ }^{\text {th }}$ Street. The proposed project will have no direct impacts on neighborhoods or subdivisions. No significant impacts or fatal flaws related to disruption of neighborhoods are anticipated.

### 8.11 Floodplains

Each build alternative would impact the 100-Year and 500-Year floodplains, with the Parclo-NE alternative resulting in the greatest area of impacts followed by the Diamond Interchange. The SPUI, Parclo-SE and DDI alternatives are similar in the magnitude of floodplain impacts, and those impacts are considered minimal.

### 8.12 Conservation Lands

No conservation lands occur on or adjacent to the project area. No impacts to conservation lands are anticipated under any alternative.

### 8.13 Construction Impacts

Impacts from construction will be addressed by implementing Best Management Practices (BMPs) from FDOT Standard Specifications for Road and Bridge Construction. To minimize impacts to the eastern indigo snake, it is anticipated that the USFWS Standard Protection Measures for the Eastern Indigo Snake will also be implemented.

### 8.14 Environmental Impacts Conclusion

A review of the existing and historic conditions of the project area did not reveal any significant environmental impacts, fatal flaws or issues that are anticipated to significantly affect the acceptance of the proposed alternative.

## 9 Funding Plan \& Cost Estimates

### 9.1 Funding Plan

The proposed project is listed as the number one (1) priority project by the Ocala/Marion TPO. Funding has been allocated for future phases of the I-75 at NW 49 ${ }^{\text {th }}$ Street interchange project, including the PD\&E study, right of way, design and construction of both the new interchange and the NW 49 ${ }^{\text {th }}$ Street extension. Following is the funding source information; Tables 9-1 thru 9-3 are for I-75 (SR 93) at NW 49 ${ }^{\text {th }}$ Street from end of NW 49 ${ }^{\text {th }}$ Street to end of NW 35 ${ }^{\text {th }}$ Street and Table 9-4 is for NW $49^{\text {th }}$ Street Extension from NW 44 ${ }^{\text {th }}$ Avenue to NW $35^{\text {th }}$ Street.

Table 9-1: FDOT Five Year Work Program Funding for New Interchange

| Phase | 2021 | 2022 | 2023 | 2024 | 2025 | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Highways/PD \& E (On-Going) | \$15,990 |  |  |  |  | \$15,990 |
| Highways/Preliminary Engineering (On-Going) | \$373,968 |  |  |  |  | \$373,968 |
| Highways/Right of Way |  | \$10,200,000 |  |  |  | \$10,200,000 |
| Highways/Construction |  |  |  |  | \$47,774,814 | \$47,774,814 |
| Item Total: | \$389,958 | \$10,200,000 |  |  | \$47,774,814 | \$58,364,772 |

Source: FDOT FY 21-25 ADOPTED WORK PROGRAM as of 08/01/2020

Table 9-2: FDOT STIP Funding for New Interchange

| PHASE |  | < 2020 | 2020 | 2021 | 2022 | 2023 | > 2023 | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PD\&E | DDR | \$2,636,410 | \$0 | \$0 | \$0 | \$0 | \$0 | \$2,636,410 |
|  | DIH | \$76,526 | \$3,599 | \$0 | \$0 | \$0 | \$0 | \$80,125 |
| PE | DDR | \$0 | \$0 | \$0 | \$442,990 | \$0 | \$0 | \$442,990 |
|  | SL | \$0 | \$0 | \$0 | \$1,661,141 | \$0 | \$0 | \$1,661,141 |
|  | TOTAL: | \$2,712,936 | \$3,599 | \$0 | \$2,104,131 | \$0 | \$0 | \$4,820,666 |

Source: FDOT Office of Work Program STIP Report July/01/2019
DDR-District Dedicated Revenue; DIH-District In-House; SL-Surface Transportation Program, Population <=200K

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Table 9-3: Ocala Marion TPO Funding for New Interchange

| Phase | Funding <br> Category | Source | < 2020/21 | 2020/21 | 2021/22 | 2022/23 | 2023/24 | 2024/25 | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ROW | LF | Local | - | - | \$10,200,000 | - | - | - | \$10,200,000 |
| CST | SL | Federal | - | - | - | - | - | \$9,440,914 | \$9,440,914 |
| CST | LF | Local | - | - | - | - | - | \$8,419,861 | \$8,419,861 |
| CST | CIGP | State | - | - | - | - | - | \$8,522,752 | \$8,522,752 |
| CST | DDR | State | - | - | - | - | - | \$14,415,217 | \$14,415,217 |
| CST | DIH | State | - | - | - | - | - | \$114,400 | \$114,400 |
| CST | TRIP | State | - | - | - | - | - | \$4,696,516 | \$4,696,516 |
| CST | TRWR | State | - | - | - | - | - | \$3,407,729 | \$3,407,729 |
|  | Prior Costs |  | \$3,921,477 |  |  |  |  |  | \$3,921,477 |
| Total |  |  | \$3,921,477 | - | \$10,200,000 | - | - | \$49,017,389 | \$63,138,866 |

Source: 2020/21-2024/25 Transportation Improvement Program, Ocala Marion TPO
ROW-Right of Way; CST-Construction; LF-Local Funds; SL-Surface Transportation Program, Population <=200K; LF-Local Funds; CIGPCounty Incentive Grant Program; DDR-District Dedicated Revenue; DIH-District In-House; TRIP-Transportation Regional Incentive Program; TRWR-Wheels on the Road, TRIP

Table 9-4: Marion County TIP Funding for NW 49 ${ }^{\text {th }}$ Street /NW 35 ${ }^{\text {th }}$ Street Extension

| \# | NW 49 ${ }^{\text {th }}$ Street <br> Extension Segment | Description | Phase Code | Fund Code | 2020/21 | 2021/22 | 2022/23 | 2023/24 | 2024/25 | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C4 | Ph 2c <br> NW 44 ${ }^{\text {th }}$ Ave to North <br> End of Limerock Pit <br> (TIP073802) <br> (S128802) <br> (STC073802) | New 4LD w/ Interchange 0.9 mi | PE <br> DES <br> ROW-A <br> CST <br> CST <br> CST | ST ST IFW IFE GT2 | \$5,700,000 |  |  |  | $\begin{aligned} & \$ 2,209,931 \\ & \$ 3,609,931 \\ & \$ 2,600,000 \end{aligned}$ | $\begin{aligned} & \$ 5,700,000 \\ & \$ 2,209,931 \\ & \$ 3,609,931 \\ & \$ 2,600,000 \end{aligned}$ |
| C5 | Ph 3A 1.1 mi W of NW $44^{\text {th }}$ Ave to NW $44^{\text {th }}$ Ave (TIP60800F) | New 2 Lane 1.1 miles | $\begin{gathered} \text { DES } \\ \text { ROW-A } \\ \text { CST } \end{gathered}$ | GT2 <br> IFW <br> IFW | \$2,000,000 |  |  |  |  | \$2,000,000 |
| Total |  |  |  |  | \$7,700,000 |  |  |  | \$8,419,862 | \$16,119,862 |

Source: 2020/2021 -2024/2025 Marion County Transportation Improvement Program
ROW-Right of Way; CST-Construction; DES-Design; GT2-2 ${ }^{\text {nd }}$ Local Option Fuel Tax; IFW-Impact Fee-West; ST-Sales Tax

## Ocala/Marion TPO LRTP

The I-75 and NW 49 ${ }^{\text {th }}$ Street interchange is listed in the Adopted Ocala/Marion TPO 2040 LRTP Update Final Report. The new interchange is allocated funds of $\$ 20$ million by Year 2040.

## Current FDOT STIP

The current PD\&E Study and Preliminary Engineering for this project are included in the current
FDOT STIP (2021-2025) and Five-Year Work Programs in Years prior to 2020, 2020 and 2023.

Roadway Investments
As previously mentioned, the City of Ocala and Marion County have already constructed roadways that will facilitate development of Ocala 489. Under the original Master Development Agreement approved by the City, County, and the Ocala 489 development entity in August 2011, the County, agreed to spend an estimated $\$ 13.6$ million to four-lane NW $35{ }^{\text {th }}$ Street from US 441 (North Pine Avenue) to NW $35^{\text {th }}$ Avenue Road. Under that Master Agreement, the City agreed to spend an estimated $\$ 14.3$ million to build NW 35 ${ }^{\text {th }}$ Avenue Road north from US 27 (NW Blitchton Road) into the site and to provide water and sewer service. Both road construction projects, the City of Ocala's NW $35^{\text {th }}$ Avenue Road and Marion County's NW $35^{\text {th }}$ Street projects are now open to the public. The Ocala 489 development entity agreed to contribute $\$ 7$ million of right-of-way towards the NW $35^{\text {th }}$ Street and NW $35^{\text {th }}$ Avenue Road, road improvements and to build a $\$ 2.4$ million rail spur to tie into CSX Transportation's "S" line. In addition, Marion County has been actively pursuing all funding options, in the amount of over $\$ 25$ million to complete the engineering and design, right-of-way acquisition, and construction of the proposed I-75 and NW $49^{\text {th }}$ Street interchange and a new four-lane extension of NW $49^{\text {th }}$ Street.

### 9.2 Cost Estimates

Cost estimates were developed for all five Build alternatives. Table 9-5 summarizes the cost estimates for each Build alternative. The costs range from $\$ 35.7$ million for the DDI to $\$ 54.0$ million for the SPUI. Cost estimate details provided in Appendix L.

Table 9-5: Cost Estimates for I-75 at NW 49 ${ }^{\text {th }}$ Street Interchange Alternatives

| Component | DIAMOND | SPUI | PARCLO SE | PARCLO NE | DDI |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Earthwork | \$10,331,566 | \$9,771,170 | \$10,373,704 | \$10,070,665 | \$10,389,789 |
| Roadway | \$3,957,747 | \$3,572,395 | \$3,833,036 | \$3,753,752 | \$3,884,577 |
| Shoulder | \$1,439,665 | \$1,360,330 | \$1,362,560 | \$1,362,730 | \$1,501,680 |
| Median | \$371,895 | \$371,895 | \$311,650 | \$371,895 | \$405,765 |
| Drainage | \$2,209,963 | \$2,221,153 | \$2,328,294 | \$2,342,374 | \$2,326,928 |
| Signing | \$172,338 | \$140,867 | \$198,219 | \$189,896 | \$227,195 |
| Signalization | \$592,137 | \$592,112 | \$592,112 | \$592,121 | \$905,006 |
| Lighting | \$749,542 | \$730,621 | \$787,397 | \$692,739 | \$730,695 |
| Bridges | \$6,313,660 | \$19,961,675 | \$6,320,831 | \$6,254,844 | \$5,211,935 |
| SUBTOTAL | \$26,138,513 | \$38,722,217 | \$26,107,802 | \$25,631,016 | \$25,583,570 |
| MOT (10\%) | \$2,613,851 | \$3,872,222 | \$2,610,780 | \$2,563,102 | \$2,558,357 |
| Mobilization (10\%) | \$2,875,236 | \$4,259,444 | \$2,871,858 | \$2,819,412 | \$2,814,193 |
| SUBTOTAL | \$31,627,600 | \$46,853,883 | \$31,590,441 | \$31,013,529 | \$30,956,119 |
| Project Unknowns (15\%) | \$4,744,140 | \$7,028,082 | \$4,738,566 | \$4,652,029 | \$4,643,418 |
| Initial Contingency Amount | \$150,000 | \$150,000 | \$150,000 | \$150,000 | \$150,000 |
| TOTAL | \$36,521,740 | \$54,031,966 | \$36,479,007 | \$35,815,558 | \$35,749,537 |

## 10 Conclusions \& Recommendations

The operational analysis provided a performance evaluation for each individual element within the system (for example freeway segments, freeway ramp junctions, crossroad ramp terminals and other crossroad intersections). The analysis indicated that the proposed DDI is the recommended alternative and is not projected to have a significant adverse impact on operations along the I-75 mainline system or the existing adjacent interchanges within the study limits.

As indicated in this IJR, the recommended DDI alternative meets FHWA's Two Policy Requirements. The Interchange is justified as follows:

1. An operational and safety analysis has concluded that the proposed change in access does not have a significant adverse impact on the safety and operation of the interstate facility (which includes mainline lanes, existing, new or modified ramps, ramp intersections with crossroads) or on the local street network based on both the current and the planned future traffic projections. The analysis shall, particularly in urbanized areas, include at least the first adjacent existing or proposed interchange on either side of the proposed change in access (23 CFR 625.2(a), 655.603(d) and 771.111(f)). The crossroads and the local street network, to at least the first major intersection on either side of the proposed change in access, shall be included in this analysis to the extent necessary to fully evaluate the safety and operational impacts that the proposed change in access and other transportation improvements may have on the local street network (23 CFR 625.2(a) and 655.603(d)). Requests for a proposed change in access must include a description and assessment of the impacts and ability of the proposed changes to safely and efficiently collect, distribute and accommodate traffic on the interstate facility, ramps, intersection of ramps with crossroad and local street network (23 CFR 625.2(a) and 655.603(d)). Each request also must include a conceptual plan of the type and location of the signs proposed to support each design alternative (23 U.S.C. 109(d) and 23 CFR 655.603(d)).

A traffic operational analysis was conducted as part of this study. The analysis was performed for the AM and PM peak hours using the methodologies documented in the HCM 2010 as applied using the HCS 6.8, Synchro 10 and Vissim 2020.00-07.

Figures 10-1 and 10-2 present the segmented breakdown of the I-75 mainline and interchange ramps under the No Build and DDI alternatives; along with the summarized results for the 2045

AM segment and merge/diverge analysis. The differences between the No Build and DDI alternatives are as follow:

## o 2045 AM Northbound:

- No Build conditions
- I-75 south of US 27 including the off-ramp diverge operates at Level of Services (LOS) F and the basic segment between US 27 and SR 326, operates at LOS E.
- Build conditions
- Similar to No Build, I-75 south of US 27 operates at LOS F.
- Shifts in travel patterns reflect the use of I-75 as a by-pass between US 27 and NW 49 ${ }^{\text {th }}$ Street. Under No Build, for segment densities that are close to the LOS D maximum threshold of $35 \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$; the shift in traffic from improved connectivity corresponds to a minimal density increase, resulting in LOS E segments under Build.
- North of US 27 interchange through the NW 49 ${ }^{\text {th }}$ Street interchange, LOS are the same or better than under No Build.
- SR 326 diverge segment, the minimal increase in density is at the $35 \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ LOS D target threshold.


## o 2045 AM Southbound:

- No Build conditions
- I-75 south of US 27 including the on-ramp merge operates at LOS E.


## - Build conditions

- I-75 at the US 27 on-ramp merge condition; the traffic pattern shift from improved connectivity creates a slight increase in density where the LOS E threshold is exceeded.
- All remaining locations meet the LOS D target.

Figures 10-3 and 10-4 present the 2045 PM segment and merge/diverge analysis results for the No Build and DDI alternatives, respectively. Along with the directional peak change, the shifts in travel patterns, reflecting increases and decreases in traffic are similar to those observed for the AM.

Figure 10-1: No Build 2045 AM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 10-2: DDI Alternative 2045 AM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 10-3: No Build 2045 PM I-75 Segment \& Merge/Diverge Analysis Summary


Figure 10-4: DDI Alternative 2045 PM I-75 Segment \& Merge/Diverge Analysis Summary


The differences between the No Build and DDI alternatives under 2045 PM are as follow:
o 2045 PM Northbound:

- No Build conditions
- I-75 mainline segment south of US 27 operates at LOS E.
- All remaining locations meet the LOS D target.
- Build conditions
- For the US 27 off-ramp diverge; shift in travel pattern from improved connectivity corresponds to a minimal increase in density where the LOS D target threshold is exceeded at LOS E.
- The NW 49 ${ }^{\text {th }}$ Street on-ramp merge operates at LOS E; both adjacent mainline segments meet the LOS D target.
- Remaining northbound segments meet the LOS D target.


## o 2045 PM Southbound:

- No Build conditions
- I-75 on-ramp merge from US 27 and adjacent mainline segment operate at LOS F.
- I-75 segment between US 27 and SR 326 operates at LOS E.


## - Build conditions

- I-75 off-ramp diverge to US 27 and adjacent mainline segment, the ramp volume increase from improved connectivity creates a minor increase in density resulting in LOS E.
- Remaining southbound segments operate similar to No Build conditions.

As shown in the No Build segment and merge/diverge analysis results, the segments of I-75 between US 27 and SR 326 do not meet the LOS D target in year 2045 and are anticipated to operate at LOS E during either the AM or PM peak hours. The proposed interchange along NW $49^{\text {th }}$ Street is projected to meet the LOS D target; however, similar No Build I-75 segment operations (segments operating at LOS E) are also projected under build conditions. Therefore, a year of failure analysis was performed for the DDI alternative where I-75 segments reach LOS E in 2045. The analysis was conducted by interpolating volumes between years 2035 and 2045; then entering the volume for each year into HCS, until LOS E results were reached. Analysis results are summarized as follow:

## o AM Northbound:

- I-75 mainline segment south of US 27-2035
- I-75 mainline segment between US 27 and NW 49 ${ }^{\text {th }}$ Street - 2037
- NW 49 ${ }^{\text {th }}$ Street off-ramp diverge condition - 2041
- NW 49 ${ }^{\text {th }}$ Street on-ramp merge condition - 2044
- I-75 mainline segment between NW 49 ${ }^{\text {th }}$ Street and SR 326 - 2041


## o PM Southbound:

- I-75 south of US 27-2035
- I-75 mainline segment between SR 326 and NW $49^{\text {th }}$ Street -2041
- NW $49^{\text {th }}$ Street on-ramp merge condition -2045
- I-75 mainline segment between NW 49 ${ }^{\text {th }}$ Street and US $27-2037$

Based on the year of failure analysis, additional I-75 mainline improvements may be required in order for I-75 to meet the LOS D target through design year. The analysis also shows that the proposed DDI at the NW 49 ${ }^{\text {th }}$ Street interchange will not have a significant adverse impact on operations along the I-75 mainline system or the existing adjacent interchanges within the study limits, when compared to No Build conditions; therefore, meeting this FHWA policy requirement. To address identified mainline deficiencies, the District is looking into potential improvements via separate projects or other methods such as the I-75 PD\&E Study (FM Number 443623-1-2201 \& 443624-1-22-01) to improve overall operations on the I-75 mainline. The results and recommendations of this IJR will be shared with the I-75 PD\&E Study team and District Traffic Operations group.

Table 10-1 presents the 2045 No Build and DDI alternative intersection delay and LOS during the AM and PM peak hours. Under No Build conditions, none of the signalized intersections meet the LOS D target except for the intersection of I-75 northbound ramps at US 27; however, the northbound off-ramp approach fails.

For Build conditions, the only signalized intersections within the AOI operating at the LOS D Target or better are the US 27 northbound ramps and the SR 326 northbound ramps intersections. The shift in traffic patterns from improved connectivity is expected to reduce total ramp volumes at both existing interchanges (US 27 and SR 326) by approximately 1,000 vehicles per day under the build condition. Although not meeting the LOS D Target for some intersections, during the AM peak hour, all intersection delays are reduced when compared to No Build conditions. During the PM peak hour, delays are decreased at all but three intersections. The difference in overall intersection delay, compared to No Build is not significant at the three intersections.

Table 10-1: 2045 No Build \& DDI Alternative Intersection Delay and LOS

| \# | Intersection | DIR | No Build |  |  |  |  |  | Build DDI |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM |  |  | PM |  |  | AM |  |  |  | PM |  |  |  |
|  |  |  | App. Delay ${ }^{2}$ LOS |  | Int. <br> Delay $^{2}$ LOS | $\begin{gathered} \text { App. } \\ \text { Delay }^{2} \text { LOS } \end{gathered}$ |  | $\begin{gathered} \text { Int. } \\ \text { Delay }^{2} \text { LOS } \end{gathered}$ | $\begin{gathered} \text { App. } \\ \text { Delay }^{2} \text { LOS } \end{gathered}$ |  | Int. <br> Delay $^{2}$ LOS |  | App. <br> Delay ${ }^{2}$ LOS |  | Int. <br> Delay ${ }^{2}$ LOS |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | NW 44 Ave at US 27 | EB <br> WB <br> NB <br> SB | $\begin{array}{r} 151.8 \\ 34.4 \\ 64.2 \\ 51.5 \end{array}$ |  | 89.5 F | $\begin{array}{r} 54.3 \\ 153.7 \\ 66.2 \\ 50.5 \end{array}$ | $\begin{gathered} \mathrm{D} \\ \mathrm{~F} \\ \mathrm{E} \\ \mathrm{D} \end{gathered}$ | 105.1 F | 111.1 <br> 33.0 <br> 49.7 <br> 45.9 | $\begin{aligned} & \mathrm{F} \\ & \mathrm{C} \\ & \mathrm{D} \\ & \mathrm{D} \end{aligned}$ | 70.5 | E | $\begin{gathered} 39.0 \\ 171.5 \\ 60.4 \\ 48.3 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ \mathrm{~F} \\ \mathrm{E} \\ \mathrm{D} \end{gathered}$ | 111.1 | F |
| 2 | $\begin{aligned} & \mathrm{I}-75 \mathrm{SB} \\ & \text { at US } 27 \end{aligned}$ | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { SB } \end{gathered}$ | $\begin{array}{r} 142.4 \\ 73.3 \\ 59.6 \end{array}$ | $\begin{gathered} \mathrm{F} \\ \mathrm{E} \\ \mathrm{E} \end{gathered}$ | 108.3 F | $\begin{aligned} & 77.5 \\ & 63.7 \\ & 59.2 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{E} \\ & \mathrm{E} \end{aligned}$ | 68.8 E | $\begin{aligned} & 90.5 \\ & 21.4 \\ & 50.7 \end{aligned}$ | $\begin{aligned} & \text { F } \\ & \text { C } \\ & \text { D } \end{aligned}$ | 57.6 | E | $\begin{aligned} & 62.2 \\ & 53.7 \\ & 97.9 \end{aligned}$ | E <br> D <br> F | 58.5 | E |
| 3 | $\begin{aligned} & \text { I-75 NB } \\ & \text { at US } 27 \end{aligned}$ | EB <br> WB <br> NB | $\begin{array}{r} 6.7 \\ 21.8 \\ 60.8 \end{array}$ | A <br> C <br> E | 25.4 C | $\begin{array}{r} 1.2 \\ 36.3 \\ 119.6 \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{D} \\ & \mathrm{~F} \end{aligned}$ | 46.2 D | $\begin{gathered} 2.2 \\ 19.4 \\ 33.7 \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { B } \\ & \text { C } \end{aligned}$ | 15.5 | B | $\begin{gathered} 1.5 \\ 45.4 \\ 77.3 \end{gathered}$ | A <br> D <br> E | 39.6 | D |
| 4 | NW 35 Ave Rd at US 27 | $\begin{gathered} \text { EB } \\ \mathrm{WB} \\ \mathrm{NB} \\ \mathrm{SB} \end{gathered}$ | $\begin{array}{r} 66.5 \\ 69.0 \\ 57.4 \\ 415.1 \end{array}$ | $\begin{gathered} \mathrm{E} \\ \mathrm{E} \\ \mathrm{E} \\ \mathrm{~F} \end{gathered}$ | 125.6 F | $\begin{array}{r} 101.1 \\ 178.3 \\ 54.8 \\ 463.0 \end{array}$ | $\begin{gathered} \text { F } \\ \text { F } \\ \text { D } \\ \text { F } \end{gathered}$ | 199.2 F | $\begin{gathered} 49.0 \\ 60.6 \\ 55.0 \\ 397.8 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ \mathrm{E} \\ \mathrm{E} \\ \mathrm{~F} \end{gathered}$ | 112.7 | F | 99.6 193.5 55.0 517.8 | $\begin{aligned} & F \\ & F \\ & D \\ & \text { F } \end{aligned}$ | 218.1 | F |
| 5 | NW 44 Ave at NW 49 ST | $\begin{gathered} \mathrm{EB} \\ \mathrm{WB} \\ \mathrm{NB} \\ \mathrm{SB} \end{gathered}$ | $\begin{array}{r} 61.6 \\ 81.6 \\ 208.6 \\ 37.7 \end{array}$ | $\mathrm{E}$ F F D | 96.8 F | $\begin{array}{r} 64.7 \\ 159.6 \\ 64.9 \\ 25.3 \end{array}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{~F} \\ & \mathrm{E} \\ & \mathrm{C} \end{aligned}$ | 88.4 F | $\begin{aligned} & 43.0 \\ & 36.1 \\ & 25.0 \\ & 27.2 \end{aligned}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{D} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 30.1 | C | $\begin{aligned} & 42.6 \\ & 33.2 \\ & 21.8 \\ & 27.2 \end{aligned}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \hline \end{aligned}$ | 28.4 | C |
| 6 | NW 44 Ave/ I-75 SB Off at SR 326 | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \end{gathered}$ | $\begin{array}{r} 22.7 \\ 47.6 \\ 111.5 \\ 116.3 \end{array}$ | C <br> D <br> F <br> F | 68.6 E | $\begin{array}{r} 25.6 \\ 43.2 \\ 145.5 \\ 96.8 \end{array}$ | $\begin{aligned} & C \\ & D \\ & \text { F } \\ & \text { F } \end{aligned}$ | 74.2 E | $\begin{aligned} & 15.8 \\ & 15.9 \\ & 28.3 \\ & 24.2 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~B} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 19.4 | B | $\begin{aligned} & 19.8 \\ & 20.5 \\ & 32.7 \\ & 31.5 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 24.9 | C |
| 7 | $\begin{aligned} & \text { I-75 SB On- } \\ & \text { Ramp (Loop) } \\ & \text { at SR } 326 \\ & \text { Unsignalized } \end{aligned}$ | EB <br> WB <br> NB | $\begin{array}{r} 0.0 \\ 17.1 \\ 15 \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 10.4 B | $\begin{array}{r} 0.0 \\ 2.2 \\ 14.7 \end{array}$ | $\begin{gathered} \text { A } \\ \text { A } \\ \text { B } \end{gathered}$ | 1.5 A | $\begin{gathered} 0.0 \\ 6.5 \\ 13.6 \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { A } \\ \text { B } \end{gathered}$ | 4.4 | A | $\begin{gathered} 0.0 \\ 1.5 \\ 12.6 \end{gathered}$ | A <br> A <br> B | 1.2 | A |
| 8 | $\begin{aligned} & \text { I- } 75 \text { NB Off/ } \\ & \text { I75 NB On } \\ & \text { at SR } 326^{1} \end{aligned}$ | EB <br> WB <br> NB | $\begin{array}{r} 45.7 \\ 329.8 \\ 851.8 \end{array}$ | D <br> F <br> F | 418.3 F | $\begin{array}{r} 95.7 \\ 395.6 \\ 409.4 \end{array}$ | $\begin{aligned} & \mathrm{F} \\ & \mathrm{~F} \\ & \mathrm{~F} \end{aligned}$ | 332.0 F | $\begin{gathered} 13.9 \\ 251.1 \\ 774.4 \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \mathrm{~F} \\ \mathrm{~F} \end{gathered}$ | 365.7 | F | $\begin{gathered} 57.8 \\ 431.3 \\ 431.2 \end{gathered}$ | $\mathrm{E}$ F F | 367.2 | F |
| 9 | $\begin{gathered} 175 \mathrm{SB} \\ \text { at NW } 49 \mathrm{ST}^{1} \end{gathered}$ | $\begin{gathered} \text { SBR } \\ \text { SBL } \\ \text { EBT } \\ \text { WBT } \end{gathered}$ |  |  |  |  |  |  | 21.4 <br> 34.8 <br> 18.2 $13.8$ | $\begin{gathered} \mathrm{C} \\ \mathrm{C} \\ \text { B } \\ \text { B } \end{gathered}$ | 18.2 | B | $\begin{gathered} 20.8 \\ 28.3 \\ 9.9 \\ 18.4 \end{gathered}$ | C C A B | 17.3 | B |
| 10 | $\begin{aligned} & 175 \text { NB } \\ & \text { at NW } 49 \text { ST }^{1} \end{aligned}$ | $\begin{gathered} \text { NBL } \\ \text { NBR } \\ \text { EBT } \\ \text { WBT } \end{gathered}$ |  |  |  |  |  |  | 32.4 <br> 16.3 <br> 13.6 <br> 18.6 | $\begin{aligned} & \text { C } \\ & \text { B } \\ & \text { B } \\ & \text { B } \end{aligned}$ | 20.5 | B | $\begin{gathered} 30.1 \\ 19.3 \\ 7.3 \\ 20.2 \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ \mathrm{~B} \\ \mathrm{~A} \\ \mathrm{C} \end{gathered}$ | 19.3 | B |

[^10]Table 10-2 summarizes the network performance from the Vissim analysis. The benefits of the build alternative are visibly higher during the AM peak period. During the PM peak period, the benefits are not as significant due to the higher demand volumes, which results in higher congestion on I-75 southbound at the US 27 interchange. Overall, all performance measures show improvement under the DDI alternative compared to No Build. Network statistic improvements are as follow:

## - AM Peak

o Total Delay: Reduced by $37 \%$
o Total Stops: Reduced by 47\%
o Average Speed: Increased by 3 mph
o Vehicles Arrived: Increased by 1,188 vehicles
o VMT: Increase by 15,464 miles
o Latent Delay: Reduced by 387 hours
o Latent Demand: Reduced by 1,697 hours

- PM Peak
o Total Delay: Reduced by 15\%
o Total Stops: Reduced by 25\%
o Average Speed: Increased by 2 mph
o Vehicles Arrived: Increased by 1,466 vehicles
o VMT: Increase by 16,387 miles
o Latent Delay: Reduced by 51 hours
o Latent Demand: Reduced by 217 hours

Table 10-2 2045 Vissim Network Performance Summary

| Peak Hour | $\begin{aligned} & 15-\mathrm{min} \\ & \text { Period } \end{aligned}$ | No Build |  |  |  |  |  |  | DDI |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | VehicleMiles Traveled | Latent Delay (Hours) | Latent Demand (Vehicles) | $\begin{aligned} & \hline \text { Total } \\ & \text { Delay } \\ & \text { (Hours) } \\ & \hline \end{aligned}$ | Total Stops | Average Speed (mph) | Vehicles Arrived (Vehicles) | VehicleMiles Traveled | Latent Delay (Hours) | Latent Demand (Vehicles) |
| AM | 1 | 21 | 1,980 | 58 | 2,854 | 13,513 | 0 | 0 | 24 | 2,152 | 56 | 2,874 | 14,262 | 0 | 0 |
|  | 2 | 33 | 3,034 | 56 | 3,558 | 16,829 | 0 | 0 | 36 | 3,142 | 55 | 3,565 | 17,796 | 0 | 0 |
|  | 3 | 43 | 3,981 | 55 | 4,048 | 18,965 | 0 | 1 | 46 | 4,026 | 54 | 4,081 | 19,997 | 0 | 1 |
|  | 4 | 53 | 5,095 | 54 | 4,283 | 20,027 | 0 | 1 | 53 | 4,666 | 54 | 4,359 | 21,230 | 0 | 1 |
|  | 5 | 93 | 9,964 | 50 | 4,667 | 22,275 | 0 | 3 | 83 | 7,802 | 51 | 4,746 | 23,652 | 1 | 5 |
|  | 6 | 165 | 18,817 | 44 | 4,878 | 22,897 | 9 | 97 | 127 | 13,118 | 47 | 5,087 | 24,632 | 3 | 19 |
|  | 7 | 215 | 24,529 | 40 | 4,832 | 22,799 | 47 | 293 | 166 | 17,774 | 44 | 5,032 | 24,507 | 14 | 109 |
|  | 8 | 211 | 23,218 | 39 | 4,694 | 21,326 | 75 | 326 | 160 | 17,568 | 43 | 4,797 | 22,682 | 22 | 89 |
|  | 9 | 187 | 20,770 | 40 | 4,496 | 20,691 | 84 | 347 | 133 | 14,654 | 45 | 4,602 | 22,012 | 21 | 79 |
|  | 10 | 182 | 20,154 | 41 | 4,507 | 20,757 | 91 | 382 | 116 | 12,211 | 47 | 4,630 | 22,262 | 19 | 74 |
|  | 11 | 178 | 19,332 | 42 | 4,574 | 21,335 | 100 | 403 | 106 | 10,502 | 48 | 4,692 | 22,650 | 19 | 76 |
|  | 12 | 176 | 20,012 | 41 | 4,393 | 19,981 | 97 | 357 | 89 | 8,646 | 49 | 4,507 | 21,177 | 17 | 60 |
|  | Total ${ }^{1}$ | 1,557 | 170,886 | 46 | 51,784 | 241,395 | 503 | 2,210 | 1,139 | 116,261 | 49 | 52,972 | 256,859 | 116 | 513 |
| PM | 1 | 78 | 6,781 | 51 | 4,465 | 20,171 | 0 | 2 | 85 | 6,904 | 50 | 4,545 | 21,429 | 1 | 9 |
|  | 2 | 88 | 7,486 | 49 | 4,428 | 19,854 | 4 | 20 | 89 | 6,701 | 49 | 4,553 | 21,113 | 7 | 29 |
|  | 3 | 113 | 9,992 | 47 | 4,572 | 21,238 | 12 | 73 | 108 | 8,479 | 48 | 4,672 | 22,600 | 21 | 127 |
|  | 4 | 137 | 12,609 | 45 | 4,739 | 21,598 | 37 | 183 | 123 | 9,860 | 47 | 4,892 | 23,030 | 50 | 239 |
|  | 5 | 158 | 16,407 | 43 | 4,748 | 21,700 | 67 | 330 | 135 | 11,555 | 46 | 4,870 | 23,210 | 79 | 374 |
|  | 6 | 175 | 17,801 | 42 | 4,724 | 21,355 | 105 | 474 | 146 | 13,453 | 44 | 4,901 | 22,797 | 112 | 499 |
|  | 7 | 198 | 20,597 | 41 | 4,759 | 22,182 | 151 | 717 | 160 | 15,527 | 44 | 4,911 | 23,637 | 153 | 702 |
|  | 8 | 221 | 24,377 | 39 | 4,839 | 22,198 | 217 | 971 | 184 | 19,593 | 42 | 4,985 | 23,932 | 206 | 902 |
|  | 9 | 236 | 26,684 | 38 | 4,797 | 21,984 | 275 | 1,199 | 211 | 23,172 | 40 | 4,912 | 23,441 | 255 | 1,110 |
|  | 10 | 222 | 25,246 | 38 | 4,620 | 20,428 | 316 | 1,282 | 191 | 21,240 | 40 | 4,794 | 21,733 | 293 | 1,190 |
|  | 11 | 176 | 19,134 | 40 | 4,429 | 19,423 | 327 | 1,310 | 144 | 14,620 | 43 | 4,504 | 20,576 | 302 | 1,201 |
|  | 12 | 134 | 13,881 | 43 | 4,152 | 18,122 | 326 | 1,255 | 106 | 9,755 | 46 | 4,199 | 19,142 | 307 | 1,217 |
|  | Total ${ }^{1}$ | 1,936 | 200,995 | 43 | 55,272 | 250,253 | 1,837 | 7,816 | 1,682 | 160,859 | 45 | 56,738 | 266,640 | 1,786 | 7,599 |

A predictive crash analysis was conducted to compare predicted crashes of the No Build and the five Build alternatives. The analysis was conducted for future conditions utilizing the predictive methods set forth in the HSM Parts C and D. A summary of the predicted number of annual crashes for the project site (interchange alternatives) is provided in Table 10-3 and for the AOI in Table 10-4. The predicted number of annual crashes for the interchange alternatives range from 96.3 crashes per year for the DDI alternative, the best in regard to safety; to 108.0 crashes per year for the Diamond alternative, ranking the worst. In addition, the project AOI shows a net reduction in total crashes from 321.9 crashes under No Build to 317.2 crashes under Build conditions. It should be noted that compared to No Build, Build AADT values are higher; which inherently increases predicted crashes, even when the same scenario is maintained.

Table 10-3: Project Site Predicted 2045 Annual Crashes

| Location | DIAMOND |  |  | SPUI |  |  | ParClo SE |  |  | ParClo NE |  |  | DDI |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total | FI | PDO | Total |
| 1-75 (N of US 27 to NW 49 ${ }^{\text {th }}$ Street to $S$ of SR 326) | 19.4 | 48.5 | 67.8 | 19.8 | 49.9 | 69.7 | 17.6 | 44.3 | 61.8 | 18.5 | 46.8 | 65.3 | 19.4 | 48.5 | 67.8 |
| I-75 \& NW 49 ${ }^{\text {th }}$ Street Interchange ${ }^{1}$ | 11.9 | 25.3 | 37.2 | 8.0 | 22.2 | 30.1 | 12.9 | 26.6 | 39.5 | 10.2 | 19.2 | 29.4 | 8.0 | 17.5 | 25.5 |
| NW 49 ${ }^{\text {th }}$ Street, NW 44 ${ }^{\text {th }}$ Avenue to I-75 | 0.1 | 0.2 | 0.3 | 0.1 | 0.3 | 0.4 | 0.1 | 0.2 | 0.3 | 0.1 | 0.2 | 0.3 | 0.1 | 0.2 | 0.3 |
| NW 49 ${ }^{\text {th }}$ Street, East of I-75 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 | 0.2 | 0.5 | 0.7 |
| NW 44 ${ }^{\text {th }}$ Avenue at NW 49 ${ }^{\text {th }}$ Street | 0.7 | 1.3 | 2.0 | 0.7 | 1.3 | 2.0 | 0.7 | 1.3 | 2.0 | 0.6 | 1.3 | 1.9 | 0.7 | 1.3 | 2.0 |
| TOTALS | 32.2 | 75.8 | 108.0 | 28.7 | 74.2 | 102.9 | 31.4 | 72.9 | 104.3 | 29.6 | 68.1 | 97.7 | 28.3 | 68.0 | 96.3 |

${ }^{1}$ Merge/Diverge/Ramps/Ramp Termini
Table 10-4: AOI Cumulative Predicted 2045 Annual Crash Summary

| Location | FI | PDO | NO BUILD | FI | PDO | BUILD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I-75 (S of US 27-N Ramps \& S Ramps-N of SR 326) | 18.5 | 48.1 | 66.6 | 19.4 | 51.0 | 70.3 |
| I-75 \& US 27 Interchange ${ }^{1}$ | 28.2 | 39.9 | 68.0 | 27.1 | 38.4 | 65.5 |
| I-75 \& SR 326 Interchange ${ }^{1}$ | 41.2 | 76.6 | 117.7 | 40.2 | 77.4 | 117.7 |
| US 27 (Arterial \& Intersections) | 13.5 | 28.4 | 41.8 | 12.8 | 27.0 | 39.8 |
| SR 326 (Arterial \& Intersections) | 4.7 | 12.0 | 16.7 | 4.6 | 11.8 | 16.4 |
| NW 44 ${ }^{\text {th }}$ Avenue AOI ( N \& S of NW 49 ${ }^{\text {th }} \mathbf{~ S t}$ ) | 3.0 | 8.0 | 11.0 | 2.0 | 5.4 | 7.4 |
| TOTALS | 109.0 | 212.9 | 321.9 | 106.1 | 211.0 | 317.2 |

${ }^{1}$ Merge/Diverge/Ramps/Ramp Termini

The proposed interchange ramp gores would be located at a minimum of 0.87 miles away from the US 27 ramp gores and a minimum of 0.90 miles away from the SR 326 ramp gores; and do not create weaving segments.
2. The proposed access connects to a public road only and will provide for all traffic movements. Less than "full interchanges" may be considered on a case-by-case basis for
applications requiring special access for managed lanes (e.g., transit, HOVs, HOT lanes) or park and ride lots. The proposed access will be designed to meet or exceed current standards (23 CFR 625.2(a), 625.4(a)(2), and 655.603(d)).

The new interchange will be designed to meet or exceed current FDOT Design Standards and will serve all traffic movements. The interchange will connect to the extension of NW 49th Street. This roadway project is currently under design, with funding for construction in 2024/25; it will conform to FDOT Design Standards and will be a public roadway.

Marion County and the City of Ocala have already constructed public roadways that will facilitate access to the proposed interchange. Specifically, the four-laning of NW $35^{\text {th }}$ Street from US 441 (North Pine Avenue) to NW $35^{\text {th }}$ Avenue Road and the four-lane construction of NW $35^{\text {th }}$ Avenue Road north from US 27 (NW Blitchton Road) to intersect with the NW $35^{\text {th }}$ Street project.

In summary, the I-75 and NW 49 ${ }^{\text {th }}$ Street interchange is currently listed as the number one (1) priority project in the Ocala/Marion TPO adopted FY 2025 Priority Projects. In addition, the PD\&E Study and Preliminary Design for this project is included in the current FDOT Five Year (20212025) Work Program in Years prior to 2020, 2020 and 2023, respectively.

The DDI alternative provides the highest performing operations and lowest predicted number of crashes when compared to the other Build alternatives. In terms of environmental, socioeconomic, cost, and other engineering factors, the DDI alternative ranked first in the alternative evaluation matrix. Based on the aforementioned, the DDI alternative is the recommended interchange configuration for I-75 at NW 49 ${ }^{\text {th }}$ Street. Recommended storage lengths are provided in Table 10-5. It should be noted that recommended storage lengths do not include deceleration and taper lengths. Additional storage is also suggested to accommodate the heavy truck traffic that is anticipated at the proposed interchange to support the industrial/commercial Ocala 489 commerce park. A Conceptual signing plan for the recommended DDI alternative is provided in Appendix M.

For maximum operational efficiency, it is recommended to integrate the proposed interchange into the surrounding existing and planned TSM\&O network as identified in the Marion County TSM\&O Master Plan and the FDOT F.R.A.M.E. project (FM Number 440900-1). In addition to inclusion of the recommended interchange into the TSM\&O network, the recommended DDI alternative is also being designed to accommodate future improvements should the need arise. Finally, based on the year of failure analysis, additional I-75 mainline improvements may be
required in order for I-75 to meet the LOS D target through design year. As previously mentioned, the District is looking into potential improvements to the I-75 mainline via separate projects or other methods such as the I-75 PD\&E Study (FM Number 443623-1-22-01 \& 443624-1-22-01) to improve overall operations on the I-75 mainline. The results and recommendations of this IJR will be shared with the I-75 PD\&E Study team and District Traffic Operations group.

Table 10-5: 2045 Recommended Turn Lane Storage Lengths

| Interchange | Ramps | Movement | Turn Bay Length ${ }^{1}$ (ft) | 95th Percentile Queue Length ${ }^{2}$ ( ft ) |  | Vissim Max Queue Length (ft) |  | Recommended <br> Storage <br> Length ${ }^{3}$ (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | AM | PM | AM | PM |  |
| DDI | I-75 NB | WBR | 250 | 40 | 37 | 4 | 0 | 50 |
|  |  | NBL | - | 0 | 0 | 228 | 256 | 275 |
|  | I-75 SB | EBR | 300 | 24 | 13 | 201 | 265 | 275 |
|  |  | SBL | - | 0 | 0 | 166 | 207 | 225 |

${ }^{1}$ Turn Bay Length used in traffic analysis; Turn Bay Length = Storage + Deceleration + Taper Lengths
${ }^{2}$ Queue length from Synchro Analysis
${ }^{3}$ Recommended Storage Length does not include Deceleration+ Taper Lengths.


[^0]:    ${ }^{1}$ LOS results based on HCM 2000 methodology; ${ }^{2}$ Delay in sec/veh

[^1]:    ${ }^{1}$ Turn Bay Length used in traffic analysis; Turn Bay Length = Storage + Deceleration + Taper Lengths
    ${ }^{2}$ Queue length from Synchro Analysis
    ${ }^{3}$ Recommended Storage Length does not include Deceleration+ Taper Lengths.

[^2]:    ${ }^{1}$ Florida Traffic Online (2017/2018); 2013 -2017 TRAFFIC COUNTS \& TRENDS MANUAL, OCALA/MARION COUNTY TPO
    ${ }^{2}$ Machine count varied significantly with FDOT Historical AADT Report
    ${ }^{3}$ AADT from TMCs (see TMC2AADT); used for locations between interchange ramps or if closest AADT deemed unreasonable

[^3]:    ${ }^{1}$ passenger car equivalent based on 25 ft /veh (queue/25 ft)

[^4]:    'Volume in vph; delay in sec/veh; LOS is Estimated LOS using HCM2010 thresholds; Queue Lengths in feet

[^5]:    This space is intentionally left blank

[^6]:    AVERAGE SPEED DIFFERENCE (mph)
    Diff.: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph Upper: $70<65 \quad<60<55<50<45$ Lower: $65 \quad 60 \quad 55 \quad 50 \quad 45 \quad 0$

[^7]:    AVERAGE SPEED DIFFERENCE (mph)
    Diff:: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph Upper: $70<65 \quad<60<55<50<45$ $\begin{array}{lllllll}\text { Lower: } & 65 & 60 & 55 & 50 & 45 & 0\end{array}$ (Posted Speed-Avg. Speed)

[^8]:    AVERAGE SPEED DIFFERENCE (mph
    Diff.: 5 mph 10 mph 15 mph 20 mph 25 mph 30 mph Upper: $70<65<60<55<50<45$ $\begin{array}{lllllll}\text { Lower: } & 65 & 60 & 55 & 50 & 45 & 0\end{array}$ (Posted Speed-Avg. Speed)

[^9]:    *Property Damage Only

[^10]:    ${ }^{1}$ LOS results based on HCM 2000 methodology; ${ }^{2}$ Delay in sec/veh

