## Final

## Location Hydraulic Report

SR 514 (Malabar Road) PD\&E Study<br>From Babcock Road to US 1

Brevard County

Financial Project ID: 43013612201
ETDM Project Number: 13026

The environmental review, consultation, and other actions required by applicable federal environmental laws for this project are being, or have been, carried out by the Florida Department of Transportation (FDOT) pursuant to 23 U.S.C. $\S 327$ and a Memorandum of Understanding (MOU) dated December 14, 2016 and executed by the Federal Highway Administration (FHWA) and FDOT.

April 2018


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The Florida Department of Transportation (FDOT), District Five, conducted a Project Development and Environment (PD\&E) Study to evaluate improvements to Malabar Road [State Road (SR) 514] in Brevard County, Florida. The study limits begin east of Babcock Street (SR 507) [milepost (MP) 3.102] and extend to US 1 (MP 6.742), a distance of 3.64 miles. The purpose of the study was to provide documented environmental and engineering analyses to determine the type, location, and conceptual design of roadway improvements to Malabar Road (SR 514). The PD\&E Study Class of Action is a State Environmental Impact Report (SEIR) since no federal funds are anticipated for any phases of this project.

The purpose of this Location Hydraulic Report (LHR) was to address base floodplain encroachments resulting from the roadway improvements. The report was prepared in accordance with FDOT's PD\&E Manual, Part 2, Chapter 24 including the Minimal Encroachment Checklist for the Federal Emergency Management Agency (FEMA) Maps. This analysis ensures that all base floodplains are identified and provides recommendations regarding minimization and elimination of floodplain impacts. As a result of this process, a preliminary determination of impact was made as to the level of significance of the encroachment.

There are 5 crossdrain locations along the project limits within the 100-year (base) floodplain. The widened roadway, with extended or replaced cross drains, will result in transverse impacts with minimal floodplain encroachments. This project will not result in any new or increased adverse environmental impacts. There will not be a significant change in the potential interruption or termination of emergency service or emergency evacuation routes. The FDOT drainage design standards as well as the SJRWMD procedures will be applied during the design phase to prevent increasing flood elevations or changing floodplain limits. Typical for a roadway that traverses the floodplain, any potential impacts will be mitigated by the increased capacity of the cross culverts with no rise in the flood stages and with the storage capacity gained by the construction of new treatment ponds where no storage exists today.

It should be noted that all elevations discussed in this document are in reference to North America Vertical Datum 1988 (NAVD'88). The conversion between NAVD'88 and National Geodetic Vertical Datum 1929 (NGVD'29) at this location is NGVD'29 is equal to NAVD'88 plus 1.38 feet. For example, elevation 20 in this report is equal to elevation 21.38 NGVD'29.

### 1.0 PROJECT DESCRIPTION

Malabar Road (SR 514) is an east-west urban minor arterial located in Brevard County that begins approximately 7.4 miles west of its interchange with I-95 and continues east to US 1, traversing the City of Palm Bay and the Town of Malabar. East of Babcock Street, the Malabar Road is primarily a two-lane, undivided rural roadway. There are two signalized intersections within the project limits: at Babcock Street (SR 507) and at US 1. Land use within the corridor includes commercial, conservation, recreation, and lowdensity residential development. The Florida Division of Emergency Management has designated Malabar Road (SR 514) as an evacuation route. There is also a Florida East Coast (FEC) rail crossing approximately 600 feet west of US 1.

The PD\&E Study analyzed alternatives for widening SR 514, Malabar Road from a two-lane to a four-lane facility from Babcock Street to US 1. This project corridor traverses the City of Palm Bay and the Town of Malabar. The west end of the project falls within the limits of the City of Palm Bay and within the boundary of the local water control district, Melbourne-Tillman Water Control District or MTWCD. Palm Bay Community Hospital and large sections of conservation lands are located along the north side of the road. Single-family residences, the Florida East Coast Railroad, and light commercial developments can be found in the Town of Malabar at the east end of the project.

The proposed improvements will include the addition of sidewalks and bike lanes, and water quality treatment within new project ponds. The roadway typical section will vary along the project corridor and will include both urban and rural drainage features. The project limits are depicted on the following location map and aerial exhibit - Figures 1 and 2.

### 2.0 EXISTING DRAINAGE CONDITIONS

The USGS maps show the project alignment surrounded by a broad, low-lying, partially wooded area interspersed with irregularly-shaped drainage ways and swamps. The existing topography is comprised of level terrain with elevations varying from 17 ft to 19 ft NAVD, and slightly higher elevations near the western end of the alignment and also near a few isolated knolls and ridges on the eastern end.

The offsite area south of the roadway generally drains north. The western two-thirds of the project are within the drainage basin for Turkey Creek. Five ditches and the MTWCD C-78 Canal cross under the SR 514 alignment and combine as branches of Turkey Creek. The side ditches along the north and south edge of SR 514 drain towards these flowage ways and, in some locations, through smaller sized crossdrains that function as equalizer pipes. To the west of Marie Street, the drainage pattern is eastward through an FDOT ditch easement under the railroad and into Indian River. FDOT owns and maintains a section of drainage easement north of several of the crossdrains.

The C-78 Canal is maintained by MTWCD. The SR 514 ditches are regularly maintained by FDOT. However, the various branches of Turkey Creek upstream of SR 514 are overgrown and not well maintained. During major rainfall events like Tropical Storm Fay, the area experiences flooding on the local roads and surrounding properties. This flooding was most noted at the east side of the conservation lands that drain
through offsite wetlands with ill-defined outfalls. The city and county have recently completed maintenance upgrades within the roadside ditches and the overall drainage conditions have improved.

Camp Road maintenance yard for FDOT was contacted regarding historic flooding problems for the project corridor. FDOT reported they have recently cleared the drainage easement downstream of the culvert near Eva Lane in order to solve a local flooding concern. Based upon interviews, overtopping of portions of the project corridor was noted during Tropical Storm Fay.

Runoff from SR 514 is collected in roadside swales and conveyed to cross culverts serving the ditches that pass through the area. The flat terrain of the roadway and surrounding area creates conditions where culvert.

flow interconnects with the adjacent cross culvert and the limit of each basin is not distinctively defined. The offsite basins contributing to the crossdrains are also loosely delineated. There are linear ditches throughout the offsite areas and interconnecting ditches that follow the local roads. During flood events, flow is anticipated to overtop basin boundaries interconnecting several of the delineated basins. Figure 3 shows the location of the existing culverts along the project corridor. Figure 4 presents the drainage basins upstream of the project for each of the crossdrains and delineates the floodplain boundaries in the vicinity of the project.

It should be noted that the basin divides are based upon limited data available for the PD\&E Study. In establishing the basin divides, significant differences were noted when previous studies were compared to each other. These differences emphasize the preliminary nature of the culvert analysis and the details needed during the design phase.

Three issues concerning the offsite basins are noted here. Culvert \#2 is an $8^{\prime} \times 4^{\prime}$ box culvert for the MTWCD C-78 Canal. On historical basin maps for MTWCD, the upstream basin area is defined by the boundary limits of the water control district. However, field review south of Malabar Road showed a changed ditch network near Atz Road and it is possible that a much larger basin area drains to the C-78 Canal. This shifts basin area that would have otherwise drained to Culvert \#3. To account for this situation, Figure 4 lists two drainage basin acreage values for Culvert \#2 and Culvert \#3. A conservative approach was suggested by FDOT District Five. The assumption for this LHR analysis was to use the largest basin area for both culverts. A discussion was held with MTWCD. They were not aware of the circumstances behind the field conditions and suggested the system could change in the future. In addition, during a discussion with the City of Palm Bay, they reported a concern that the flowline of the existing MTWCD culvert is set too high. They request that FDOT revisit the flowline condition during the design phase of this project. MTWCD also provided a flow estimate obtained from the regional hydraulic model of their canal system. However, MTWCD limits the allowable runoff rate from the lands within the district. For example, the $25-\mathrm{yr}$ flow is restricted to $0.08 \mathrm{cfs} / \mathrm{acre}$ and the 100-yr flow is restricted to $0.10 \mathrm{cfs} / \mathrm{acre}$. These allowable rates are significantly less than discharge values generated from regression or rational formulas and typically would not be used for FDOT design.

A second concern stems from review of the published Flood Insurance Study (FIS) for the Turkey Creek floodplain. Table 4 of the FIS, titled Summary of Discharges, lists drainage areas for each branch of Turkey Creek. Several of the drainage areas in the FIS do not match well with the offsite drainage basin map established for this project. For example, the drainage areas for Channel C and for Channel G are both listed as 1.1 square miles at the point the branch connects into the main section of Turkey Creek. However, the size of Culvert \#6 (which drains Channel G) is 30-inches and the size of Culvert \#7 (which drains Channel C) is $8^{\prime} \times 4^{\prime}$. Since the basin areas for these two culverts are different, it appears the FIS oversimplified this parameter by comingling of the flow for each basin.

The third issue about the ill-defined drainage basins has already been mentioned. The drainage basin divides are often drawn across linear ditches where the prevailing flow direction is unclear. For example, the southern basin limits of Turkey Creek have ditches that continue into Goat Creek Basin. The network of ditches throughout the offsite area continues to change through time. When a section of land is developed, it is typical to create a small borrow pond to raise the grade on portion of the developed property. It appears the swales through the area are either improved by the site work for better conveyance or in some cases the swale was eliminated.



### 2.1 CROSSDRAINS

Refer to Figure 3. There are fourteen (14) existing crossdrains under SR 514, six (6) of which serve as crossings for the Turkey Creek Branches or the MTWCD C-78 Canal. Within the project limits, other smaller culverts act as equalizer pipes for the roadside ditches. Most of the fourteen culverts were extended as part of a 1998 roadway project that widened the shoulders of SR 514. Given the limited right-of-way, lateral pipe connections were added to the extended culverts to convey flow from the side ditches. Figure 5 presents the detail of the culvert extensions and the lateral connections. Information about the existing crossdrains within the project limits is presented in the two tables that follow.


Table 1 - Existing Crossdrains

| Cross <br> Drain ID | Location | Size | Length | No. Barrels | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $117+44$ | 24 -inch | $58^{\prime}$ | 1 | Conc. Pipe $^{(\mathbf{1})}$ |
| 2 | $125+05$ | $8^{\prime} \times 4^{\prime}$ | $62^{\prime}$ | 1 | Conc. Box Culvert |
| 3 | $143+20$ | $10^{\prime} \times 3^{\prime}$ | $96^{\prime}$ | 1 | Conc. Box Culvert |
| 4 | $149+80$ | 24 -inch | $48^{\prime}$ | 1 | Conc. pipe |
| 5 | $165+70$ | $(2) 8^{\prime} \times 3^{\prime}$ | $62^{\prime}$ | 2 | Conc. Box Culvert |
| 6 | $171+65$ | 30 -inch | $42^{\prime}$ | 1 | Conc. pipe |
| 7 | $178+60$ | $8^{\prime} \times 4^{\prime}$ | $54^{\prime}$ | 1 | Conc. Box Culvert |
| 8 | $190+24$ | 24 -inch | $42^{\prime}$ | 1 | Conc. pipe |
| 9 | $201+70$ | $10^{\prime} \times 5^{\prime}$ | $67^{\prime}$ | 1 | Conc. Box Culvert |
| 10 | $232+30$ | 24 -inch | $42^{\prime}$ | 1 | Conc. pipe |
| 11 | $250+92$ | 24 -inch | $46^{\prime}$ | 1 | Conc. pipe |
| 12 | $256+96$ | 24 -inch | $46^{\prime}$ | 1 | Conc. pipe |
| 13 | $270+35$ | 24 -inch | $36^{\prime}$ | 1 | Conc. pipe |
| 14 | $282+05$ | 18 -inch | $36^{\prime}$ | 1 | Conc. Pipe ${ }^{(\mathbf{1 )}}$ |

[^0]Table 2 - Existing Crossdrain Parameters

| Crossdrain ID | Flowlines (S. to N.) | FEMA Flood Stage (NAVD'88) | Water Mark Elev. | Comments/Condition |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 20.4 / 20.4 | -- | -- |  |
| 2 | 17.08 /17.02 | -- | $19.02 \text { (54-in }$ <br> from headwall top) | MTWCD C-78 Canal, connects to Turkey Creek via C-76 |
| 3 | 15.59 / 15.43 | Approx. 19.1 | $17.93 \text { (42-in }$ <br> from headwall top) | Channel E of Turkey Creek FDOT R/W downstream |
| 4 | 15.74 / 15.68 | -- | -- |  |
| 5 | 12.08 / 12.14 | Approx. 16.0 | 14.4 (39-in from headwall top) | Channel D of Turkey Creek |
| 6 | 14.55 / 14.36 | Approx. 18.1 | $16.11 \text { (18-in }$ <br> below crown) | Channel G of Turkey Creek |
| 7 | 14.02 / 14.17 | Approx. 17.9 | 17.5 (6-in below crown) | Channel C of Turkey Creek FDOT R/W downstream |
| 8 | 17.05 / 17.02 | -- | -- |  |
| 9 | 12.94 / 12.79 | Approx. 17 | 16.3 (47-in from headwall top) | Channel B of Turkey Creek FDOT R/W downstream |
| 10 | 18.34 / 18.45 | -- | $\begin{gathered} 19.53 \text { (2-in } \\ \text { above crown) } \end{gathered}$ |  |
| 11 | 19.94 / 18.77 | -- | $21.48 \text { (11-in }$ <br> below crown) | FDOT R/W downstream |
| 12 | 19.33 / 19.36 | -- | $21.33 \text { (At }$ crown) |  |
| 13 | 16.8 / 16.8 | -- | -- |  |
| 14 | 19.0 / 19.0 | -- | -- |  |

Notes:
1- There are several stormsewer pipes that run from the south side of Malabar Road to the north side that were constructed as part of the intersection improvements at Babcock Street. These pipe segments continue towards Babcock Street, then north and into the existing FDOT pond in the northeast corner of the intersection. One of these stormsewer pipes connected to Babcock Street drainage (Crossdrain \#1) is located where the road transitions back to two lanes (east of Enterprise Road).

### 2.2 FLOODPLAINS

Refer to Figure 4. Malabar Road traverses five branches of Turkey Creek, each with established flood profiles immediately downstream, i.e., north of the roadway. SR 514 also traverses MTWCD C-78 Canal, which connects to the floodplain at its confluence with the C-76 canal. Flood Insurance Rate Maps (FIRM) for Brevard County dated August 18, 1992, with Map Numbers 12009C0540F and 12009C0605E, cover the project limits. These maps show a defined floodway that begins at the mouth of Turkey Creek and ends just downstream of SR 514. The maps also show "Flood Zone A - No Base Flood Elevations Determined" generally confined to the area at the creeks. The creek crossings under SR 514 are not in the floodway.

There was a recent update to the FIS for Brevard County. For the Turkey Creek Basin, the notable change with this revision was the conversion to NAVD'88 datum for the listed flood stages. The update was considered "Preliminary" at the beginning of this study, but the new maps have recently been adopted with an effective date of March 17, 2014. Excerpts of the new FIS for Brevard County covering the project area, along with FIRM Maps (Numbers 12009C0613G, 12009C0614G, 12009C0677G, and 12009C0680G) are included in Appendix A.

The proposed culverts will not increase flood stages. The FDOT drainage design standards as well as SJRWMD procedures will be applied during the design phase to prevent increasing flood elevations or changing floodplain limits. As such, all anticipated floodplain encroachments are expected to be minimal. Floodplain compensation ponds are not typically required for linear projects that transverse a floodplain. Preliminary conversation with SJRWMD indicated their agreement; i.e., this project is similar to others, where hydraulicequivalent crossdrains and the new treatment ponds for the corridor will suffice for any floodplain impact. This approach was also discussed with the Brevard County FEMA coordinator, Frank Karvelis, who confirmed that floodplain compensation would not be required for the proposed conditions along Malabar Road.

### 3.0 FUTURE DRAINAGE CONDITIONS

The existing drainage boundaries and local drainage patterns will be maintained in the proposed condition. Water quality treatment will be achieved with new stormwater ponds. The stormwater runoff from SR 514 will be conveyed to the proposed ponds by closed stormsewer systems before discharging to the outfall points. There are locations where drainage from adjacent properties will be collected along with the roadway runoff and conveyed through the proposed ponds. However, according to House Bill 599, no additional treatment is required for these offsite areas. Therefore, the pond size estimates in the Pond Siting Report only considers water quality and attenuation for the onsite project area.

For the roadway widening, existing crossdrains will need to be replaced with greater or hydraulically equivalent structures. Backwater surface elevations are not expected to increase when FDOT guidelines are followed during the design phase. As a result, the project will not affect existing flood stages or floodplain limits.

Preliminary estimates of the replacement culverts have been established as part of this LHR. These culvert sizes are based upon limited available information for the offsite drainage basins and their respective runoff estimates. During the design phase of the project, these crossdrains will require a complete hydrologic and
hydraulic study. Table 3 presents anticipated crossdrain parameters for the widening project. Backup calculations are presented within Appendix B.

Table 3 - Proposed Crossdrains

| Cross <br> Drain ID | Location | Size | Length | No. Barrels | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 117+44 | 30 -inch | 112' | 1 | Conc. Pipe ${ }^{(1)}$ |
| 2 | 125+05 | (2) $6^{\prime} \times 4^{\prime}$ | 126' | 2 | Conc. Box Culvert |
| 3 | 143+20 | (2) $8^{\prime} \times 4^{\prime}$ | 126' | 2 | Conc. Box Culvert |
| 4 | 149+80 | 30 -inch | 112' | 1 | Conc. pipe |
| 5 | 165+70 | (2) $8^{\prime} \times 4^{\prime}$ | 160' | 2 | Conc. Box Culvert |
| 6 | 171+65 | (2) 30 -inch | 152' | 2 | Conc. pipe |
| 7 | 178+60 | (2) $6^{\prime} \times 4^{\prime}$ | 162' | 2 | Conc. Box Culvert |
| 8 | 190+24 | (2) 36 -inch | 148' | 2 | Conc. pipe |
| 9 | 201+70 | 10'x5' | 190 | 1 | Conc. Box Culvert |
| 10 | 232+30 | 30 -inch | $74^{\prime}$ | 1 | Conc. pipe |
| 11 | 250+92 | 24 -inch | $70^{\prime}$ | 1 | Conc. pipe |
| 12 | 256+96 | 30 -inch | $86^{\prime}$ | 1 | Conc. pipe |
| 13 | 270+35 | 36 -inch | $60^{\prime}$ | 1 | Conc. Pipe ${ }^{(1)}$ |
| 14 | 282+05 | 24 -inch | $60^{\prime}$ | 1 | Conc. Pipe ${ }^{(1)}$ |

${ }^{(1)}$ Stormsewer conveyance pipe

### 4.0 CONCLUSION

There is no change in flood "Risk" associated with this project. The proposed floodplain encroachments are classified as "minimal".

The proposed structures will perform hydraulically in a manner equal to or greater than the existing structures, and backwater surfaces are not expected to increase. The widened roadway, with extended cross drains, will result in transverse impacts with minimal floodplain encroachments. As a result, the project will not affect existing flood heights or floodplain limits. This project will not result in any new or increased adverse environmental impacts. There will not be a significant change in the potential interruption or termination of emergency service or emergency evacuation routes.

It has been determined, through consultation with local, state, and federal water resources and floodplain management agencies that there is no regulatory floodway involvement on the proposed project and that the project will not support base floodplain development that is incompatible with existing floodplain management programs

## APPENDIX A

## FEMA MAPS AND FIS

- UPDATED EFFECTIVE FIS MARCH 17, 2014






| Community Name | Community <br> Number |
| :--- | :---: |
| BREVARD COUNTY <br> (UNINCORPORATED AREAS) | 125092 |
| CAPE CANAVERAL PORT AUTHORITY | 120619 |
| CAPE CANAVERAL, CITY OF | 125094 |
| COCOA , CITY OF | 120020 |
| COCOA BEACH, CITY OF | 125097 |
| GRANT-VALKARIA, TOWN OF | 120224 |
| INDIALANTIC, TOWN OF | 125115 |
| INDIAN HARBOUR BEACH, CITY OF | 125116 |
| MALABAR, TOWN OF | 120024 |
| MELBOURNE BEACH, TOWN OF | 125128 |
| MELBOURNE VILLAGE, TOWN OF | 120329 |
| MELBOURNE, CITY OF | 120025 |
| PALM BAY, CITY OF | 120404 |
| PALM SHORES, TOWN OF | 120612 |
| ROCKLEDGE, CITY OF | 120027 |
| SATELLITE BEACH, CITY OF | 120028 |
| TITUSVILLE, CITY OF | 125152 |
| WEST MELBOURNE, CITY OF | 120335 |



## NOTICE TO

## FLOOD INSURANCE STUDY USERS

Communities participating in the National Flood Insurance Program have established repositories of flood hazard data for floodplain management and flood insurance purposes. This Flood Insurance Study may not contain all data available within the repository. It is advisable to contact the community repository for any additional data.

This preliminary Flood Insurance Study contains profiles presented at a reduced scale to minimize reproduction costs. All profiles will be included and printed at full scale in the final published report.

Part or all of this Flood Insurance Study may be revised and republished at any time. In addition, part of this Flood Insurance Study may be revised by the Letter of Map Revision process, which does not involve republication or redistribution of the Flood Insurance Study. It is, therefore, the responsibility of the user to consult with community officials and to check the community repository to obtain the most current Flood Insurance Study components. A listing of the Community Map Repositories can be found on the Index Map.

Initial Countywide FIS Effective Date: April 3, 1989
First Countywide FIS Revision Date: August 18, 1992 (Flood Insurance Rate Map Only)
Second Countywide FIS Revision Date: November 19, 1997
Third Countywide FIS Revision Date: <to be determined>

## FLOOD INSURANCE STUDY

## BREVARD COUNTY, FLORIDA AND INCORPORATED AREAS

### 1.0 INTRODUCTION

1.1 Purpose of Study

This Flood Insurance Study (FIS) revises and updates information on the existence and severity of flood hazards in the geographic area of Brevard County, including the Cities of Cape Canaveral, Cocoa, Cocoa Beach, Indian Harbour Beach, Melbourne, Palm Bay, Rockledge, Satellite Beach, Titusville, and West Melbourne; the Towns of GrantValkaria, Indialantic, Malabar, Melbourne Beach, Melbourne Village, and Palm Shores; the Cape Canaveral Port Authority; and the unincorporated areas of Brevard County (referred to collectively herein as Brevard County), and aids in the administration of the National Flood Insurance Act of 1968 and the Flood Disaster Protection Act of 1973. This study has developed flood-risk data for various areas of the community that will be used to establish actuarial flood insurance rates and to assist the community in its efforts to promote sound floodplain management. Minimum floodplain management requirements for participation in the National Flood Insurance Program (NFIP) are set forth in the Code of Federal Regulations at 44 CFR, 60.3.

In some States or communities, floodplain management criteria or regulations may exist that are more restrictive or comprehensive than the minimum Federal requirements. In such cases, the more restrictive criteria take precedence, and the State (or other jurisdictional agency) will be able to explain them.

### 1.2 Authority and Acknowledgments

The sources of authority for this FIS report are the National Flood Insurance Act of 1968 and the Flood Disaster Protection Act of 1973.

The original April 3, 1989 countywide FIS was prepared to include all jurisdictions within Brevard County into a countywide format FIS. Information on the authority and acknowledgements for each jurisdiction with a previously printed FIS report included in this countywide FIS is shown below.

For the original April 3, 1989, countywide FIS, the coastal analysis for the open coast of the Atlantic Ocean was prepared by Greenhorne \& O'Mara, Inc., under contract to FEMA. The analysis included wave setup, wave runup, dune erosion, and wave heights. The hydrologic and hydraulic analyses were performed by Gee \& Jenson, Inc., for FEMA, under Contract No. EMW-84-C-1609. That work was completed in December 1986 (Reference 1).

For the November 19, 1997, revision, the floodway for Otter Creek was added from
the City of Melbourne FIS (Reference 2) to correct the omission of this data during the preparation of the original countywide FIS for Brevard County. In support of this revision, profiles for Otter Creek and Horse Creek were added (Reference 3).

For this revision of the countywide FIS report, new hydrologic and hydraulic analyses were performed by the Watershed IV Alliance for the Federal Emergency Management Agency (FEMA), under Contract No. EMA-2002-CO-011A, Task Order No. 022B. This study was completed in January 2011. Various ponding areas within the North Merrit Island area of Brevard County were included in these analyses.

The topographic information consisted of 10 meter Digital Elevation Models produced by the U.S. Geological Survey (USGS) (Reference 2). Planimetric base map information shown on all FIRM panels was derived from multiple sources. Road centerlines, stream centerlines and political boundary files were provided by Brevard County and Florida Division of Emergency Management, and St. John's River Water Management District, and additional stream centerlines were downloaded from the National Hydrography Dataset provided by the USGS (Reference 3). Users of this FIRM should be aware that minor adjustments may have been made to specific base map features.

Base map information shown on this FIRM was provided in digital format by Brevard County and the Florida Division of Emergency management. The ortho photography is dated 2009.

The coordinate system used for the production of this FIRM is Transverse Mercator State Plane Florida East FIPS 0901, North American Datum of 1983 (NAD 83) HARN, GRS 80 spheroid. Differences in the datum and spheroid used in the production of FIRMs for adjacent counties may result in slight positional differences in map features at the county boundaries. These differences do not affect the accuracy of information shown on the FIRM.

### 1.3 Coordination

An initial Consultation Coordination Officer (CCO) meeting (also occasionally referred to as the Scoping meeting) is held with representatives of the communities, FEMA, and the study contractors to explain the nature and purpose of the FIS and to identify the streams to be studied by detailed methods. A final CCO (often referred to as the Preliminary DFIRM Community Coordination, or PDCC, meeting) is held with representatives of the communities, FEMA, and the study contractors to review the results of the study.

For the original April 3, 1989, FIS report, an initial CCO meeting was held in April 1984 and a final CCO meeting was held on May 9, 1988. Both meetings were attended by representatives of the county, Gee \& Jenson, Inc., and FEMA. Coordination with community officials and Federal, state, and regional agencies produced various information pertaining to floodplain regulations, available maps and topography, flood history, and other hydrographic data. Agencies contacted for information included the National Ocean Service, Tide and Water Levels Division and Data Control Section; the Melbourne-Tillman Water Control District; the Florida Institute of Technology; the

Florida Department of Natural Resources (FDNR), Division of Beaches and Shores; the Harbor Branch Foundation; the Press Journal and Today Newspapers; the Florida East Coast Railway; the U.S. Army Corps of Engineers (USACE), Jacksonville District; the St. John's River Water Management District; the U.S. Soil Conservation Service (now the Natural Resources Conservation Service); the U.S. Geological Survey (USGS); the Florida Department of Transportation (FDOT); and the Florida Department of Environmental Regulation.

For the November 19, 1997, revision, the county was notified by FEMA in a letter dated August 7, 1995, that flood hazard information from the City of Melbourne FIS was being incorporated into the countywide FIS.

For this revision of the countywide FIS, the initial CCO meeting was held on August 29, 2008, and attended by representatives of FEMA, the Watershed IV Alliance, community officials, Canaveral Port Authority, the State of Florida, and various consulting firms.

The results of the study were reviewed at the final CCO meeting held on $\qquad$ ,
and attended by representatives of . All
problems raised at that meeting have been addressed in this study.

### 2.0 AREA STUDIED

2.1 Scope of Study

This FIS report covers the geographic area of Brevard County, Florida, including the incorporated communities listed in Section 1.1.

For this revision, 17.5 square miles of new ponding areas within the North Merrit Island area were studied using detailed methods. Floodplain boundaries of Coastal AE areas, streams and ponding areas that had been previously studied by detailed methods were redelineated based on more detailed and up-to-date topographic data. Coastal VE zones were remapped based on the new Primary Frontal Dune (PFD) location, according to FEMA's 2007 Guidance for Atlantic and Gulf Coasts of the United States. All other coastal zone breaks were digitized from the previous effective maps and remain unchanged due to the datum shift not being at a whole foot interval. Re-running the effective coastal model for overland analysis was not included in the scope of work for this study. In addition, the lack of accurate transect location information would not have resulted in a desirable outcome. Redelineated coastal and ponding areas within the county are now shown to the tenth of a foot on the FIRM panels to reflect the datum conversion from National Geodetic Vertical Datum of 1929 (NGVD29) to North American Vertical Datum of 1988 (NAVD).

For the 1997 revision, a detailed coastal flooding analysis was performed on the complete coastline of Brevard County, where the flooding sources are the Atlantic Ocean, the Indian and Banana Rivers, Mosquito Lagoon, and New Found Harbour. Also, detailed analyses for Horse Creek and Otter Creek within the City of Melbourne were incorporated. The Melbourne-Tillman Canal, Horse Creek, Otter Creek, several lakes and
ponds in Cocoa, Channel F in Palm Bay, and Sloughs A, B, and C in Rockledge were not restudied for the 1997 revision but previous information for those streams was used in that study.

For the original 1989 countywide FIS report, the following flooding sources were studied by detailed methods: the Eau Gallie River; Crane Creek, including Channel A and Channel B; Turkey Creek, including the main channel and Channels A, B, C, D, E, and G and C-76; Goat, Kid, Trout, North and South Prong Creeks; and ponding in and around the City of Titusville.

The areas studied by detailed methods were selected with priority given to all known flood hazards and areas of projected development or proposed construction. "Flooding Sources Studied by Detailed Methods" are presented in Table 1.

Table 1: Flooding Sources Studied by Detailed Methods

| Flooding Source | Reach Length (miles) | Study Area |
| :---: | :---: | :---: |
| Atlantic Ocean | 70.0 | Brevard County Coastline |
| Channel F | 1.4 | From approximately 200 feet downstream of Dowse Court to Norwood Street |
| Crane Creek | 4.6 | From its confluence with Indian River to Evans Road |
| Crane Creek Channel A | 1.1 | From its confluence with Crane Creek to approximately 440 feet upstream of Rialto Place |
| Crane Creek Channel B | 0.9 | From its confluence with Crane Creek to approximately 300 feet upstream of Spring Oak Drive |
| Crane Creek Diversion | 2.8 | From John Rodes Boulevard to Evans Road |
| Eau Gallie River | 4.1 | From confluence with Indian River to a point approximately 240 feet downstream of Aurora Drive |
| Elbow Creek | 0.9 | From the confluence with Eau Gallie River to a point approximately 1,400 feet upstream of Laurie Street |
| Goat Creek | 3.5 | From the confluence with Indian River to a point approximately 3,450 feet upstream of Leghorn Road |
| Horse Creek | 1.2 | From confluence with Indian River to approximately 1,600 feet upstream of Croton Road |

Table 1: Flooding Sources Studied by Detailed Methods (continued)

| Flooding Source | Reach Length (miles) | Study Area |
| :---: | :---: | :---: |
| Kid Creek | 1.0 | From the confluence with Indian River to approximately 3,375 feet upstream of William Avenue |
| Melbourne Tillman Canal | 7.2 | From the confluence with Melbourne Tillman Canal Tributary 1 to the confluence with Turkey Creek Channel C |
| North Prong Creek | 2.2 | From the confluence with Sebastian Creek to a point approximately 50 feet upstream of Wilden Road |
| Otter Creek | 0.7 | From approximately 400 feet downstream of Robin Hood Drive to a point approximately 1,450 feet upstream of Sherwood Boulevard |
| Sebastian Creek | 1.4 | From the confluence with Sebastian Creek Tributary 3 to the confluence with Sebastian River |
| South Prong Creek | 2.6 | From the confluence with Indian River to the County boundary |
| St. John's River | 83.5 | From the Volusia/Seminole County boundary to the Brevard/Indian River County boundary |
| Trout Creek | 1.3 | From confluence with Indian River to Grant Road |
| Turkey Creek | 2.8 | From the confluence with Indian River to approximately 450 feet upstream of the divergence of the Melbourne Tillman Canal |
| Turkey Creek Channel A | 2.0 | From confluence with Turkey Creek to approximately 525 feet downstream of Babcock Street |
| Turkey Creek Channel B | 1.3 | From confluence with Turkey Creek to approximately 110 feet downstream of Malabar Road |
| Turkey Creek Channel C | 1.1 | From confluence with Turkey Creek to Malabar Road |
| Turkey Creek Channel C-76 | 1.9 | From confluence with Turkey Creek Channel D to a point approximately 1,400 feet upstream of Charles Boulevard |
| Turkey Creek Channel D | 0.7 | From the confluence with Turkey Creek Channel C to Malabar Road |
| Turkey Creek Channel E | 0.3 | From confluence with Turkey Creek Channel D to approximately 100 feet downstream of Malabar Road |

Table 1: Flooding Sources Studied by Detailed Methods (continued)

| Flooding Source | Reach <br> Length <br> (miles) | Study Area |
| :---: | :---: | :--- |
| Turkey Creek <br> Channel G | 0.6 | From the confluence with Turkey Creek Channel <br> C to a point approximately 150 feet downstream of <br> Malabar Road |
| Various Zone AE <br> Ponds* | 1.4 sq. <br> mi. | North - State Route 528, East -Clearlake Road, <br> South - Pluckebaum Road, West - St. John's River <br> Basin |
| Various Zone AE <br> Ponds | 3.9 sq. <br> mi. | East of I-95, South of La Flor Drive, North of <br> Wickham Road, and West of US-1 |
| Various Zone AH <br> Ponds | 1.5 sq. <br> mi. | Countywide |

* Flooding source with new or revised analysis incorporated as part of the current study update

Numerous streams were studied by approximate methods, as indicated in Table 2, "Flooding Sources Studied by Approximate Methods." Approximate analyses were used to study those areas having a low development potential or minimal flood hazards. The scope and methods of study were proposed to, and agreed upon, by FEMA and the Watershed Alliance IV. All the approximate zones for streams and ponding areas in this table were refined and re-established for this revision to the countywide FIS report.

## Table 2: Flooding Sources Studied by Approximate Methods

| Addison Creek | Jane Green Creek | Spoil Bank |
| :--- | :--- | :--- |
| Ellis Creek | Kid Creek | Ten Mile Creek |
| Eau Gallie River <br> Tributary 5 | North Prong | Trout Creek |
| Eau Gallie River <br> Tributary 7 | Otter Creek | Wolf Creek |
| Goat Creek | Sebastian Creek | Various Unnamed Streams |
| Horse Creek | Sixmile Creek | Various Unnamed Ponding |

Mapping for Brevard County, Florida, and incorporated areas has been prepared using digital data. Previously published FIRM and Flood Boundary and Floodway Map data produced manually have been converted to vector digital data by a digitizing process.

This countywide FIS also incorporates the determination of letters issued by FEMA, resulting in Letters of Map Revision as shown in Table 3, "Letters of Map Revision."

Table 3: Letters of Map Revision

| Case Number | Flooding Source(s) | Communities Affected | Effective <br> Date |
| :---: | :---: | :---: | :---: |
| 00-04-277P | Ponding Areas 1-5 | Brevard County <br> City of Rockledge | $2 / 16 / 2001$ |
| $05-04-3609 \mathrm{P}$ | N/A | Brevard County | $9 / 26 / 2005$ |
| $11-04-2906 \mathrm{P}$ | Atlantic Ocean | Brevard County | $2 / 28 / 2011$ |

### 2.2 Community Description

Brevard County is located near the middle of the east coast of Florida along the Atlantic Ocean. The county is bordered on the north by Volusia County; on the east by the Atlantic Ocean; on the south by Indian River County, Florida; on the southwest by Osceola County, Florida; on the west by Orange County, Florida; and on the northwest by Seminole County. The county encompasses an area of 1,557 square miles which includes 539 square miles of water (primarily the Atlantic Ocean, the St. John’s River, and the Indian River Lagoon).

Brevard County has a mild, subtropical climate, with average temperatures in the City of Titusville ranging from 60.5 degrees Fahrenheit ( ${ }^{\circ} \mathrm{F}$ ) in January to $80.2{ }^{\circ} \mathrm{F}$ in August (Reference 4). The wet season extends from June through November with September as the wettest month, averaging 7.83 inches of rainfall. Average annual rainfall is approximately 57 inches. Prevailing winds are from the southeast and east in the spring and summer and from the northeast in the fall. Brevard County is less frequently impacted by direct hurricane landfalls than portions of the Panhandle or South Florida because the hurricanes are often steered northwest and offshore or they weaken to a tropical storm.

The topography of Brevard County is divided into three major features: the barrier islands; the coastal ridge, which forms the eastern boundary of the mainland; and the low and marshy St. John's River Valley, which includes all of the area west of the coastal ridge. Elevations along the coastal areas vary from approximately 6 feet North American Vertical Datum of 1988 (NAVD) on Merritt Island to elevations over 20 feet NAVD along the mainland ridge, dropping to approximately 14 feet NAVD at Titusville (Reference 5). Elevations along the barrier island dunes reach 15 to 20 feet NAVD.

The primary north-south transportation arteries serving Brevard County are U.S. Route 1 and Interstate 95. State Roads 3, 5, 9, 46, 50, 192, 402, 515, 520, 524, and 528 serve the inland portions of the county and connect to Florida's Turnpike and Interstate 4. Other transportation arteries include the Florida East Coast Railway, which parallels the mainland coast, and the Intracoastal Waterway within the Indian River and Mosquito Lagoon.

The year 2010 population of Brevard County was reported as 543,376 (Reference 6). The population for the county grew by $107.1 \%$ in the last three decades of the 1900 s.

Residential, commercial, and industrial development in Brevard County occurs mainly along the coastal barrier islands and the western shore of the Indian River, east of Interstate 95. Areas west of Interstate 95 are generally undeveloped or agricultural, although the City of Palm Bay is experiencing significant development. In 2007 retail trade was the largest of 20 major economic sectors in Brevard County.

The county seat of Brevard County is the City of Titusville, which is located along the Indian River on the coastal ridge approximately 40 miles east of the City of Orlando, Florida. The year 2006 population for Titusville was estimated as 44,027 (Reference 6). Population figures for other communities discussed here are based on the year 2000. The communities of Cocoa (population 16,412), Rockledge (population 20,170), Palm Shores (population 794), Melbourne (population 71,382), Melbourne Village (706), West Melbourne (population 9,824), Palm Bay $(79,413$ ), and Malabar (population 2,622) are distributed between Interstate 95 and U.S. Route 1 on the coastal ridge south of Titusville. The John F. Kennedy Space Center and the Cape Canaveral Air Force Base are located east of Titusville on Merritt Island and the adjacent barrier islands. The communities of Cape Canaveral (population 8,829), Cocoa Beach (population 12,482), Satellite Beach (population 9,577), Indian Harbour Beach (population 8,152), Indialantic $(2,944)$, and Melbourne Beach $(3,335)$ are located on the barrier islands south of Merritt Island. The Canaveral Port Authority is an independent governmental agency created by the Florida Legislature that has jurisdiction over all fiscal and regulatory policies and operation of the Port, which is in the community of Cape Canaveral.

The northwestern boundary of Brevard County is the St. John's River. The St. John's River is the largest river in Florida, with a basin of approximately 9,430 square miles measured at its discharge into the Atlantic Ocean near the City of Jacksonville. From its headwaters in Indian River County to the south, the St. John's River flows northward through Brevard County and into Volusia County. Several small tributaries, including Jane Green Creek, Ten Mile Creek, Wolf Creek, and Sixmile Creek, are included in this study.

The eastern edge of Brevard County contains the waterways of the Indian River Lagoon. This 156-mile long estuary lies between the mainland and barrier islands from Volusia County to the north, through Brevard County, and extending south to Palm Beach County. The Atlantic Intracoastal Waterway runs through the Indian River Lagoon for its length. Five inlets allow for exchange of fresh and saltwater in the lagoon. In Brevard County, the Indian River Lagoon begins as Mosquito Lagoon in the north, picks up the Banana River on the east side of Merritt Island, and continues as the Indian River south of Merritt Island, encountering Sebastian Inlet at the southern boundary of Brevard County. Other small streams, such as the Eau Gallie River and Turkey, Crane, Goat, Kid, Trout, and Sebastian Creeks (and the North and South Prongs) drain the coastal highland areas and discharge into the Indian River.

### 2.3 Principal Flood Problems

Floods resulting from prolonged, heavy rainfall can occur in streams that drain the coastal highland areas and discharge into the Indian and St. John's Rivers. Flooding from
heavy rainfall occurs in lowland areas and streams including the Eau Gallie River, Crane Creek, Crane Creek Channels A and B, Turkey Creek, Turkey Creek Channels A, B, C, D, E, F, G, and C-76, and Goat, Kid, Trout, and North and South Prong Creeks, and their respective tributaries. In the Cocoa West area, new residential and light industrial development has flooded in areas that are shown as outside the Special Flood Hazard Areas. Repeated flooding has also been reported in areas around North Titusville and Mims.

Coastal areas of the county on the Atlantic Ocean are subject to storm surge flooding as a result of hurricane and tropical storm activity. Large tidal surges, combined with wave action and the heavy rainfall that accompanies the storms, have caused flooding. Areas along the Banana and Indian Rivers and Mosquito Lagoon experience flooding from wind tides caused by hurricane winds piling water against shorelines and various causeways and bridges over the rivers. North Merritt Island has had repeated flooding since the last major FIS revision.

There is considerable historical evidence of storms affecting the southeastern coast of the United States before the 20th century (Reference 7). Some of the most significant 20th (Reference 8) and 21st century storms (Reference 9) that have affected the study area are described below.

September 6-22, 1926 - The Cities of Titusville and Melbourne had tide levels in the Indian River estimated at 5 feet NGVD.

September 6-20, 1928 - Hurricane winds of 80 miles per hour (mph) lasted nearly 6 hours along the Indian River. Tide levels in the Indian River were estimated at 3.5 feet NGVD in the Town of Mims, 5 feet NGVD in Titusville, and 7 feet NGVD in Melbourne.

October 13-21, 1944 - A tide level of 3.9 feet NGVD was measured in the Eau Gallie River at the Atlantic Ocean, and the tide level was estimated at 3.4 feet NGVD in the Banana River at the City of Audubon.

September 11-19, 1947 - A hurricane made landfall at the City of Fort Lauderdale, with the Eau Gallie River measuring 4.6 feet NGVD at the Atlantic Ocean. The City of Fort Pierce reported tide levels of 6.8 to 8.8 feet NGVD at the Atlantic Ocean and the river areas near the inlet.

September 19-25, 1948 - The Eau Gallie River had tides at the Atlantic Ocean of 4.9 feet NGVD. The Indian River had a tide level of 4.8 feet NGVD at Melbourne and the Banana River had a tide level of 3.3 feet NGVD at Audubon.

August 24-29, 1949 - The Eau Gallie River had tide levels at the Atlantic Ocean of 4.5 feet NGVD. Melbourne estimated tide levels to be 3.5 feet NGVD in the Indian River, and the City of Sebastian measured tide levels at 1.8 feet NGVD in the Indian River.

October 15-19, 1950 - Hurricane King made landfall at the City of Miami and traveled inland parallel to the coastline. The Eau Gallie River measured 3.4 feet NGVD at the

Atlantic Ocean, the Indian River at Titusville was 5.0 feet NGVD, and the Banana River at Audubon was 2.3 feet NGVD.

October 7-12, 1953 - Tropical Storm Hazel exited into the Atlantic Ocean near Vero Beach. Tide levels in the Atlantic Ocean at Eau Caine were measured at 5.0 feet NGVD, and the Indian River at Titusville measured 2.3 feet NGVD.

August 25-September 7, 1979 - Hurricane David - The Kennedy Space Center reported tides of 5 feet above normal at the Atlantic Ocean, the Port Canaveral Coast Guard reported tides 4 feet above normal, and Patrick Air Force Base recorded a total rainfall of 6.28 inches (Reference 10).

August 2, 1995 - Tropical Storm Erin storm dropped 7-10 inches of rain, flooding much of Palm Bay and Melbourne. Most major and secondary roads were impassable and over 100 homes and businesses received some flood damage, while one department had its roof collapse due to the weight of the water (Reference 9).

September 3, 2004 - Hurricane Frances struck neighboring Vero Beach, Indian County directly and caused widespread flooding of roads, residences, and businesses in Brevard County.

September 25-26, 2004 - Hurricane Jeanne struck Vero Beach directly, following nearly the same path as Hurricane Frances. Palm Bay reported flooded streets and roads.

October 24, 2005 - Hurricane Wilma produced 10-13 inches of rain in the northern part of the county, flooding approximately 200 homes in Cocoa.

August 19-20, 2008 - Tropical Storm Fay dropped more than 27 inches of rain in Melbourne. The storm caused flooding or damage to over 1,600 homes and businesses across the county, with a loss of nearly 60 million dollars in private property and an additional 10 million dollars in damage to public infrastructure.

### 2.4 Flood Protection Measures

A series of levees exist in the eastern portion of the St. John’s River floodplain. Breaks occur in the levees and the elevations are not uniform. In addition, they do not have a consistent 3 -foot freeboard above 1-percent-annual-chance frequency levels. It has therefore been ascertained that the levees may not protect the community from rare events such as the 1-percent-annual-chance flood, although they do afford some protection from lower flood stages. Levees and dikes exist along canals in other areas and are generally not considered adequate for flood control for the same reasons.

A water control structure (the Melbourne-Tillman Water Control Structure MS-1) to control water levels in the Melbourne-Tillman canal system is located just above Port Malabar road in Palm Bay. Although not designed as a flood control structure, it provides some protection during low level flood conditions.

No other flood protection measures are known to exist within the study area.

### 3.0 ENGINEERING METHODS

For the flooding sources studied by detailed methods in the county, standard hydrologic and hydraulic study methods were used to determine the flood-hazard data required for this study. Flood events of a magnitude that is expected to be equaled or exceeded once on the average during any 10 -, $50-$ - 100 -, or 500 -year period (recurrence interval) have been selected as having special significance for floodplain management and for flood insurance rates. These events, commonly termed the 10 -, $50-, 100$-, and 500 -year floods, have a $10-, 2-, 1-$, and 0.2 -percent chance, respectively, of being equaled or exceeded during any year. Although the recurrence interval represents the long-term, average period between floods of a specific magnitude, rare floods could occur at short intervals or even within the same year. The risk of experiencing a rare flood increases when periods greater than 1 year are considered. For example, the risk of having a flood that equals or exceeds the 1-percent-annual-chance flood in any 50 -year period is approximately 40 percent ( 4 in 10 ); for any 90 -year period, the risk increases to approximately 60 percent ( 6 in 10). The analyses reported herein reflect flooding potentials based on conditions existing in the community at the time of completion of this study. Maps and flood elevations will be amended periodically to reflect future changes.

### 3.1 Hydrologic Analyses

Hydrologic analyses were carried out to establish peak discharge-frequency relationships for each flooding source studied by detailed methods affecting Brevard County, including both riverine and coastal sources.

Information on the methods used to determine peak discharge-frequency relationships for the streams studied by detailed methods is shown below.

### 3.1.1 Methods for Flooding Sources Incorporated from Previous Studies

The 1-percent-annual-chance flood profile for the St. John's River was obtained from the St. John's River Water Management District (Reference 11). The flood profile was completed by conducting statistical frequency analyses on observed or simulated annual peak flow data and then performing backwater computations on flood flows of the desired frequencies, mean annual peak flow, and the 20-, 10-, 4-, 2-, and 1-percent-annual-chance floods. These flood profiles supersede those presented in the USAGE "General Design Memorandum" (Reference 12).

Regionalized regression equations developed by the USGS, in cooperation with the Florida Department of Transportation, were used for determining peak discharge-frequency relationships for the Eau Gallie River, Crane, Goat, Trout, Kid, and North Prong Creeks, and Tributaries of Turkey Creek (Reference 13). The peak discharges for Turkey Creek east of the Melbourne-Tillman Water Control District water control structure MS-1 were adopted from a detailed hydrologic study (Reference 14). Storm water runoff hydrographs were generated for over 380 individual drainage subbasins and then routed hydrodynamically
through Turkey Creek and its associated canals and tributaries.
The upstream portion of Crane Creek is a manmade canal that cuts through a land ridge, which formerly divided the natural drainage areas of the St. John's River and the Indian River. During high flood stages, this allows a portion of the flow to go westward into the St. John's River floodplain. The drainage areas shown in Table 4 represent the areas under low flow conditions. During the period of high flood stages, the actual contributing drainage areas may vary due to overflow toward the St. John's River. The rates of overflow westward were computed based on the hydraulic conditions of Crane Creek and the St. John's River. The westerly flow rates were computed with the assumption that the starting watersurface elevations at the west side of John Rodes Boulevard are the same elevations as the St. John's River flood elevations for the 10-, 2-, 1-, and 0.2-percent-annual-chance frequencies.

Some of the flood conditions in the Titusville area were considered as pondingtype flooding. The flood elevations were determined with a volumetric analysis of the stormwater runoff. The study area was divided into five subbasins and stage-storage relationships were computed using topographic maps developed by the City of Titusville (Reference 15).

For Horse Creek and Otter Creek, rainfall-frequency estimates were obtained by statistical analysis of records prepared by the U.S. Weather Bureau, Technical Paper No. 40 (Reference 16). The amount of rainfall that will run off (rainfall excess) from a particular basin is less than the rainfall due to soil permeability, vegetation cover, and other characteristics. To estimate the rainfall excess, the SCS has developed Runoff Curve Numbers which relate rainfall to direct runoff (Reference 17). The Runoff Curve Numbers were used to calculate the infiltration losses based on the soil type and land use.

The hydrology for Horse Creek and Otter Creek were formulated by the TRACOR Method (Reference 18). The TRACOR method of urban hydrology uses mathematical equations derived from field experiments and observations to calculate volume and peak rates of storm runoff at a desired location as a result of recurring storms of $10-$, $2-, 1$-, and 0.2 -percent-annual-chance frequencies. The SCS method was used to check the TRACOR method (Reference 17). The SCS method uses mathematical equations derived from field experiments and observations to calculate peak flows and volumes.

### 3.1.2 Methods for Flooding Sources with New or Revised Analyses in Current Study

Detailed hydrologic calculations for North Merrit Island area were performed using the ICPR program (Reference 19). The standard Soil Conservation Service (SCS) methodology was utilized, with the exception of using a peaking factor of 256 in lieu of the standard 484 peaking factor (Reference 20). This variation was adopted to account for the difference in terrain between the SCS default terrain and the terrain in Brevard County (gently rolling hills and flat areas with slight
slopes, respectively). Land use data was obtained from Saint Johns River Water Management District and soil data was obtained from Natural Resources Conservation Service's Soil Data Mart. Based on guidance from NRCS TR-55 (Reference 21), a 24 hour event with SCS antecedent moisture type III distribution is used for North Merrit Island area.

A summary of the drainage area-peak discharge relationships for the streams studied by detailed methods is shown in Table 4, "Summary of Discharges."
Table 4: Summary of Discharges
$\left.\begin{array}{lccccc}\text { Flooding Source and Location } & \begin{array}{c}\text { Drainage Area } \\ \text { (Square miles) }\end{array} & \begin{array}{c}\text { Peak Discharges (Cubic Feet per Second) } \\ \text { 1-percent- } \\ \text { 10-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 0-percent- } \\ \text { annual-chance }\end{array} \\ \text { annual-chance }\end{array}\right]$
Table 4: Summary of Discharges (continued)

| Flooding Source and Location | Drainage Area (Square miles) | Peak Discharges (Cubic Feet per Second) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 10-percent-annual-chance | 2-percent-annual-chance | 1-percent-annual-chance | 0.2-percent-annual-chance |
| At a point approximately 1,600 feet downstream of Dairy Road | 1.37 | 155 | 305 | 400 | 610 |
| CRANE CREEK DIVERSION FROM ST. JOHN'S RIVER |  |  |  |  |  |
| At Dayton Boulevard | 6.85 | 295 | * | * | * |
| At Wickham Road | 5.47 | * | 130 | 272 | 618 |
| At John Rodes Boulevard | 3.44 | 83 | 130 | 272 | 618 |
| EAU GALLIE RIVER |  |  |  |  |  |
| At mouth | 8.25 | 675 | 1,220 | 1,475 | 2,210 |
| At U.S. Route 1 | 4.79 | 495 | 885 | 1,075 | 1,590 |
| At Florida East Coast Railway | 4.62 | 485 | 870 | 1,055 | 1,560 |
| At Eau Gallie Boulevard | 3.23 | 390 | 700 | 860 | 1,285 |
| At Croton Road | 2.78 | 350 | 635 | 780 | 1,185 |
| At Wickham Road | 1.37 | 193 | 360 | 435 | 669 |
| GOAT CREEK |  |  |  |  |  |
| At U.S. Route 1 | 9.91 | 298 | 542 | 680 | 1,038 |
| At Old Valkaria Road | 9.36 | 285 | 520 | 650 | 995 |
| At Henderson Drive | 8.74 | 273 | 492 | 620 | 947 |
| At Highland Road | 7.20 | 238 | 428 | 541 | 827 |
| At a point approximately 800 feet downstream at Leghorn Road | 6.90 | 230 | 417 | 528 | 805 |

Table 4: Summary of Discharges (continued)

| Flooding Source and Location | Drainage Area (Square miles) | Peak Discharges (Cubic Feet per Second) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 10-percent-annual-chance | 2-percent-annual-chance | 1-percent-annual-chance | 0.2-percent-annual-chance |
| GOAT CREEK(continued) |  |  |  |  |  |
| At Leghorn Road | 0.96 | 75 | 134 | 185 | 298 |
| HORSE CREEK |  |  |  |  |  |
| At mouth | 3.09 | 870 | 1,490 | 1,800 | 2,200 |
| At Croton Road | 1.97 | 530 | 960 | 1,080 | 1,400 |
| KID CREEK |  |  |  |  |  |
| At mouth | 1.77 | 99 | 180 | 240 | 378 |
| At a point approximately 600 feet upstream of Old Dixie Highway | 1.59 | 94 | 170 | 229 | 360 |
| At a point approximately 2,600 feet upstream of Old Dixie Highway | 1.35 | 88 | 157 | 212 | 340 |
| At a point approximately 0.91 mile upstream of Old Dixie Highway | 1.26 | 84 | 150 | 205 | 330 |
| NORTH PRONG CREEK |  |  |  |  |  |
| At mouth | 20.79 | 771 | 1,383 | 1,690 | 2,533 |
| At a point approximately 1.52 miles upstream of mouth | 19.43 | 749 | 1,344 | 1,642 | 2,457 |
| At a point approximately 1.99 miles upstream of mouth | 18.55 | 634 | 1,148 | 1,408 | 2,145 |
| OTTER CREEK |  |  |  |  |  |
| At mouth | 1.08 | 350 | 650 | 790 | 980 |

Table 4: Summary of Discharges (continued)

| Flooding Source and Location | Drainage Area | Peak Discharges (Cubic Feet per Second) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | (Square miles) | 10-percent-annual-chance | 2-percent-annual-chance | 1-percent-annual-chance | 0.2-percent-annual-chance |
| At Robin Hood Drive | 0.71 | 220 | 410 | 490 | 610 |
| SOUTH PRONG CREEK |  |  |  |  |  |
| At U.S. Route 1 | 202.00 | 2,800 | 5,000 | 6,000 | 9,000 |
| At a point approximately 2.08 miles upstream of U.S. Route 1 | 80.80 | 1,950 | 3,400 | 4,150 | 6,100 |
| TROUT CREEK |  |  |  |  |  |
| At mouth | 10.57 | 314 | 570 | 710 | 1,088 |
| At Third Street | 8.35 | 264 | 478 | 600 | 918 |
| TURKEY CREEK |  |  |  |  |  |
| At mouth | * | 8,500 | 10,000 | 10,700 | 12,000 |
| Just downstream of confluence of Turkey Creek Channel B | * | 7,400 | 8,800 | 9,450 | 10,800 |
| At Control Structure MS-1 | * | 6,200 | 7,400 | 8,000 | 9,000 |
| TURKEY CREEK CHANNEL A |  |  |  |  |  |
| At mouth | 3.73 | 258 | 490 | 635 | 955 |
| At Clearmont Street | 2.53 | 210 | 407 | 535 | 800 |
| TURKEY CREEK CHANNEL A |  |  |  |  |  |
| At a point approximately 1,500 feet upstream of Clearmont Street | 0.81 | 120 | 240 | 337 | 510 |

Table 4: Summary of Discharges (continued)

| Flooding Source and Location | Drainage Area (Square miles) | Peak Discharges (Cubic Feet per Second) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 10-percent-annual-chance | 2-percent-annual-chance | 1-percent-annual-chance | 0.2-percent-annual-chance |
| TURKEY CREEK CHANNEL B |  |  |  |  |  |
| At mouth | 1.68 | 173 | 330 | 442 | 668 |
| At Malabar Road | 1.14 | 140 | 280 | 380 | 575 |
| TURKEY CREEK CHANNEL C |  |  |  |  |  |
| At mouth | 7.34 | 395 | 733 | 915 | 1,400 |
| Just upstream of confluence of Turkey Creek Channel D | 1.10 | 80 | 152 | 190 | 345 |
| TURKEY CREEK CHANNEL C-76 |  |  |  |  |  |
| At mouth | 1.49 | 164 | 318 | 427 | 640 |
| At Babcock Street | 0.70 | 110 | 223 | 320 | 490 |
| TURKEY CREEK CHANNEL D |  |  |  |  |  |
| At mouth | 4.96 | 305 | 570 | 730 | 1,105 |
| TURKEY CREEK CHANNEL D |  |  |  |  |  |
| At a point approximately 400 feet downstream of confluence of Turkey Creek Channel E | 3.40 | 245 | 468 | 610 | 912 |
| At a point approximately 700 feet upstream of confluence of Turkey Creek Channel E | 3.00 | 215 | 400 | 528 | 797 |
| TURKEY CREEK CHANNEL E |  |  |  |  |  |
| At mouth | 3.03 | 30 | 70 | 82 | 115 |

Table 4: Summary of Discharges (continued)

| Flooding Source and Location | Drainage Area <br> (Square miles) | Peak Discharges (Cubic Feet per Second) <br> 10-percent- <br> 2-percent- <br> 1-percent- <br> annual-chance |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| annual-chance | 0.2-percent- <br> annual-chance |  |  |  |  |
| TURKEY CREEK CHANNEL G <br> At mouth | 1.10 | 120 | 230 | 315 | 410 |
| * Data Not Available |  |  |  |  | 4 |

Inundation from the Atlantic Ocean, the Indian River, and the Banana River caused by passage of storms (storm surge) was determined by the joint probability method (Reference 22). The storm populations were described by probability distributions of five parameters that influence surge heights. These parameters were central pressure depression (which measures the intensity of the storm), radius to maximum winds, forward speed of the storm, shoreline crossing point, and crossing angle. These characteristics were described statistically based on an analysis of observed storms in the vicinity of Brevard County. Primary sources of data for this analysis were the Tropical Cyclones of the North Atlantic Ocean; Some Climatological Characteristics of Hurricanes and Tropical Storms, Gulf and East Coasts of the United States; and Meteorological Criteria for Standard Project Hurricane and Probable Maximum Hurricane Windfields, Gulf and East Coasts of the United States, all prepared by the U.S. Department of Commerce, National Oceanic and Atmospheric Administration (NOAA) (References 23; 24; 25). A summary of the parameters used for the area is presented in Table 5, "Parameter Values for Surge Elevations."

Table 5: Parameter Values for Surge Elevations

| Parameter | Assigned Values |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Central pressure depression (millibars) | 18.9 | 32.6 | 46.4 | 60.1 | 73.9 | 87.6 | 101.4 | 115.1 |
| Probability ${ }^{1}$ | 0.274 | 0.358 | 0.181 | 0.092 | 0.047 | 0.024 | 0.012 | 0.012 |
| Storm radius to maximum winds (nautical miles) | 13.0 |  |  |  | 28.0 |  |  |  |
| Probability | 0.433 |  |  |  | 0.567 |  |  |  |
| Forward speed (knots) | 7.5 |  |  | 16.5 |  | 25.5 |  |  |
| Probability ${ }^{2}$ | 0.533 |  | 0.413 |  |  | 0.054 |  |  |
| Direction of storm path (degrees from true north) | 47.0 |  | 111.0 |  | 174.0 |  | 238.0 |  |
| Probability ${ }^{2}$ | 0.036 |  | 0.222 |  | 0.353 |  | 0.389 |  |
| Frequency of storm occurrence (storm/nautical mile/year) | 0.00455 |  |  |  |  |  |  |  |
| ${ }^{1}$ Probabilities for entering, alongshore, and exiting <br> ${ }^{2}$ Probabilities for entering |  |  |  |  |  |  |  |  |

For areas subject to flooding directly from the Atlantic Ocean, the Indian River, and the Banana River, the FEMA standard storm surge model was used to simulate the coastal surge generated by any chosen storm (that is, any combination of the five storm parameters defined previously). By performing such simulations for a large number of
storms, each of known total probability, the frequency distribution of surge height can be established as a function of coastal location. These distributions incorporate the largescale surge behavior, but do not include an analysis of the added effects associated with much finer scale wave phenomena, such as wave height or runup. As the final step in the calculations, the astronomic tide for the region is then statistically combined with the computed storm surge to yield recurrence intervals of total water level (Reference 26).

Wave setup was determined to significantly contribute to the total stillwater flood levels along the Atlantic Ocean coast. The amount of wave setup was calculated using methodology outlined in the USACE "Shore Protection Manual" (Reference 27).

The storm-surge elevations for the 10-, 2-, 1-, and 0.2-percent-annual-chance floods have been determined for the Atlantic Ocean, the Indian and Banana Rivers, Mosquito Lagoon, and New Found Harbour and are shown in Table 6, "Summary of Stillwater Elevations." The analyses reported herein reflect the stillwater elevations due to tidal and wind setup effects and include the contributions from wave action effects.
Table 6: Summary of Stillwater Elevations

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Elevat 2-percent-annual-chance | (Feet NAVD) 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 1 | 40 | 2.2 | 4.4 | 5.4 | 7.8 | AE | 5.7-6.7 |
| 2 | 40 | 2.1 | 4.0 | 5.2 | 7.3 | AE | 5.7-6.7 |
| MOSQUITO LAGOON |  |  |  |  |  |  |  |
| 3 | 45 | 1.4 | 2.9 | 3.7 | 6.5 | AE | 3.7-5.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 4 | 45 | 1.5 | 4.1 | 4.9 | 6.9 | $\begin{aligned} & \mathrm{VE} \\ & \mathrm{AE} \end{aligned}$ | $\begin{aligned} & \text { 6.7-7.7 } \\ & \text { 4.7-6.7 } \end{aligned}$ |
| 5 | 40 | 1.6 | 3.6 | 4.5 | 6.3 | AE | 4.7-6.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 6 | 65 | 3.5 | 5.8 | $8.8{ }^{3}$ | 9.2 | $\begin{aligned} & \mathrm{VE} \\ & \mathrm{AE} \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| MOSQUITO LAGOON |  |  |  |  |  |  |  |
| 7 | 45 | 1.4 | 2.9 | 3.7 | 6.5 | AE | 3.7-5.7 |
| 8 | 45 | 1.4 | 2.9 | 3.7 | 6.5 | AE | 3.7-5.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 9 | 45 | 1.2 | 3.2 | 4.0 | 5.7 | AE | 3.7-5.7 |
|  | 45 | 1.2 | 3.2 | 5.1 | 5.9 | AE | 4.7-6.7 |
| 10 | 105 | 1.0 | 2.6 | 3.4 | 4.9 | AE | 3.7-5.7 |

Table 6: Summary of Stillwater Elevations (continued)

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Elevat 2-percent-annual-chance | (Feet NAVD) <br> 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11 | 110 | 0.8 | 3.0 | 3.8 | 5.4 | AE | 3.7-5.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 12 | 130 | 3.4 | 5.7 | $8.6{ }^{3}$ | 9.0 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | 10.7-13.7 |
|  |  |  |  |  |  |  | 8.7-10.7 |
|  |  | 3.4 | 5.7 | 6.6 | 9.0 | AE | 6.7-7.7 |
| MOSQUITO LAGOON |  |  |  |  |  |  |  |
| 13 | 130 | 1.4 | 2.9 | 3.7 | 6.5 | AE | 3.7-5.7 |
| 14 | 130 | 1.4 | 2.9 | 3.7 | 6.5 | AE | 3.7-5.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 15 | 110,120,130 | 1.3 | 3.5 | 4.3 | 6.0 | VE | 6.7-7.7 |
|  |  |  |  |  |  | AE | 4.7-6.7 |
| 16 | 115 | 0.6 | 2.0 | 2.5 | 3.9 | AE | 2.7-3.7 |
| 17 | 110, 130 | 1.3 | 3.1 | 3.7 | 5.2 | AE | 3.7-5.7 |
|  | 110, 130 | 1.3 | 2.4 | 3.0 | 4.5 | AE | 2.7-4.7 |
|  | 110, 130 | 1.3 | 1.6 | 1.9 | 3.1 | AE | 1.7-3.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 18 | 130,135 | 3.4 | 5.7 | $8.6{ }^{3}$ | 9.0 | VE | 10.7-13.7 |
|  |  |  |  |  |  | AE | 8.7-10.7 |
|  |  | 3.4 | 5.7 | 6.6 | 9.0 | AE | 6.7-7.7 |
| MOSQUITO LAGOON |  |  |  |  |  |  |  |
| 19 | 130 | 1.4 | 2.9 | 3.7 | 6.5 | AE | 3.7-5.7 |

Table 6: Summary of Stillwater Elevations (continued)

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Eleva 2-percent-annual-chance | (Feet NAVD) 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 130 | 1.4 | 2.9 | 3.7 | 6.5 | AE | 3.7-5.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 21 | 120,130,140 | 0.9 | 2.3 | 2.8 | 4.4 | AE | 2.7-4.7 |
|  | 120,130,140 | 0.9 | 1.5 | 1.9 | 2.9 | AE | 1.7-2.7 |
| 22 | 115 | 1.0 | 2.1 | 2.7 | 3.8 | AE | 2.7-3.7 |
| 23 | 115,180 | 0.7 | 1.7 | 2.2 | 3.3 | AE | 2.7-3.7 |
| 24 | 185 | 1.0 | 2.0 | 2.5 | 3.6 | AE | 2.7-3.7 |
| 25 | 140,185,205 | 0.6 | 1.5 | 1.9 | 3.1 | AE | 1.7-3.7 |
| 26 | 185 | 0.5 | 1.3 | 1.7 | 2.5 | AE | 1.7-2.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 27 | 145,230 | 3.5 | 5.7 | $8.9{ }^{3}$ | 9.3 | VE | 10.7-14.7 |
|  |  |  |  |  |  | AE | 8.7-10.7 |
|  |  | 3.5 | 5.7 | 6.9 | 9.3 | AE | 6.7-7.7 |
| MOSQUITO LAGOON |  |  |  |  |  |  |  |
| 28 | 145 | 1.7 | 3.6 | 4.3 | 6.0 | AE | 4.7-5.7 |
| 29 | 145 | 2.1 | 3.8 | 4.6 | 6.1 | AE | 4.7-5.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 30 | 205,210 | 0.5 | 1.6 | 2.1 | 2.9 | AE | 1.7-3.7 |
|  | 205,210 | 0.5 | 2.0 | 2.3 | 3.3 | AE | 2.7-3.7 |
|  | 205,210 | 0.5 | 3.0 | 3.7 | 5.2 | AE | 3.7 |
| 31 | 195 | -0.1 | 0.8 | 1.1 | 2.1 | AE | 0.7-2.7 |

Table 6: Summary of Stillwater Elevations (continued)
$\left.\begin{array}{cccccccc}\begin{array}{c}\text { Flooding Source } \\ \text { and Transect }\end{array} & \text { FIRM Panel } & \begin{array}{c}\text { 10-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Stillwater Elevation (Feet NAVD) } \\ \text { 2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 1-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 0.2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Base Flood } \\ \text { Elevation, }\end{array} \\ \text { (Feet NAVD) }\end{array}\right)$
Table 6: Summary of Stillwater Elevations (continued)
$\left.\begin{array}{cccccccc}\begin{array}{c}\text { Flooding Source } \\ \text { and Transect }\end{array} & \text { FIRM Panel } & \begin{array}{c}\text { 10-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Stillwater Elevation (Feet NAVD) } \\ \text { 2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 1-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 0.2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Base Flood } \\ \text { Elevation }\end{array} \\ \hline 42 & 285 & 0.3 & 0.9 & 1.2 & 2.0 & \text { AE } & 1.7-2.7 \\ \text { (Feet NAVD) }\end{array}\right\}$
Table 6: Summary of Stillwater Elevations (continued)

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Table 6: Summary of Stillwater Elevations (continued)

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Elevat 2-percent-annual-chance | (Feet NAVD) 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 64 | 355 | 1.1 | 2.5 | 3.1 | 4.6 | AE | 2.7-4.7 |
| 65 | 355 | 1.2 | 2.7 | 3.4 | 4.9 | AE | 3.7-4.7 |
| BANANA RIVER |  |  |  |  |  |  |  |
| 66 | 360 | 0.4 | 0.9 | 1.1 | 1.8 | AE | 0.7-1.7 |
| 67 | 360 | 0.5 | 1.1 | 1.3 | 1.9 | AE | 1.7 |
| NEWFOUND HARBOUR |  |  |  |  |  |  |  |
| 68 | 360 | 0.6 | 1.4 | 1.7 | 2.3 | AE | 1.7-2.7 |
| 69 | 360 | 0.8 | 1.7 | 2.2 | 3.0 | AE | 2.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 70 | 386,388 | $\begin{aligned} & 3.4 \\ & 3.4 \end{aligned}$ | 5.7 5.7 | $\begin{aligned} & 8.9^{3} \\ & 6.9 \end{aligned}$ | 9.4 9.4 | $\begin{aligned} & \text { VE } \\ & \text { AE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-14.7 \\ 8.7-10.7 \\ 6.7-7.7 \end{gathered}$ |
| BANANA RIVER |  |  |  |  |  |  |  |
| 71 | 386,388 | 0.1 | 1.0 | 1.1 | 1.4 | AE | 0.7-1.7 |
| 72 | 370 | 0.3 | 1.0 | 1.4 | 2.1 | AE | 1.7-2.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 73 | 370 | 0.5 | 1.6 | 2.1 | 3.2 | AE | 1.7-2.7 |
| 74 | 365 | 0.6 | 1.7 | 2.2 | 3.5 | AE | 2.7 |
| 75 | 370 | 0.5 | 1.5 | 1.9 | 2.9 | AE | 1.7-2.7 |

Table 6: Summary of Stillwater Elevations (continued)

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Elevat 2-percent-annual-chance | (Feet NAVD) 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 76 | 365,370 | 0.5 | 1.5 | 1.9 | 2.9 | AE | 1.7-2.7 |
| BANANA RIVER |  |  |  |  |  |  |  |
| 77 | 388 | 0.1 | 0.6 | 0.8 | 1.1 | AE | 0.7-1.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 78 | 451 | 3.3 | 5.6 | $8.8{ }^{3}$ | 9.2 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-14.7 \\ 8.7-10.7 \end{gathered}$ |
| BANANA RIVER |  |  |  |  |  |  |  |
| 79 | 453 | 0.4 | 1.2 | 1.5 | 2.3 | AE | 1.7-2.7 |
| 80 | 435 | 0.3 | 1.0 | 1.3 | 2.1 | AE | 1.7-2.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 81 | 435 | 0.3 | 1.3 | 1.8 | 2.7 | AE | 1.7-2.7 |
| 82 | 435 | 0.4 | 1.4 | 1.8 | 2.6 | AE | 1.7-2.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 83 | 451,453 | 3.3 | 5.5 | $8.7^{3}$ | 9.0 | VE AE | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| BANANA RIVER |  |  |  |  |  |  |  |
| 84 | 451,453 | 0.7 | 1.9 | 2.3 | 3.3 | AE | 2.7-3.7 |
| 85 | 435 | 0.6 | 1.5 | 1.9 | 2.9 | AE | 1.7-2.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 86 | 435 | 0.3 | 1.3 | 1.7 | 2.7 | AE | 1.7-2.7 |

Table 6: Summary of Stillwater Elevations (continued)

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Elevat 2-percent-annual-chance | (Feet NAVD) 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 87 | 435 | 0.3 | 1.3 | 1.8 | 2.6 | AE | 1.7-2.7 |
| BANANA RIVER |  |  |  |  |  |  |  |
| 88 | 435 | 0.1 | 1.0 | 1.4 | 2.3 | AE | 1.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 89 | 435 | 0.5 | 1.8 | 2.4 | 3.8 | AE | 2.7-3.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 90 | 453,462 | 3.3 | 5.5 | $8.7^{3}$ | 9.0 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| BANANA RIVER |  |  |  |  |  |  |  |
| 91 | 461 | 0.3 | 1.1 | 1.4 | 2.3 | AE | 1.7 |
| 92 | 461 | 0.3 | 1.1 | 1.4 | 2.3 | AE | 1.7 |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 93 | 461,442 | 0.3 | 1.4 | 2.0 | 3.2 | AE | 1.7-2.7 |
| 94 | 442 | 0.4 | 1.6 | 2.2 | 3.3 | AE | 1.7-3.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 95 | 464 | 3.3 | 5.5 | 8.7 | 9.0 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 96 | 463 | 0.3 | 1.3 | 1.7 | 2.9 | AE | 1.7-2.7 |
| 97 | 444 | 0.3 | 1.3 | 1.8 | 2.8 | AE | 1.7-2.7 |

Table 6: Summary of Stillwater Elevations (continued)
$\left.\begin{array}{cccccccc}\begin{array}{c}\text { Flooding Source } \\ \text { and Transect }\end{array} & \text { FIRM Panel } & \begin{array}{c}\text { 10-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Stillwater Elevation (Feet NAVD) } \\ \text { 2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 1-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 0.2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Base Flood } \\ \text { Zlevation }\end{array} \\ \hline \text { ATLANTIC OCEAN } \\ \text { (Feet NAVD) }\end{array}\right)$
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Table 6: Summary of Stillwater Elevations (continued)
$\left.\begin{array}{cccccccc}\begin{array}{c}\text { Flooding Source } \\ \text { and Transect }\end{array} & \text { FIRM Panel } & \begin{array}{c}\text { 10-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Stillwater Elevation (Feet NAVD) } \\ \text { 2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 1-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { 0.2-percent- } \\ \text { annual-chance }\end{array} & \begin{array}{c}\text { Base Flood } \\ \text { Elevation, }\end{array} \\ \text { (Feet NAVD) }\end{array}\right\}$
Table 6: Summary of Stillwater Elevations (continued)

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Elevat 2-percent-annual-chance | (Feet NAVD) 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 119 | 607,609 | 3.2 | 5.3 | $8.3{ }^{3}$ | 8.8 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 120 | 607,609 | 2.2 | 3.4 | 3.9 | 5.2 | AE | 3.7-5.7 |
| 121 | 610 | 2.2 | 3.4 | 3.9 | 5.2 | AE | 3.7-5.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 122 | 636 | 3.2 | 5.3 | $8.3{ }^{3}$ | 8.8 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 123 | 609,617 | 2.3 | 3.5 | 4.0 | 5.3 | AE | 3.7-5.7 |
| 124 | 617 | 2.3 | 3.5 | 4.0 | 5.3 | AE | 3.7-5.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 125 | 636 | 3.2 | 5.3 | $8.3{ }^{3}$ | 8.7 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 126 | 617,636 | 2.1 | 3.3 | 3.7 | 4.9 | AE | 3.7-4.7 |
| 127 | 617 | 2.3 | 3.4 | 4.0 | 5.3 | AE | 3.7-5.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 128 | 636,638 | 3.1 | 5.2 | $8.2{ }^{3}$ | 8.5 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |

Table 6: Summary of Stillwater Elevations (continued)

| Flooding Source and Transect | FIRM Panel | 10-percent-annual-chance | Stillwater Elevat 2-percent-annual-chance | (Feet NAVD) 1-percent-annual-chance | 0.2-percent-annual-chance | Zone | Base Flood Elevation ${ }^{1,2}$ (Feet NAVD) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 129 | 636,638 | 1.7 | 2.7 | 3.3 | 4.5 | AE | 3.7-4.7 |
| 130 | 619 | 2.0 | 3.5 | 4.0 | 5.4 | AE | 3.7-5.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 131 | 639 | 3.1 | 5.2 | $8.2{ }^{3}$ | 8.5 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 132 | 638,639,726,727 | 1.8 | 3.0 | 3.6 | 5.0 | AE | 3.7-5.7 |
| 133 | 726 | 2.1 | 3.6 | 4.2 | 5.6 | AE | 3.7-5.7 |
| ATLANTIC OCEAN |  |  |  |  |  |  |  |
| 134 | 727 | 3.1 | 5.2 | $8.2{ }^{3}$ | 8.5 | $\begin{aligned} & \text { VE } \\ & \text { AE } \end{aligned}$ | $\begin{gathered} 10.7-13.7 \\ 8.7-10.7 \end{gathered}$ |
| INDIAN RIVER |  |  |  |  |  |  |  |
| 135 | 727 | 1.9 | 3.2 | 3.8 | 5.4 | AE | 3.7-5.7 |

${ }^{1}$ May include effects of wave action
${ }^{2}$ Due to map scale limitations, base flood elevations shown on map may represent average elevations

### 3.2 Hydraulic Analyses

Analyses of the hydraulic characteristics of flooding from the sources studied were carried out to provide estimates of the elevations of floods of the selected recurrence intervals. Users should be aware that flood elevations shown on the FIRM represent rounded whole-foot elevations and may not exactly reflect the elevations shown on the Flood Profiles or in the Floodway Data tables in the FIS report. Flood elevations shown on the FIRM are primarily intended for flood insurance rating purposes. For construction and/or floodplain management purposes, users are cautioned to use the flood elevation data presented in this FIS in conjunction with the data shown on the FIRM.

Locations of selected cross sections used in the hydraulic analyses are shown on the Flood Profiles (Exhibit 1). For stream segments for which a Floodway was computed, selected cross-section locations are also shown on the FIRM (Exhibit 2).

The hydraulic analyses for this study were based on unobstructed flow. The flood elevations shown on the Flood Profiles (Exhibit 1) are thus considered valid only if hydraulic structures remain unobstructed, operate properly, and do not fail.

### 3.2.1 Methods for Flooding Sources with New or Revised Analyses in Current Study

The dynamic hydraulic routing for North Merrit Island area with many depression areas was performed using the Interconnected Channel and Pond Routing (ICPR) program, version 3.10 (Reference 28) to determine the 1-percent-annual-chance flood elevation. The dimensions and geometry of drainage structures and interconnected channels were obtained form field survey. Storage volume parameters are calculated using the ArcHydro ESRI toolset (Reference 29) based on digital terrain data and updated with as-built information. The available storage of ponding area was calculated in a half foot increment from the lowest elevation in the sub-basin to the highest.
3.2.2 Methods for Flooding Sources Incorporated from Previous Studies

Water-surface elevations for floods of the selected recurrence intervals were developed using the HEC-2 computer model (Reference 30). Cross sections for the backwater analyses were obtained from field surveys (Reference 31). In some cases, topographic maps were used to extend surveyed cross sections (Reference 32; 33). Some cross sections for Turkey Creek tributaries were obtained from the "Brook Hollow Stormwater Management Master Plan" (Reference 14).

All bridges and culverts were field-checked to obtain elevation data and structural geometry.

Channel roughness factors (Manning's " n " values) used in the hydraulic computations were chosen by engineering judgment on the basis of field observation and aerial photographs of the streams and floodplain areas (Reference 34; 35; 36). The detailed roughness value ranges for each stream are listed in Table 7, "Summary of Roughness Coefficients."

Table 7: Summary of Roughness Coefficients

| Flooding Source | Roughness Coefficients |  |
| :--- | :---: | :---: |
|  | Channel | Overbanks |
| Crane Creek | $0.030-0.060$ | $0.040-0.100$ |
| Crane Creek Channel A | $0.030-0.060$ | $0.040-0.100$ |
| Crane Creek Channel B | $0.030-0.060$ | $0.050-0.100$ |
| Crane Creek Diversion from <br> St. John's River | $0.030-0.060$ | $0.040-0.100$ |
| Eau Gallie River | $0.035-0.050$ | $0.050-0.130$ |
| Goat Creek | $0.030-0.060$ | $0.040-0.090$ |
| Horse Creek | 0.060 | 0.150 |
| Kid Creek | $0.035-0.070$ | $0.060-0.120$ |
| North Prong Creek | $0.030-0.038$ | 0.100 |
| Otter Creek | 0.060 | 0.150 |
| South Prong Creek | $0.040-0.050$ | $0.070-0.090$ |
| Trout Creek | $0.035-0.060$ | $0.060-0.090$ |
| Turkey Creek (including Channels A-E, <br> G, and C-76) | $0.030-0.100$ | $0.050-0.150$ |

The slope-area method was used to set the HEC-2 starting water-surface elevation for all streams studied in detail other than Horse Creek and Otter Creek; starting water-surface elevations for those two streams were based on the computed water-surface elevation at the confluence with the receiving stream.

The water-surface profiles for the St. John's River were obtained from the USACE (Reference 12). The 0.2 -percent-annual-chance frequency profiles were projected from the lower frequency levels of this study.

Hydraulic analyses were carried out to provide estimates of the elevations of floods of the selected recurrence intervals caused by storm surge along each of the shorelines. These analyses considered storm characteristics and the shoreline and bathymetric characteristics of the flooding sources. The FEMA standard coastal storm surge model is a numerical hydrodynamic computer model that calculates the coastal storm surges previously described in Section 3.1.

The FEMA storm surge model was used to simulate the hydrodynamic behavior of the surge generated by the various synthetic storms. This model utilizes a grid pattern approximating the geographical features of the study area and the adjoining areas. Surges were computed using grids of 5 nautical miles.

Water depths and land heights for the model grid systems were obtained from topographic maps, bathymetric maps, hydrographic surveys, nautical charts, beach profiles, aerial photographs, and coastal construction control line maps (References 32; 37; 38; 39; 40; 41; 42).

The methodology for analyzing the effects of wave heights associated with coastal storm surge flooding is described in a report prepared by the National Academy of Sciences (NAS) (Reference 43). This method is based on the following major concepts. First, depth-limited waves in shallow water reach a maximum breaking height that is equal to 0.78 times the stillwater depth. The wave crest is 70 percent of the total wave height above the stillwater level. The second major concept is that wave height may be diminished by dissipation of energy due to the presence of obstructions, such as sand dunes, dikes and seawalls, buildings, and vegetation. The amount of energy dissipation is a function of the physical characteristics of the obstruction and is determined by NAS procedures (Reference 43). The third major concept is that wave height can be regenerated in open fetch areas due to the transfer of wind energy to the water. This added energy is related to fetch length and depth.

Transects (cross-section lines) were located along the coastal areas as illustrated in Figure 1, The transects were located with consideration given to the physical and cultural characteristics of the land so that they would closely represent conditions in their locality. Transects were spaced close together in areas of complex topography and dense development. In areas having more uniform characteristics, they were spaced at large intervals. It was also necessary to locate transects in areas where unique flooding existed and in areas where computed wave heights varied significantly between adjacent transects.


Table 8: Transect Locations, Stillwater Starting Elevations, and Initial Wave Crest Elevations (continued)

| Transect | Location |  | 1-percent-annual-chance <br> Elevation (Feet NAVD) |  |
| :---: | :--- | :---: | :---: | :---: |
|  |  | Stillwater | Wave Crest |  |
| 134 | From the Atlantic coastline, approximately 1.3 miles <br> south of Long Point Road, extending west | $8.2^{6}$ | $13.7^{1}$ |  |
| 135 | From the Indian River east bank, approximately 1.3 <br> miles south of Long Point Road, extending east | 3.8 | $5.8^{3}$ |  |

FLOODING SOURCE
$\begin{array}{ll}{ }^{1} \text { Atlantic Ocean } & { }^{4} \text { Banana River } \\ { }^{2} \text { Mosquito Lagoon } & { }^{5} \text { Banana River/New Found Harbour } \\ { }^{3} \text { Indian River } & { }^{6} \text { Includes the effects of wave runup }\end{array}$

### 3.3 Vertical Datum

All FIS reports and FIRMs are referenced to a specific vertical datum. The vertical datum provides a starting point against which flood, ground, and structure elevations can be referenced and compared. Until recently, the standard vertical datum used for newly created or revised FIS reports and FIRMs was the National Geodetic Vertical Datum of 1929 (NGVD). With the completion of the North American Vertical Datum of 1988 (NAVD), many FIS reports and FIRMs are now prepared using NAVD as the referenced vertical datum.

Flood elevations shown in this FIS report and on the FIRM are referenced to the NAVD88. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. Some of the data used in this revision were taken from the prior effective FIS reports and FIRMs and adjusted to NAVD88. The datum conversion factor from NGVD29 to NAVD88 in Brevard County is negative 1.3 feet.

For information regarding conversion between the NGVD and NAVD, visit the National Geodetic Survey website at www.ngs.noaa.gov, or contact the National Geodetic Survey at the following address:

Vertical Network Branch, N/CG13
National Geodetic Survey, NOAA
Silver Spring Metro Center 3
1315 East-West Highway
Silver Spring, Maryland 20910
(301) 713-3191

Temporary vertical monuments are often established during the preparation of a flood hazard analysis for the purpose of establishing local vertical control. Although these monuments are not shown on the FIRM, they may be found in the Technical Support Data Notebook associated with the FIS report and FIRM for this community. Interested individuals may contact FEMA to access these data.

To obtain current elevation, description, and/or location information for benchmarks shown on this map, please contact the Information Services Branch of the NGS at (301) 713-3242, or visit their Web site at www.ngs.noaa.gov.

### 4.0 FLOODPLAIN MANAGEMENT APPLICATIONS

The NFIP encourages State and local governments to adopt sound floodplain management programs. To assist in this endeavor, each FIS report provides 1-percent-annual-chance floodplain data, which may include a combination of the following: 10-, $2-$, $1-$, and 0.2 -percent-annual-chance flood elevations; delineations of the 1 - and 0.2 -percent-annual-chance floodplains; and a 1-percent-annual-chance floodway. This information is presented on the FIRM and in many components of the FIS report, including Flood Profiles, Floodway Data tables, and Summary of Stillwater Elevation tables. Users should reference the data presented in the FIS report as well as additional information that may be available at the local community map repository before making flood elevation and/or floodplain boundary determinations.

### 4.1 Floodplain Boundaries

To provide a national standard without regional discrimination, the 1-percent-annualchance flood has been adopted by FEMA as the base flood for floodplain management purposes. The 0.2-percent-annual-chance flood is employed to indicate additional areas of flood risk in the community. For each stream studied by detailed methods, the 1 - and 0.2-percent-annual-chance floodplain boundaries have been delineated using the flood elevations determined at each cross section.

For each stream studied by detailed methods, the 1- and 0.2-percent-annual-chance floodplain boundaries have been delineated using the flood elevations determined at each cross section. Between cross sections, the boundaries were interpolated using elevations obtained from 10 meter Digital Elevation Models produced by the U.S. Geological Survey (Reference 2).

The 1- and 0.2-percent-annual-chance floodplain boundaries are shown on the FIRM. On this map, the 1-percent-annual-chance floodplain boundary corresponds to the boundary of the areas of special flood hazards (Zones A and AE), and the 0.2-percent-annualchance floodplain boundary corresponds to the boundary of areas of moderate flood hazards. In cases where the 1 - and 0.2 -percent-annual-chance floodplain boundaries are close together, only the 1-percent-annual-chance floodplain boundary has been shown. Small areas within the floodplain boundaries may lie above the flood elevations, but cannot be shown due to limitations of the map scale and/or lack of detailed topographic data.

For the streams studied by approximate methods, only the 1-percent-annual-chance floodplain boundary is shown on the FIRM.

### 4.2 Floodways

Encroachment on floodplains, such as structures and fill, reduces flood-carrying capacity, increases flood heights and velocities, and increases flood hazards in areas beyond the
encroachment itself. One aspect of floodplain management involves balancing the economic gain from floodplain development against the resulting increase in flood hazard. For purposes of the NFIP, a floodway is used as a tool to assist local communities in this aspect of floodplain management. Under this concept, the area of the 1-percent-annual-chance floodplain is divided into a floodway and a floodway fringe. The floodway is the channel of a stream, plus any adjacent floodplain areas, that must be kept free of encroachment so that the base flood can be carried without substantial increases in flood heights. Minimum Federal standards limit such increases to 1 foot, provided that hazardous velocities are not produced. The floodways in this study are presented to local agencies as minimum standards that can be adopted directly or that can be used as a basis for additional floodway studies.

The floodways presented in this study were computed for certain stream segments on the basis of equal-conveyance reduction from each side of the floodplain. Floodway widths were computed at cross sections. Between cross sections, the floodway boundaries were interpolated. The results of the floodway computations are tabulated for selected cross sections (see Table 9, "Floodway Data Table"). In cases where the floodway and 1-percent-annual-chance floodplain boundaries are either close together or collinear, only the floodway boundary is shown.

There are no cross sections located within the City of Melbourne for Otter Creek; therefore, no Floodway Data is provided for this stream. No floodway was computed for Horse Creek. Portions of the floodway width for South Prong Creek extend beyond the county boundary.

Encroachment into areas subject to inundation by floodwaters having hazardous velocities aggravates the risk of flood damage, and heightens potential flood hazards by further increasing velocities. A listing of stream velocities at selected cross sections is provided in Table 9, "Floodway Data Table." In order to reduce the risk of property damage in areas where the stream velocities are high, the community may wish to restrict development in areas outside the floodway.









Near the mouths of streams studied in detail, floodway computations are made without regard to flood elevations on the receiving water body. Therefore, "Without Floodway" elevations presented in Table 9 for certain downstream cross sections of the Eau Gallie River; Turkey Creek; Turkey Creek Channels A, B, C, D, and G; Goat Creek; Kid Creek; Crane Creek; North Prong Creek; and South Prong Creek are lower than the regulatory flood elevations in those areas, which must take into account the 1-percent-annual-chance flooding due to backwater from other sources.

The area between the floodway and 1-percent-annual-chance floodplain boundaries is termed the floodway fringe. The floodway fringe encompasses the portion of the floodplain that could be completely obstructed without increasing the water-surface elevation (WSEL) of the base flood more than 1 foot at any point. Typical relationships between the floodway and the floodway fringe and their significance to floodplain development are shown in Figure 3, "Floodway Schematic.".

Figure 3: Floodway Schematic


### 5.0 INSURANCE APPLICATIONS

For flood insurance rating purposes, flood insurance zone designations are assigned to a community based on the results of the engineering analyses. These zones are as follows:

Zone A
Zone A is the flood insurance rate zone that corresponds to the 1-percent-annual-chance floodplains that are determined in the FIS report by approximate methods. Because detailed hydraulic analyses are not performed for such areas, no base (1-percent-annual-chance) flood elevations (BFEs) or depths are shown within this zone.

Zone AE
Zone AE is the flood insurance rate zone that corresponds to the 1-percent-annual-chance floodplains that are determined in the FIS report by detailed methods. Whole-foot BFEs derived from the detailed hydraulic analyses are shown at selected intervals within this zone.

Zone AH
Zone AH is the flood insurance rate zone that corresponds to the areas of 1-percent-annual-choice shallow flooding (usually areas of ponding) where average depths are between 1 and 3 feet. Whole-foot base flood elevations derived from the detailed hydraulic analyses are shown at selected intervals within this zone.

Zone AO
Zone AO is the flood insurance rate zone that corresponds to the areas of 1-percent-annualchance shallow flooding (usually sheet flow on sloping terrain) where average depths are between 1 and 3 feet. Average whole-depths derived from the detailed hydraulic analyses are shown within this zone.

Zone VE
Zone VE is the flood insurance rate zone that corresponds to the 1-percent-annual-chance coastal floodplains that have additional hazards associated with storm waves. Whole-foot base flood elevations derived from the detailed hydraulic analyses are shown at selected intervals within this zone.

Zone X
Zone X is the flood insurance rate zone that corresponds to areas outside the 0.2 -percent-annual-chance floodplain, areas within the 0.2 -percent-annual-chance floodplain, areas of 1-percent-annual-chance flooding where average depths are less than 1 foot, areas of 1 -percent-annual-chance flooding where the contributing drainage area is less than 1 square mile (sq. mi.), and areas protected from the base flood by levees. No BFEs or depths are shown within this zone.

### 6.0 FLOOD INSURANCE RATE MAP

The FIRM is designed for flood insurance and floodplain management applications.
For flood insurance applications, the map designates flood insurance rate zones as described in Section 5.0 and, in the 1 -percent-annual-chance floodplains that were studied by detailed methods, shows selected whole-foot BFEs or average depths. Insurance agents use zones and BFEs in conjunction with information on structures and their contents to assign premium rates for flood insurance policies.

For floodplain management applications, the map shows by tints, screens, and symbols, the 1and 0.2 -percent-annual-chance floodplains, floodways, and the locations of selected cross sections used in the hydraulic analyses and floodway computations.

The countywide FIRM presents flooding information for the entire geographic area of Brevard County. Previously, FIRMs were prepared for each incorporated community and the unincorporated areas of the County identified as flood-prone. This countywide FIRM also includes flood-hazard information that was presented separately on Flood Boundary and Floodway Maps (FBFMs), where applicable. Historical data relating to the maps prepared for each community are presented in Table 10, "Community Map History."


| COMMUNITY NAME | INITIAL IDENTIFICATION | FLOOD HAZARD BOUNDARY MAP REVISIONS DATE | FIRM <br> EFFECTIVE DATE | FIRM REVISIONS DATE |
| :---: | :---: | :---: | :---: | :---: |
| Indialantic, Town of | August 18, 1972 | --- | August 18, 1972 | July 1, 1974 May 7, 1976 September 16, 1982 April 3, 1989 |
| Indian Harbour Beach, City of | June 16, 1972 | --- | June 16, 1972 | July 1, 1974 September 25, 1975 September 30, 1982 April 3, 1989 |
| Malabar, Town of | March 1, 1974 | December 19, 1975 | September 28, 1982 | September 30, 1982 April 3, 1989 August 18, 1992 |
| Melbourne, City of | August 30, 1974 | October 1, 1976 | July 1, 1979 | September 30, 1982 April 3, 1989 November 19, 1997 |
| Melbourne Beach, Town of | November 25, 1972 | --- | November 25, 1972 | July 1, 1974 October 3, 1975 September 30, 1982 April 3, 1989 August 18, 1992 November 19, 1997 |

FEDERAL EMERGENCY MANAGEMENT AGENCY
BREVARD COUNTY, FL
AND INCORPORATED AREAS
COMMUNITY MAP HISTORY



### 7.0 OTHER STUDIES

FIS reports were previously prepared for the unincorporated areas of Brevard County (Reference 47) and for the Cities of Melbourne, Palm Bay, and Titusville and the Town of Malabar (References 2; 48; 49; 50).

FIS reports were previously prepared for the unincorporated and incorporated areas of Volusia County, Indian River County, Osceola County, Orange County, and Seminole County (References 51; 52; 53; 54; 55). A flood hazard boundary map was prepared for the Town of Palm Shores (Reference 56)

This FIS report either supersedes or is compatible with all previous studies published on streams studied in this report and should be considered authoritative for the purposes of the NFIP.

### 8.0 LOCATION OF DATA

Information concerning the pertinent data used in the preparation of this study can be obtained by contacting Federal Insurance and Mitigation Division, FEMA Region IV, Koger-Center Rutgers Building, 3003 Chamblee Tucker Road, Atlanta, GA 30341.

### 9.0 BIBLIOGRAPHY AND REFERENCES

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### 10.0 REVISION DESCRIPTIONS

This section has been added to provide information regarding significant revisions made since the original FIS was printed. Future revisions may be made that do not result in the republishing of the FIS report. To assure that the user is aware of all revisions, it is advisable to contact the community repository of flood-hazard data located at:

- Brevard County Public Works Department

Brevard County Government Center
2725 Judge Fran Jamieson Way
Vierra, Florida 32940

- Cape Canaveral City Hall

105 Polk Avenue
Cap Canaveral, Florida 32920

- Cocoa City Hall

603 Brevard Avenue
Cocoa, Florida 32922

- Cocoa Beach City Hall

Building Department
2 South Orlando Avenue
Cocoa Beach, Florida 32931

- Indialantic Town Hall

216 Fifth Avenue
Indialantic, Florida 32903

- Indian Harbour Beach City Hall

2055 South Patrick Drive
Indian Harbour Beach, Florida 32937

- Malabar Town Hall

2725 Malabar Road
Malabar, Florida 32950

- Melbourne City Hall

900 East Strawbridge Avenue
Melbourne, Florida 32901

- Melbourne Village Town Hall

555 Hammock Road
Melbourne Village, Florida 32904

- Melbourne Beach Town Hall

507 Ocean Avenue
Melbourne Beach, Florida 32951

- Palm Bay City Hall

120 Malabar Road, S.E.
Palm Bay, Florida 32907

- Palm Shores Town Clerk's Office

151 Palm Circle
Palm Shores, Florida 32940

- Rockledge City Hall

Building Department
1600 Huntington Lane
Rockledge, Florida 32956

- Satellite Beach City Hall

Building and Zoning Department
565 Cassia Boulevard
Satellite Beach, Florida 32937

- Titusville City Hall

Department of Planning and Zoning
555 South Washington Avenue
Titusville, Florida 32796

- West Melbourne City Hall

2285 Minton Road
West Melbourne, Florida 32904
10.1 First Revision (Revised August 19, 1992)

The August 19, 1992 revision was initiated by a Physical Map Revision (PMR) request submitted to FEMA. That revision involved changes to the FIRM only.
10.2 Second Revision (Revised November 19, 1997)

For the November 19, 1997 revision, detailed analyses for Horse Creek and Otter Creek, within the City of Melbourne, were incorporated into the countywide FIS.
10.3 Third Revision (Revised Month Day, Year)

This Month, Day, year revision was initiated in support of the FEMA Risk MAP Program.
This revision involved updating the mapping for the entire area of Brevard County, Florida. The revision includes new detailed hydrologic and hydraulic analyses for various ponding areas within the North Merrit Island area of Brevard County. Coastal AE zones, streams, and ponding areas that had been previously studied by detailed methods were redelineated based on more detailed and up-to-date topographic data. In addition to the coastal redelineation, the location of the zone break between the AE and VE zones was revised based on the location of the Primary Frontal Dune.






# APPENDIX B 

## PRELIMINARY SIZING OF PROPOSED CROSSDRAINS

\author{

- HYDROLOGIC CALCS
}
- EXISTING CULVERTS
- PROPOSED CULVERTS


# PRELIMINARY SIZING OF PROPOSED CROSSDRAINS 

## - HYDROLOGIC CALCS



## RATIONAL METHOD COMPUTATIONS - SUMMARY OF RESULTS

## Rational Method Flow Calculations

| Project: | SR 514 |  |
| :--- | :--- | :--- |
| Basin: | $1-14$ |  |
| Designer: | CA Estrella | Checked by: |
| Date: | $6 / 24 / 2014$ | Date: |

## 1. Using the Rational Method calculate the flows for the following basins:

| Basin | Structure | Tc | Storm | C | 1 | A (ac) | Q (cfs) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | Culvert 2 | 127.7 | 2 | 0.38 | 1.38 | 286.00 | 149.38 |
|  |  |  | 10 | 0.38 | 1.91 | 286.00 | 206.54 |
|  |  |  | 25 | 0.42 | 2.20 | 286.00 | 262.16 |
|  |  |  | 50 | 0.45 | 2.43 | 286.00 | 316.03 |
|  |  | (1.) | 100 | 0.47 | 2.67 | 286.00 | 362.38 |
|  |  | (2.) | 500 |  |  |  | 470.00 |
| 3 ALT | Culvert 3 | 93.0 | 2 | 0.25 | 1.77 | 236.00 | 104.69 |
|  |  |  | 10 | 0.25 | 2.42 | 236.00 | 142.98 |
|  |  |  | 25 | 0.28 | 2.79 | 236.00 | 181.21 |
|  |  |  | 50 | 0.30 | 3.08 | 236.00 | 218.00 |
|  |  | (1.) | 100 | 0.31 | 3.37 | 236.00 | 248.99 |
|  |  | (2.) | 500 |  |  |  | 320.93 |
| 5 | Culvert 5 | 56.9 | 2 | 0.35 | 2.51 | 220.00 | 190.47 |
|  |  |  | 10 | 0.35 | 3.35 | 220.00 | 254.98 |
|  |  |  | 25 | 0.38 | 3.85 | 220.00 | 321.77 |
|  |  |  | 50 | 0.41 | 4.23 | 220.00 | 385.78 |
|  |  | (1.) | 100 | 0.43 | 4.61 | 220.00 | 437.87 |
|  |  | (2.) | 500 |  |  |  | 558.82 |
| 6 | Culvert 6 | 24.7 | 2 | 0.27 | 4.04 | 29.00 | 31.89 |
|  |  |  | 10 | 0.27 | 5.20 | 29.00 | 41.10 |
|  |  |  | 25 | 0.30 | 5.90 | 29.00 | 51.28 |
|  |  |  | 50 | 0.33 | 6.44 | 29.00 | 61.05 |
|  |  | (1.) | 100 | 0.34 | 6.97 | 29.00 | 68.81 |
|  |  | (2.) | 500 |  |  |  | 86.84 |
| 8 | Culvert 8 | 21.1 | 2 | 0.30 | 4.36 | 40.00 | 52.37 |
|  |  |  | 10 | 0.30 | 5.58 | 40.00 | 66.96 |
|  |  |  | 25 | 0.33 | 6.31 | 40.00 | 83.32 |
|  |  |  | 50 | 0.36 | 6.88 | 40.00 | 99.04 |
|  |  | (1.) | 100 | 0.38 | 7.44 | 40.00 | 111.54 |
|  |  | (2.) | 500 |  |  |  | 140.57 |
| 10 | Culvert 10 | 19.5 | 2 | 0.70 | 4.53 | 4.30 | 13.63 |
|  |  |  | 10 | 0.70 | 5.77 | 4.30 | 17.36 |
|  |  |  | 25 | 0.77 | 6.52 | 4.30 | 21.58 |
|  |  |  | 50 | 0.84 | 7.09 | 4.30 | 25.63 |
|  |  | (1.) | 100 | 0.88 | 7.67 | 4.30 | 28.85 |
|  |  | (2.) | 500 |  |  |  | 36.34 |
| 13 | Culvert 13 | 31.3 | 2 | 0.40 | 3.57 | 30.00 | 42.82 |
|  |  |  | 10 | 0.40 | 4.65 | 30.00 | 55.82 |
|  |  |  | 25 | 0.44 | 5.30 | 30.00 | 69.90 |
|  |  |  | 50 | 0.48 | 5.79 | 30.00 | 83.41 |
|  |  | (1.) | 100 | 0.50 | 6.28 | 30.00 | 94.14 |
|  |  | (2.) | 500 |  |  |  | 119.08 |


| Intensity $=\mathrm{A}+\mathrm{BX}+\mathrm{CX}^{\wedge} 2+\mathrm{DX}^{\wedge} 3$ <br> (from Table T-19, FDOT Hydrology Handbook, Feb. 2012 ) |  |  |  |  | $x=\ln$ Tc |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Zone 7 | 2 Yr | 10 Yr | 25 Yr | 50 Yr | 100 Yr CAE est |
| A | 12.10821 | 12.49556 | 12.92209 | 13.2955 | 14.671 |
| B | -2.79255 | -1.67116 | -1.11084 | -0.70432 | -1.0717 |
| C | 0.02002 | -0.34901 | -0.55019 | -0.70152 | -0.6606 |
| D | 0.02053 | 0.05017 | 0.06666 | 0.07933 | 0.0766 |

Notes:
3. Intensitites for the 100 -yr storm have been estimated from the Zone 7, 100-year IDF curve. 2. Please refer to attached Frequency vs. Discharge Curves

## RATIONAL METHOD COMPUTATIONS - TC

## Method and Date Formulat for $\mathrm{t}_{\mathrm{c}}(\mathbf{m i n}) \quad$ Remark

Kirpich (1940) $\quad \mathrm{t}_{\mathrm{c}}=0.0078 \mathrm{~L}^{0.77} \mathrm{~S}^{-0.385} \quad$ Developed from SCS data for several rural basins in Tennessee with well-defined channel and steep slopes (3\% to $10 \%$ ); for overland flow on concrete or asphalt surfaces multiply tc by 0.4 ; for concrete channels multiply by 0.2 ; no adjustments for overland flow on bare soil or flow in roadside ditches.

Variables
L= length of flow path, ft
$\mathrm{S}=$ slope of flow path, ft/ft

| Basin | Basin Area (ac) | L (ft) | $E L_{1}$ | $\mathrm{EL}_{2}$ | S (ft/ft) | $\mathrm{t}_{\mathrm{c}}(\mathrm{min})$ | $\mathrm{ft} / \mathrm{min}$ | fps |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Equilizer Pipe. Refer to Hydraulic Calcs. |  |  |  |  |  |  |  |
| 2 | 286 | 7350 | 26 | 21.5 | 0.0006 | 128 | 58 | 1.0 |
| 2 Alt. | 852 | SEE REGRESSION CALCS |  |  |  |  |  |  |
| 3 | 802 | SEE REGRESSION CALCS |  |  |  |  |  |  |
| 3 Alt. | 236 | 6150 | 26 | 20 | 0.0010 | 93 | 66 | 1.1 |
| 4 | Equilizer Pipe. Refer to Hydraulic Calcs. |  |  |  |  |  |  |  |
| 5 | 220 | 4760 | 26 | 16 | 0.0021 | 57 | 84 | 1.4 |
| 6 | 29 | 1950 | 23.5 | 17.5 | 0.0031 | 25 | 79 | 1.3 |
| 7 | 1376 | SEE REGRESSION CALCS |  |  |  |  |  |  |
| 8 | 40 | 1600 | 24 | 19 | 0.0031 | 21 | 76 | 1.3 |
| 9 | 638 | SEE REGRESSION CALCS |  |  |  |  |  |  |
| 10 | 4.3 | 1500 | 23.5 | 18.45 | 0.0034 | 19 | 77 | 1.3 |
| 11 | Equilizer Pipe. Refer to Hydraulic Calcs. |  |  |  |  |  |  |  |
| 12 | Equilizer Pipe. Refer to Hydraulic Calcs. |  |  |  |  |  |  |  |
| 13 | 30 | 2000 | 23 | 19.5 | 0.0018 | 31 | 64 | 1.1 |
| 14 | Pond emergency flow. Refer to Hydraulic Calcs. |  |  |  |  |  |  |  |


| Landuse |  | C Values |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Woodlands | Residential | $\mathrm{C}_{2,10}$ | $\mathrm{C}_{25}$ | $\mathrm{C}_{50}$ | $\mathrm{C}_{100}$ |
| 29.9 | 256.1 | 0.38 | 0.42 | 0.45 | 0.47 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| 176.8 | 59.2 | 0.25 | 0.28 | 0.30 | 0.31 |
|  |  |  |  |  |  |
| 60 | 160 | 0.35 | 0.38 | 0.41 | 0.43 |
| 18.5 | 10.5 | 0.27 | 0.30 | 0.33 | 0.34 |
|  |  |  |  |  |  |
| 20 | 20 | 0.30 | 0.33 | 0.36 | 0.38 |
|  |  |  |  |  |  |
| See Not | 1 below | 0.7 | 0.77 | 0.84 | 0.88 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  | 30 | 0.40 | 0.44 | 0.48 | 0.50 |
|  |  |  |  |  |  |

## Notes:

1. Basin 10 is only composed of road right of way; $\mathrm{C}=0.7$
2. Woodlands, pasturs, and grass; $\mathrm{C}=0.2$
3. Single family residential, $1 / 2$ acre lots or larger; $C=0.4$
4. Runoff coefficients have been multiplied by frequency factors for each storm based on Table T-5 of the FDOT Hydrology Handbook, Feb. 2012

## Frequency vs. Discharge Curves

```
Project: SR 514 PDE
Basins: 2, 3 Alt., 5, 6, 8, 10, 13
Designer: CA Estrella
Date: 6/24/2014
```


## Culvert 2

| Year | Frequency (\%) | Discharge (cfs) |
| :---: | :---: | :---: | :---: |
| 50 | 2 | 316.03 |
| 100 | 1 | 362.38 |
| 500 | 0.2 | $470.00 \quad$ Frequency vs. Discharge |

## Culvert 3 Alt.



## Frequency vs. Discharge Curves

| Project: | SR 514 PDE |
| :--- | :--- |
| Basins: | 2,3 Alt., 5, 6, 8, 10, 13 |
| Designer: | CA Estrella |
| Date: | $6 / 24 / 2014$ |

Culvert 5

| Year | Frequency (\%) | Discharge (cfs) |  |
| :---: | :---: | :---: | :---: |
| 50 | 2 | 385.78 |  |
| 100 | 1 | 437.87 |  |
| 500 | 0.2 | 558.82 | Use equation generated by charting to obtain $Q$ |



## Culvert 6



## Frequency vs. Discharge Curves

| Project: | SR 514 PDE |
| :--- | :--- |
| Basins: | 2,3 Alt., 5, 6, 8, 10, 13 |
| Designer: | CA Estrella |
| Date: | $6 / 24 / 2014$ |

Culvert 8


Culvert 10

| Year | Frequency (\%) | Discharge (cfs) |
| :---: | :---: | :---: | :---: |
| 50 | 2 | 25.63 |
| 100 | 1 | 28.85 |
| 500 | 0.2 | $36.34 \quad$ Frequency vs. Discharge |

## Frequency vs. Discharge Curves

```
Project: SR 514 PDE
Basins: 2, 3 Alt., 5, 6, 8, 10, 13
Designer: CA Estrella
Date: 6/24/2014
```

Culvert 13


## REGRESSION ANALYSIS - INPUT PARAMETERS

|  | A | B | C | F | G |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Regression Equation Input Values |  |  |  |  |
| 2 | Variable | Description | Range of Applicability |  |  |
| 3 |  |  |  |  |  |
| 4 | $\begin{aligned} & \mathrm{DA} \\ & \mathrm{ST} \end{aligned}$ | Drainage Area Basin Storage | $\begin{aligned} & 0.2 \text { miles }^{2} \text { (120 acres) } 120 \text { a } \\ & 0 \text { to } 34.12 \% \end{aligned}$ | 2,833 miles ${ }^{2}$ |  |
| 5 |  |  |  |  |  |
| 6 |  |  |  |  |  |
| 7 |  |  |  |  |  |
| 8 | Culvert \# | Basin Area (ac) | Basin Area (miles ${ }^{2}$ ) | Basin Storage (ac) | Basin Storage (\%) |
| 9 | 1 | EQUILIZER PIPE. SEE HYDRAULIC CALCS. |  | 0.00 |  |
| 10 | 2 | 286 | 0.45 | 22.17 | 7.75 |
| 11 | 2 Alt. | 852 | 1.33 | 44.08 | 5.17 |
| 12 | 3 | 802 | 1.25 | 31.68 | 3.95 |
| 13 | 3 Alt | 236 | 0.37 | 9.77 | 4.14 |
| 14 | 4 | EQUILIZER PIPE. SEE HYDRAULIC CALCS. |  | 0.00 |  |
| 15 | 5 | SEE RATIONAL METHOD CALCS |  | 17.13 |  |
| 16 | 6 | SEE RATIONAL METHOD CALCS |  | 0.00 |  |
| 17 | 7 | 1376 | 2.15 | 146.46 | 10.64 |
| 18 | 8 | SEE RATIONAL METHOD CALCS |  | 4.40 |  |
| 19 | 9 | 638 | 1.00 | 34.03 | 5.33 |
| 20 | 10 | SEE RATIONAL METHOD CALCS |  | 0.00 |  |
| 21 | 11 | EQUILIZER PIPE. SEE HYDRAULIC CALCS. |  | 0.00 |  |
| 22 | 12 | EQUILIZER PIPE. SEE HYDRAULIC CALCS. |  | 0.00 |  |
| 23 | 13 | SEE RATIONAL METHOD CALCS |  | 0.00 |  |
| 24 | 14 | POND EMERGENCY FLOW. SEE HYDRAULIC CALCS |  | 0.00 |  |
| 25 | N/A |  |  | 7.26 |  |
| 26 | TOTAL | 3,102 | 4.85 | 263.13 |  |

## USGS REGRESSION EQUATIONS FOR NATURAL FLOW CONDITIONS IN FLORIDA: REGION 4

| Project: | SR514 PDE |  |
| :--- | :--- | :--- |
| Basin: <br> Location: <br> Computed by: <br> Date: | Culvert 2 | Brevard County |
| C. Estrella |  |  |
| 6/24/2014 |  |  |$\quad$| Checked by: |
| :--- |
| Date: |


| Range of Applicability of Basin Characteristics: |  |
| :---: | :---: |
| DA | 120 acres to 2,833 miles $^{2}$ |
| ST | 0 to $34.12 \%$ |


| Peak Runoff Equation | Standard <br> Error (\%) | $\mathrm{Q}_{\mathbf{T}}\left(\mathrm{ft}^{3} / \mathbf{s}\right)$ |
| :---: | :---: | :---: |
| $\mathrm{Q}_{2}=171 \mathrm{DA}^{0.628}(\mathrm{ST}+1)^{-0.401}$ | 36.0 | $\mathbf{4 4}$ |
| $\mathrm{Q}_{5}=321 \mathrm{DA}^{0.618}(\mathrm{ST}+1)^{-0.395}$ | 39.0 | $\mathbf{8 4}$ |
| $\mathrm{Q}_{10}=447 \mathrm{DA}^{0.614}(\mathrm{ST}+1)^{-0.396}$ | 43.0 | $\mathbf{1 1 5}$ |
| $\mathrm{Q}_{25}=636 \mathrm{DA}^{0.610}(\mathrm{ST}+1)^{-0.401}$ | 48.0 | $\mathbf{1 6 3}$ |
| $\mathrm{Q}_{50}=797 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.406}$ | 53.0 | $\mathbf{2 0 2}$ |
| $\mathrm{Q}_{100}=975 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.411}$ | 57.0 | $\mathbf{2 4 5}$ |
| $\mathrm{Q}_{200}=1171 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.416}$ | 62.0 | $\mathbf{2 9 1}$ |
| $\mathrm{Q}_{500}=1461 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.424}$ | 69.0 | $\mathbf{3 5 7}$ |

## Calculations and Documentation

Location

1. Drainage Map showing basin area.
2. Calculation of Basin Storage

Attached

Reference: FDOT Hydrology Handbook, Feb. 2012, Table T-13

## USGS REGRESSION EQUATIONS FOR NATURAL FLOW CONDITIONS IN FLORIDA: REGION 4



| Range of Applicability of Basin Characteristics: |  |
| :---: | :---: |
| DA | 120 acres to 2,833 miles $^{2}$ |
| ST | 0 to $34.12 \%$ |


| Peak Runoff Equation | Standard <br> Error (\%) | $\mathrm{Q}_{\mathrm{T}}\left(\mathbf{f t}^{\mathbf{3} / \mathbf{s})}\right.$ |
| :---: | :---: | :---: |
| $\mathrm{Q}_{2}=171 \mathrm{DA}^{0.628}(\mathrm{ST}+1)^{-0.401}$ | 36.0 | $\mathbf{1 0 0}$ |
| $\mathrm{Q}_{5}=321 \mathrm{DA}^{0.618}(\mathrm{ST}+1)^{-0.395}$ | 39.0 | $\mathbf{1 8 9}$ |
| $\mathrm{Q}_{10}=447 \mathrm{DA}^{0.614}(\mathrm{ST}+1)^{-0.396}$ | 43.0 | $\mathbf{2 5 9}$ |
| $\mathrm{Q}_{25}=636 \mathrm{DA}^{0.610}(\mathrm{ST}+1)^{-0.401}$ | 48.0 | 365 |
| $\mathrm{Q}_{50}=797 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.406}$ | 53.0 | 453 |
| $\mathrm{Q}_{100}=975 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.411}$ | 57.0 | $\mathbf{5 4 9}$ |
| $\mathrm{Q}_{200}=1171 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.416}$ | 62.0 | $\mathbf{6 5 3}$ |
| $\mathrm{Q}_{500}=1461 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.424}$ | 69.0 | $\mathbf{8 0 4}$ |

## Calculations and Documentation

Location
Figure 4
Attached

Reference: FDOT Hydrology Handbook, Feb. 2012, Table T-13

## USGS REGRESSION EQUATIONS FOR NATURAL FLOW CONDITIONS IN FLORIDA: REGION 4

| Project: | SR514 PDE |  |
| :--- | :--- | :--- |
| Basin: <br> Location: <br> Computed by: <br> Date: | Culvert 3 | Brevard County |
| C. Estrella |  |  |
| 6/24/2014 |  |  |$\quad$| Checked by: |
| :--- |
| Date: |


| Range of Applicability of Basin Characteristics: |  |
| :---: | :---: |
| DA | 120 acres to 2,833 miles $^{2}$ |
| ST | 0 to $34.12 \%$ |


| Peak Runoff Equation | Standard <br> Error (\%) | $\mathrm{Q}_{\mathbf{T}}\left(\mathrm{ft}^{3} / \mathbf{s}\right)$ |
| :---: | :---: | :---: |
| $\mathrm{Q}_{2}=171 \mathrm{DA}^{0.628}(\mathrm{ST}+1)^{-0.401}$ | 36.0 | $\mathbf{1 0 5}$ |
| $\mathrm{Q}_{5}=321 \mathrm{DA}^{0.618}(\mathrm{ST}+1)^{-0.395}$ | 39.0 | $\mathbf{1 9 8}$ |
| $\mathrm{Q}_{10}=447 \mathrm{DA}^{0.614}(\mathrm{ST}+1)^{-0.396}$ | 43.0 | $\mathbf{2 7 3}$ |
| $\mathrm{Q}_{25}=636 \mathrm{DA}^{0.610}(\mathrm{ST}+1)^{-0.401}$ | 48.0 | $\mathbf{3 8 4}$ |
| $\mathrm{Q}_{50}=797 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.406}$ | 53.0 | $\mathbf{4 7 8}$ |
| $\mathrm{Q}_{100}=975 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.411}$ | 57.0 | 580 |
| $\mathrm{Q}_{200}=1171 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.416}$ | 62.0 | $\mathbf{6 9 1}$ |
| $\mathrm{Q}_{500}=1461 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.424}$ | 69.0 | $\mathbf{8 5 1}$ |

## Calculations and Documentation

Location
Figure 4
Attached

Reference: FDOT Hydrology Handbook, Feb. 2012, Table T-13

## USGS REGRESSION EQUATIONS FOR NATURAL FLOW CONDITIONS IN FLORIDA: REGION 4

| Project: <br> Basin: <br> Location: <br> Computed by: <br> Date: | SR514 PDE <br> Culvert 3 Alt. <br> Brevard County <br> C. Estrella <br> 6/24/2014 | Checked by: Date: |  |
| :---: | :---: | :---: | :---: |
|  | Required Basin Data: |  |  |
|  | Drainage Area (DA) | 0.37 | miles $^{2}$ |
|  | Basin Storage (ST) | 4.14 | \% of total area |


| Range of Applicability of Basin Characteristics: |  |
| :---: | :---: |
| DA | 120 acres to 2,833 miles $^{2}$ |
| ST | 0 to $34.12 \%$ |


| Peak Runoff Equation | Standard <br> Error (\%) | $\mathrm{Q}_{\mathbf{T}}\left(\mathrm{ft}^{3} / \mathbf{s}\right)$ |
| :---: | :---: | :---: |
| $\mathrm{Q}_{2}=171 \mathrm{DA}^{0.628}(\mathrm{ST}+1)^{-0.401}$ | 36.0 | $\mathbf{4 8}$ |
| $\mathrm{Q}_{5}=321 \mathrm{DA}^{0.618}(\mathrm{ST}+1)^{-0.395}$ | 39.0 | $\mathbf{9 2}$ |
| $\mathrm{Q}_{10}=447 \mathrm{DA}^{0.614}(\mathrm{ST}+1)^{-0.396}$ | 43.0 | $\mathbf{1 2 7}$ |
| $\mathrm{Q}_{25}=636 \mathrm{DA}^{0.610}(\mathrm{ST}+1)^{-0.401}$ | 48.0 | $\mathbf{1 8 0}$ |
| $\mathrm{Q}_{50}=797 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.406}$ | 53.0 | $\mathbf{2 2 3}$ |
| $\mathrm{Q}_{100}=975 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.411}$ | 57.0 | $\mathbf{2 7 1}$ |
| $\mathrm{Q}_{200}=1171 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.416}$ | 62.0 | $\mathbf{3 2 3}$ |
| $\mathrm{Q}_{500}=1461 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.424}$ | 69.0 | $\mathbf{3 9 8}$ |

## Calculations and Documentation

Location
Figure 4
Attached

Reference: FDOT Hydrology Handbook, Feb. 2012, Table T-13

## USGS REGRESSION EQUATIONS FOR NATURAL FLOW CONDITIONS IN FLORIDA: REGION 4



| Range of Applicability of Basin Characteristics: |  |
| :---: | :---: |
| DA | 120 acres to 2,833 miles $^{2}$ |
| ST | 0 to $34.12 \%$ |


| Peak Runoff Equation | Standard <br> Error (\%) | $\mathrm{Q}_{\mathbf{T}}\left(\mathrm{ft}^{3} / \mathbf{s}\right)$ |
| :---: | :---: | :---: |
| $\mathrm{Q}_{2}=171 \mathrm{DA}^{0.628}(\mathrm{ST}+1)^{-0.401}$ | 36.0 | $\mathbf{1 0 5}$ |
| $\mathrm{Q}_{5}=321 \mathrm{DA}^{0.618}(\mathrm{ST}+1)^{-0.395}$ | 39.0 | 197 |
| $\mathrm{Q}_{10}=447 \mathrm{DA}^{0.614}(\mathrm{ST}+1)^{-0.396}$ | 43.0 | $\mathbf{2 7 1}$ |
| $\mathrm{Q}_{25}=636 \mathrm{DA}^{0.610}(\mathrm{ST}+1)^{-0.401}$ | 48.0 | $\mathbf{3 7 9}$ |
| $\mathrm{Q}_{50}=797 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.406}$ | 53.0 | 469 |
| $\mathrm{Q}_{100}=975 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.411}$ | 57.0 | 566 |
| $\mathrm{Q}_{200}=1171 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.416}$ | 62.0 | $\mathbf{6 7 2}$ |
| $\mathrm{Q}_{500}=1461 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.424}$ | 69.0 | $\mathbf{8 2 2}$ |

## Calculations and Documentation

Location
Figure 4
Attached

Reference: FDOT Hydrology Handbook, Feb. 2012, Table T-13

## USGS REGRESSION EQUATIONS FOR NATURAL FLOW CONDITIONS IN FLORIDA: REGION 4

| Project: | SR514 PDE |  |
| :--- | :--- | :--- |
| Basin: <br> Location: <br> Computed by: <br> Date: | Culvert 9 | Brevard County |
| C. Estrella |  |  |
| 6/24/2014 |  |  |$\quad$| Checked by: |
| :--- |
| Date: |


| Range of Applicability of Basin Characteristics: |  |
| :---: | :---: |
| DA | 120 acres to 2,833 miles $^{2}$ |
| ST | 0 to $34.12 \%$ |


| Peak Runoff Equation | Standard <br> Error (\%) | $\mathrm{Q}_{\mathbf{T}}\left(\mathrm{ft}^{3} / \mathbf{s}\right)$ |
| :---: | :---: | :---: |
| $\mathrm{Q}_{2}=171 \mathrm{DA}^{0.628}(\mathrm{ST}+1)^{-0.401}$ | 36.0 | $\mathbf{8 2}$ |
| $\mathrm{Q}_{5}=321 \mathrm{DA}^{0.618}(\mathrm{ST}+1)^{-0.395}$ | 39.0 | 156 |
| $\mathrm{Q}_{10}=447 \mathrm{DA}^{0.614}(\mathrm{ST}+1)^{-0.396}$ | 43.0 | $\mathbf{2 1 5}$ |
| $\mathrm{Q}_{25}=636 \mathrm{DA}^{0.610}(\mathrm{ST}+1)^{-0.401}$ | 48.0 | $\mathbf{3 0 3}$ |
| $\mathrm{Q}_{50}=797 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.406}$ | 53.0 | $\mathbf{3 7 6}$ |
| $\mathrm{Q}_{100}=975 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.411}$ | 57.0 | $\mathbf{4 5 6}$ |
| $\mathrm{Q}_{200}=1171 \mathrm{DA}^{0.608}(\mathrm{ST}+1)^{-0.416}$ | 62.0 | $\mathbf{5 4 2}$ |
| $\mathrm{Q}_{500}=1461 \mathrm{DA}^{0.609}(\mathrm{ST}+1)^{-0.424}$ | 69.0 | $\mathbf{6 6 7}$ |

## Calculations and Documentation

Location
Figure 4
Attached

Reference: FDOT Hydrology Handbook, Feb. 2012, Table T-13


# Table T-4 <br> Runoff Coefficients for a Design Storm Return Period of 10 Years or Less ${ }^{\text {a }}$ 

| Slope | Land Use | Sandy Soils |  | Clay Soils |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Max. | Min. | Max. |
| $\begin{aligned} & \text { Flat } \\ & \text { (0-2\%) } \end{aligned}$ | Woodlands | 0.10 | 0.15 | 0.15 | 0.20 |
|  | Pasture, grass, and farmland ${ }^{\text {b }}$ | 0.15 | 0.20 | 0.20 | 0.25 |
|  | Bare Earth | 0.30 | 0.50 | 0.50 | 0.60 |
|  | Rooftops and pavement | 0.95 | 0.95 | 0.95 | 0.95 |
|  | Pervious pavements ${ }^{\text {c }}$ | 0.75 | 0.95 | 0.90 | 0.95 |
|  | SFR: 1/2-acre lots and larger | 0.30 | 0.35 | 0.35 | 0.45 |
|  | Smaller lots | 0.35 | 0.45 | 0.40 | 0.50 |
|  | Duplexes | 0.35 | 0.45 | 0.40 | 0.50 |
|  | MFR:Apartments, townhouses, and condominiums | 0.45 | 0.60 | 0.50 | 0.70 |
|  | Commercial and Industrial | 0.50 | 0.95 | 0.50 | 0.95 |
| $\begin{aligned} & \text { Rolling } \\ & \text { (2-7\%) } \end{aligned}$ | Woodlands | 0.15 | 0.20 | 0.20 | 0.25 |
|  | Pasture, grass, and farmland ${ }^{\text {b }}$ | 0.20 | 0.25 | 0.25 | 0.30 |
|  | Bare Earth | 0.40 | 0.60 | 0.60 | 0.70 |
|  | Rooftops and pavement | 0.95 | 0.95 | 0.95 | 0.95 |
|  | Pervious pavements ${ }^{\text {c }}$ | 0.80 | 0.95 | 0.90 | 0.95 |
|  | SFR: 1/2-acre lots and larger | 0.35 | 0.50 | 0.40 | 0.55 |
|  | Smaller lots | 0.40 | 0.55 | 0.45 | 0.60 |
|  | Duplexes | 0.40 | 0.55 | 0.45 | 0.60 |
|  | MFR:Apartments, townhouses, and condominiums | 0.50 | 0.70 | 0.60 | 0.80 |
|  | Commercial and Industrial | 0.50 | 0.95 | 0.50 | 0.95 |
| $\begin{aligned} & \text { Steep } \\ & (7 \%+) \end{aligned}$ | Woodlands | 0.20 | 0.25 | 0.25 | 0.30 |
|  | Pasture, grass, and farmland ${ }^{\text {b }}$ | 0.25 | 0.35 | 0.30 | 0.40 |
|  | Bare Earth | 0.50 | 0.70 | 0.70 | 0.80 |
|  | Rooftops and pavement | 0.95 | 0.95 | 0.95 | 0.95 |
|  | Pervious pavements ${ }^{\text {c }}$ | 0.85 | 0.95 | 0.90 | 0.95 |
|  | SFR: 1/2-acre lots and larger | 0.40 | 0.55 | 0.50 | 0.65 |
|  | Smaller lots | 0.45 | 0.60 | 0.55 | 0.70 |
|  | Duplexes | 0.45 | 0.60 | 0.55 | 0.70 |
|  | MFR:Apartments, townhouses, and condominiums | 0.60 | 0.75 | 0.65 | 0.85 |
|  | Commercial and Industrial | 0.60 | 0.95 | 0.65 | 0.95 |

[^1]TOPIC NO. 625-040-002-A
dRainage manual
APPENDIX B- IDF CURVES

ZONES FOR PRECIPITATION IDF CURVES DEVELOPED BY THE DEPARTMENT



# Table T-5 <br> Design Storm Frequency Factors for Pervious Area Runoff Coefficients * 

| Return Period (years) | Design Storm <br> Frequency Factor, $X_{I}$ |
| :---: | :---: |
| 2 to 10 | 1.0 |
| 25 | 1.1 |
| 50 | 1.2 |
| 100 | 1.25 |

Reference: Wright-McLaughlin Engineers (1969).

* DUE TO THE INCREASE IN THE DURATION TIME THAT THE PEAK OR NEAR PEAK DISCHARGE RATE IS RELEASED FROM STORMWATER MANAGEMENT SYSTEMS, THE USE OF THESE SHORT DURATION PEAK RATE DISCHARGE ADJUSTMENT FACTORS IS NOT APPROPRIATE FOR FLOOD ROUTING COMPUTATIONS.


# Table T-19 <br> Department Intensity-Duration-Frequency (IDF) <br> Regression Equation Constants and Coefficients 

## (Page 2 of 3)

|  |  | Polynomial Coefficients <br> for a Third Degree Polynomial |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rainfall Zone | Storm Frequency in Years | A | B | C | D |
| 6 | 2 | 14.09519 | -4.17207 | 0.31773 | 0.00029 |
| 6 | 3 | 14.98331 | -4.44963 | 0.35683 | -0.00224 |
| 6 | 5 | 14.54762 | -3.89935 | 0.22564 | 0.00674 |
| 6 | 10 | 14.35386 | -3.10140 | -0.01003 | 0.02525 |
| 6 | 25 | 16.15961 | -3.48135 | -0.00160 | 0.02677 |
| 6 | 50 | 15.67671 | -2.52635 | -0.26055 | 0.04609 |
| 7 | 2 | 12.10821 | -2.79255 | 0.02002 | 0.02053 |
| 7 | 3 | 12.43560 | -2.56458 | -0.06903 | 0.02787 |
| 7 | 5 | 12.51872 | -2.17764 | -0.19805 | 0.03849 |
| 7 | 10 | 12.49556 | -1.67116 | -0.34901 | 0.05017 |
| 7 | 25 | 12.92209 | -1.11084 | -0.55019 | 0.06666 |
| 7 | 50 | 13.29550 | -0.70432 | -0.70152 | 0.07933 |
| 8 | 2 | 11.51282 | -2.10568 | -0.16578 | 0.03515 |
| 8 | 3 | 11.13440 | -1.44999 | -0.34027 | 0.04808 |
| 8 | 5 | 11.41155 | -1.34465 | -0.38409 | 0.05149 |
| 8 | 10 | 11.54908 | -0.89694 | -0.53000 | 0.06319 |
| 8 | 25 | 10.92111 | 0.51710 | -0.93480 | 0.09473 |
| 8 | 50 | 11.58787 | 0.73605 | -1.04111 | 0.10384 |
| 9 | 2 | 11.08062 | -1.66022 | -0.28464 | 0.04453 |
| 9 | 3 | 11.54667 | -1.49353 | -0.35960 | 0.05071 |
| 9 | 5 | 11.76664 | -1.38391 | -0.39880 | 0.05352 |
| 9 | 10 | 12.08400 | -1.00328 | -0.53661 | 0.06491 |
| 9 | 25 | 12.38592 | -0.27352 | -0.77352 | 0.08370 |
| 9 | 50 | 14.16172 | -0.73486 | -0.75377 | 0.08518 |
| 10 | 2 | 11.33384 | -1.86569 | -0.22813 | 0.04005 |
| 10 | 3 | 11.32916 | -1.38557 | -0.36672 | 0.05012 |
| 10 | 5 | 11.19083 | -0.93165 | -0.48526 | 0.05836 |
| 10 | 10 | 10.84265 | -0.18976 | -0.69575 | 0.07495 |
| 10 | 25 | 11.83969 | 0.09353 | -0.84451 | 0.08783 |
| 10 | 50 | 11.59208 | 1.00204 | -1.10384 | 0.10762 |


|  | K | L | M | N | O | P | Q | R | S | T | U |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Storage Area Table |  |  |  |  |  |  |  |  |  |  |
| 2 | The regression equations for natural flow conditions are being used to estimate the Q at some of the culverts across SR514. |  |  |  |  |  |  |  |  |  |  |
| 3 | developlment conditions. |  |  |  |  |  |  |  |  |  |  |
| 5 | Area ID Area (ac) Main Culvert |  |  | Alt. Culvert |  |  |  |  |  |  |  |
| 6 | 9962 | 4.73 | 2 | 2 |  |  |  |  |  |  |  |
| 7 |  | 0.80 | 2 | 2 |  |  |  |  |  |  |  |
| 8 | 9964 | 1.92 | 2 | 2 |  |  |  |  |  |  |  |
| 9 | 9965 | 11.62 | 2 | 2 |  |  |  |  |  |  |  |
| 10 | 9966 | 0.57 | 3 | 2 |  |  |  |  |  |  |  |
| 11 | 9967 | 2.20 | 3 | 2 |  |  |  |  |  |  |  |
| 12 | 9968 | 0.80 | 3 | 2 |  |  |  |  |  |  |  |
| 13 | 9969 | 6.12 | 3 | 2 |  |  |  |  |  |  |  |
| 14 | 9970 | 1.00 | 2 | 2 |  |  |  |  |  |  |  |
| 15 | 9971 | 2.10 | 2 | 2 |  |  |  |  |  |  |  |
| 16 | 9972 | 4.52 | 3 | 2 |  |  |  |  |  |  |  |
| 17 | 9973 | 1.34 | 3 | 3 |  |  |  |  |  |  |  |
| 18 | 9974 | 3.69 | 3 | 3 |  |  |  |  |  |  |  |
| 19 | 9975 | 2.59 | 3 | 3 |  |  |  |  |  |  |  |
| 20 | 9976 | 6.32 | 5 | 5 |  |  |  |  |  |  |  |
| 21 | 9977 | 3.70 | 5 | 5 |  |  |  |  |  |  |  |
| 22 | 9978 | 4.61 | 5 | 5 |  |  |  |  |  |  |  |
| 23 | 9979 | 2.50 | 5 | 5 |  |  |  |  |  |  |  |
| 24 | 9980 | 3.98 | 7 | 7 |  |  |  |  |  |  |  |
| 25 | 9981 | 2.15 | 3 | 3 |  |  |  |  |  |  |  |
| 26 | 9982 | 1.30 | 3 | 2 |  |  |  |  |  |  |  |
| 27 | 9983 | 1.03 | 3 | 2 |  |  |  |  |  |  |  |
| 28 | 9984 | 2.47 | 3 | 2 |  |  |  |  |  |  |  |
| 29 | 9985 | 2.90 | 3 | 2 |  |  |  |  |  |  |  |
| 30 | 9986 | 3.48 | 7 | 7 |  |  |  |  |  |  |  |
| 31 | 9987 | 0.97 | 7 | 7 |  |  |  |  |  |  |  |
| 32 | 9988 | 1.76 | 7 | 7 |  |  |  |  |  |  |  |
| 33 | 9989 | 4.08 | 7 | 7 |  |  |  |  |  |  |  |
| 34 | 9990 | 0.77 | 7 | 7 |  |  |  |  |  |  |  |
| 35 | 9991 | 2.40 | 7 | 7 |  |  |  |  |  |  |  |
| 36 | 9992 | 18.55 | 7 | 7 |  |  |  |  |  |  |  |
| 37 | 9993 | 1.78 | 7 | 7 |  |  |  |  |  |  |  |
| 38 | 9994 | 3.33 | 7 | 7 |  |  |  |  |  |  |  |
| 39 | 9995 | 10.73 | 7 | 7 |  |  |  |  |  |  |  |
| 40 | 9996 | 0.57 | 7 | 7 |  |  |  |  |  |  |  |
| 41 | 9997 | 1.54 | 7 | 7 |  |  |  |  |  |  |  |
| 42 | 9998 | 1.34 | 7 | 7 |  |  |  |  |  |  |  |
| 43 | 9999 | 0.54 | 7 | 7 |  |  |  |  |  |  |  |
| 44 | 10000 | 1.34 | 7 | 7 |  |  |  |  |  |  |  |
| 45 | 10001 | 1.86 | 7 | 7 |  |  |  |  |  |  |  |
| 46 | 10002 | 3.51 | 7 | 7 |  |  |  |  |  |  |  |
| 47 | 10003 | 1.85 | 7 | 7 |  |  |  |  |  |  |  |
| 48 | 10004 | 9.38 | 7 | 7 |  |  |  |  |  |  |  |
| 49 | 10005 | 0.46 | 7 | 7 |  |  |  |  |  |  |  |
| 50 | 10006 | 4.98 | 7 | 7 |  |  |  |  |  |  |  |
| 51 | 10007 | 22.37 | 7 | 7 |  |  |  |  |  |  |  |
| 52 | 10008 | 0.86 | 7 | 7 |  |  |  |  |  |  |  |
| 53 | 10009 | 12.30 | 7 | 7 |  |  |  |  |  |  |  |
| 54 | 10010 | 5.46 | 7 | 7 |  |  |  |  |  |  |  |
| 55 | 10011 | 1.28 | 7 | 7 |  |  |  |  |  |  |  |
| 56 | 10012 | 13.25 | 7 | 7 |  |  |  |  |  |  |  |
| 57 | 10013 | 3.24 | 7 | 7 |  |  |  |  |  |  |  |
| 58 | 10014 | 8.50 | 7 | 7 |  |  |  |  |  |  |  |
| 59 | 10015 | 3.15 | 9 | 9 |  |  |  |  |  |  |  |
| 60 | 10016 | 5.73 | 9 | 9 |  |  |  |  |  |  |  |
| 61 | 10017 | 2.37 | 9 | 9 |  |  |  |  |  |  |  |
| 62 | 10018 | 12.34 | 9 | 9 |  |  |  |  |  |  |  |
| 63 | 10019 | 1.43 | 9 | 9 |  |  |  |  |  |  |  |
| 64 | 10020 | 0.87 | 8 | 8 |  |  |  |  |  |  |  |
| 65 | 10021 | 0.00 | N/A | NA |  |  |  |  |  |  |  |
| 66 | 10022 | 1.25 | 8 | 8 |  |  |  |  |  |  |  |
| 67 | 10023 | 0.87 | 8 | 8 |  |  |  |  |  |  |  |
| 68 | 10024 | 1.41 | 8 | 8 |  |  |  |  |  |  |  |
| 69 | 10025 | 3.32 | 9 | 9 |  |  |  |  |  |  |  |
| 70 | 10026 | 0.59 | 9 | 9 |  |  |  |  |  |  |  |
| 71 | 10027 | 1.01 | 9 | 9 |  |  |  |  |  |  |  |
| 72 | 10028 | 4.09 | 9 | 9 |  |  |  |  |  |  |  |
| 73 | 10029 | 2.22 | N/A | N/A |  |  |  |  |  |  |  |
| 74 | 10030 | 1.29 | N/A | N/A |  |  |  |  |  |  |  |
| 75 | 10031 | 0.65 | N/A | N/A |  |  |  |  |  |  |  |
| 76 | 10032 | 3.10 | N/A | N/A |  |  |  |  |  |  |  |
| 77 |  |  |  |  |  |  |  |  |  |  |  |
| 78 | TOTAL | 263.13 |  |  |  |  |  |  |  |  |  |

## F-4 Regions for USGS Regression Equations for Natural Flow Conditions in Florida



## Table T-13 <br> USGS Regression Equations for Natural Flow Conditions in Florida - Region 4

Peak Runoff Equation
Standard Error of Prediction (\%)
$\mathrm{Q}_{2}=171 \mathrm{~A}^{0.628}(\mathrm{ST}+1)^{-0.401} \quad 36$
$\mathrm{Q}_{5}=321 \mathrm{~A}^{0.618}(\mathrm{ST}+1)^{-0.395} \quad 39$
$\mathrm{Q}_{10}=447 \mathrm{~A}^{0.614}(\mathrm{ST}+1)^{-0.396} \quad 43$
$\mathrm{Q}_{25}=636 \mathrm{~A}^{0.610}(\mathrm{ST}+1)^{-0.401} 48$
$\mathrm{Q}_{50}=797 \mathrm{~A}^{0.609}(\mathrm{ST}+1)^{-0.406} \quad 53$
$\mathrm{Q}_{100}=975 \mathrm{~A}^{0.608}(\mathrm{ST}+1)^{-0.411} 57$
$\mathrm{Q}_{200}=1171 \mathrm{~A}^{0.608}(\mathrm{ST}+1)^{-0.416} 62$
$\mathrm{Q}_{500}=1461 \mathrm{~A}^{0.609}(\mathrm{ST}+1)^{-0.424} 69$
$\mathrm{Q}_{\mathrm{T}}=$ Peak runoff rate for return period of T-years, in cfs
$\mathrm{A}=$ Drainage area, in miles ${ }^{2}$
$\mathrm{ST}=$ Basin storage, the percentage of the drainage basin occupied by lakes, reservoirs, swamps, and wetland. In-channel storage of a temporary nature, resulting from computation of ST

Basin Characteristic
Drainage Area (A)
miles $^{2}$
Storage Area (ST)
Reference: Verdi (2006)
See Figure F-4 for zone delineation.

| Existing c prelimina proposed crossing. Proposed | nditions for culvert siz pipe is sized able below Conditions. | he proje for Prop o match ummarie | t's culve osed Co or reduc s the res | rts have ditions. e the esti ults of th | een analyz ased upon mated 50-y calculatio | d to help de available data ar headwat s for Existing | ermine a , the at each and |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 50 yr |  | Existing | oposed |
| Ex. Size | Prop. Size | Culvert | Q (cfs) | Pre HW | Post HW | Road CL EL | Road CL EL |
| $24 "$ | 30" | 1 | 23 | 24.16 | 23.31 | 24.34 | 25.25 |
| $8 \times 4$ | $8 \times 4$ | 2 | 316 | 24.12 | 24.12 | 24.31 | 25.58 |
| $8 \times 4$ | (2) $6 \times 4$ | 2 Alt | 453 | 24.64 | 23.78 | 24.31 | 25.58 |
| 10x3 | (2) $8 \times 4$ | 3 | 478 | 21.23 | 20.93 | 20.84 | 24.02 |
| 10x3 | $10 \times 3$ | 3 Alt | 218 | 20.40 | 20.49 | 20.84 | 24.02 |
| 24" | 30" | 4 | 20 | 19.86 | 19.21 | 20.46 | 24.66 |
| (2) $8 \times 3$ | (2) $8 \times 4$ | 5 | 386 | 17.24 | 16.86 | 18.3 | 22.98 |
| 30" | (2) 30 " | 6 | 61 | 19.56 | 19.11 | 19.4 | 23.06 |
| $8 \times 4$ | (2) $6 \times 4$ | 7 | 469 | 21.42 | 21.46 | 21.08 | 23.62 |
| $24 "$ | (2) 36 " | 8 | 99 | 22.13 | 21.42 | 21.76 | 25.65 |
| 10x5 | 10x5 | 9 | 376 | 19.06 | 19.06 | 21.07 | 25.01 |
| 24" | 30" | 10 | 25.6 | 22.41 | 21.43 | 22.9 | 22.9 |
| $24 "$ | $24 "$ | 11 | 10 | 22.31 | 22.35 | 24.07 | 24.07 |
| 24" | 30" | 12 | 10 | 21.64 | 21.51 | 23.97 | 23.97 |
| 24" | $36 "$ | 13 | 83 | 24.08 | 24.48 | 23.8 | 24.5 |
| 18" | $24 "$ | 14 | 10 | 23.62 | 22.94 | 25 | 25 |

Culvert \#13 is part of the storm sewer system east of Marie Street. Results for existing conditions indicate overtopping of roadway where no problems are reported. Either runoff shifts to nearby inlet or basin area is different than assumed. Large pipe for proposed condition assumes downstream portion of storm sewer system is upsized to handle. Roadway profile affects peak stage if overtopping is present.

# PRELIMINARY SIZING OF PROPOSED CROSSDRAINS 

## - EXISTING CULVERTS

EXISTING CULVERTS HAVE BEEN PRELIMINARILY ANALYZED USING BEST AVAILABLE DATA:
A) SURVEY OF INVERTS AND PIPE SIZES WERE OBTAINED FOR CULVERTS 2,3,5,6,7,8,9,10,11,12
B) FLOWLINES FOR OTHER CULVERTS (1,4,13, AND 14) WERE OBTAINED FROM VARIOUS CONSTRUCTION PLANS (SPN 7080-3506 AND SJRWMD ERP DATA)

## HY-8 Culvert Analysis Report EXISTING CULVERT 1

Table 1 - Summary of Culvert Flows at Crossing: Culvert 1-24" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 01 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 23.48 | 18.00 | 18.00 | 0.00 | 1 |
| 23.57 | 18.80 | 18.80 | 0.00 | 1 |
| 23.68 | 19.60 | 19.60 | 0.00 | 1 |
| 23.78 | 20.40 | 20.40 | 0.00 | 1 |
| 23.89 | 21.20 | 21.20 | 0.00 | 1 |
| 24.01 | 22.00 | 22.00 | 0.00 | 1 |
| 24.13 | 22.80 | 22.80 | 0.00 | 1 |
| 24.16 | 23.00 | 23.00 | 0.00 | 1 |
| 24.34 | 24.40 | 24.20 | 0.09 | 34 |
| 24.36 | 25.20 | 24.29 | 0.78 | 5 |
| 24.37 | 26.00 | 24.36 | 1.52 | 4 |
| 24.34 | 24.17 | 24.17 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 1-24" RCP


Table 2 - Culvert Summary Table: Culvert 01

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18.00 | 18.00 | 23.48 | 2.645 | 2.956 | $4-\mathrm{FFf}$ | 2.000 | 1.523 | 2.000 | 2.000 | 5.730 | 0.000 |
| 18.80 | 18.80 | 23.57 | 2.760 | 3.053 | $4-\mathrm{FFf}$ | 2.000 | 1.556 | 2.000 | 2.000 | 5.984 | 0.000 |
| 19.60 | 19.60 | 23.68 | 2.880 | 3.155 | $4-\mathrm{FFf}$ | 2.000 | 1.590 | 2.000 | 2.000 | 6.239 | 0.000 |
| 20.40 | 20.40 | 23.78 | 3.005 | 3.262 | $4-\mathrm{FFf}$ | 2.000 | 1.617 | 2.000 | 2.000 | 6.494 | 0.000 |
| 21.20 | 21.20 | 23.89 | 3.136 | 3.372 | $4-\mathrm{FFf}$ | 2.000 | 1.640 | 2.000 | 2.000 | 6.748 | 0.000 |
| 22.00 | 22.00 | 24.01 | 3.272 | 3.487 | $4-\mathrm{FFf}$ | 2.000 | 1.664 | 2.000 | 2.000 | 7.003 | 0.000 |
| 22.80 | 22.80 | 24.13 | 3.414 | 3.606 | $4-\mathrm{FFf}$ | 2.000 | 1.687 | 2.000 | 2.000 | 7.257 | 0.000 |
| 23.00 | 23.00 | 24.16 | 3.451 | 3.636 | $4-\mathrm{FFf}$ | 2.000 | 1.693 | 2.000 | 2.000 | 7.321 | 0.000 |
| 24.40 | 24.20 | 24.34 | 3.677 | 3.824 | $4-\mathrm{FFf}$ | 2.000 | 1.728 | 2.000 | 2.000 | 7.702 | 0.000 |
| 25.20 | 24.29 | 24.36 | 3.695 | 3.839 | $4-\mathrm{FFf}$ | 2.000 | 1.731 | 2.000 | 2.000 | 7.732 | 0.000 |
| 26.00 | 24.36 | 24.37 | 3.708 | 3.850 | $4-\mathrm{FFf}$ | 2.000 | 1.733 | 2.000 | 2.000 | 7.754 | 0.000 |

Inlet Elevation (invert): $20.52 \mathrm{ft}, \quad$ Outlet Elevation (invert): 20.40 ft
Culvert Length: $58.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0021


## Culvert Performance Curve Plot: Culvert 01

Performance Curve
Culvert: Culvert 01


Water Surface Profile Plot for Culvert: Culvert 01
Crossing - Culvert 1-24" RCP, Design Discharge - 23.0 cfs
Culvert - Culvert 01, Culvert Discharge - 23.0 cfs


## Site Data - Culvert 01

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 20.52 ft
Outlet Station: 58.00 ft
Outlet Elevation: 20.40 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 01

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 1-24" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 18.00 | 22.40 | 2.00 |
| 18.80 | 22.40 | 2.00 |
| 19.60 | 22.40 | 2.00 |
| 20.40 | 22.40 | 2.00 |
| 21.20 | 22.40 | 2.00 |
| 22.00 | 22.40 | 2.00 |
| 22.80 | 22.40 | 2.00 |
| 23.00 | 22.40 | 2.00 |
| 24.40 | 22.40 | 2.00 |
| 25.20 | 22.40 | 2.00 |
| 26.00 | 22.40 | 2.00 |

Tailwater Channel Data - Culvert 1-24" RCP
Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 22.40 ft

## Roadway Data for Crossing: Culvert 1-24" RCP

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 24.34 ft
Roadway Surface: Paved
Roadway Top Width: 36.00 ft

## HY-8 Culvert Analysis Report

EXISTING CULVERT 2

Table 1 - Summary of Culvert Flows at Crossing: Culvert 02

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 02 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 02
Total Rating Curve
Crossing: Culvert 02


Table 2 - Culvert Summary Table: Culvert 02

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 207.00 | 207.00 | 21.83 | 4.746 | 4.723 | 2-M2c | 4.000 | 2.756 | 2.748 | 2.160 | 9.414 | 0.000 |
| 233.30 | 233.30 | 22.32 | 5.236 | 5.114 | 2-M2c | 4.000 | 2.984 | 2.976 | 2.370 | 9.799 | 0.000 |
| 259.60 | 259.60 | 22.84 | 5.761 | 5.491 | 2-M2c | 4.000 | 3.205 | 3.195 | 2.570 | 10.157 | 0.000 |
| 285.90 | 285.90 | 23.41 | 6.330 | 5.856 | 2-M2c | 4.000 | 3.418 | 3.409 | 2.770 | 10.482 | 0.000 |
| 312.20 | 312.20 | 24.03 | 6.949 | 6.331 | 7-M2c | 4.000 | 3.624 | 3.615 | 2.970 | 10.795 | 0.000 |
| 316.00 | 316.00 | 24.12 | 7.043 | 6.406 | 7-M2c | 4.000 | 3.653 | 3.644 | 2.990 | 10.838 | 0.000 |
| 364.80 | 329.35 | 24.46 | 7.382 | 6.738 | $4-\mathrm{FFf}$ | 4.000 | 3.756 | 4.000 | 4.030 | 10.292 | 0.000 |
| 391.10 | 331.75 | 24.52 | 7.444 | 6.778 | $4-\mathrm{FFf}$ | 4.000 | 3.774 | 4.000 | 4.030 | 10.367 | 0.000 |
| 417.40 | 333.85 | 24.58 | 7.499 | 6.813 | $4-\mathrm{FFf}$ | 4.000 | 3.790 | 4.000 | 4.030 | 10.433 | 0.000 |
| 443.70 | 335.71 | 24.63 | 7.548 | 6.845 | $4-\mathrm{FFf}$ | 4.000 | 3.804 | 4.000 | 4.030 | 10.491 | 0.000 |
| 470.00 | 337.45 | 24.67 | 7.595 | 6.875 | $4-\mathrm{FFf}$ | 4.000 | 3.817 | 4.000 | 4.030 | 10.545 | 0.000 |

Inlet Elevation (invert): $17.08 \mathrm{ft}, \quad$ Outlet Elevation (invert): 17.03 ft
Culvert Length: $62.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0008
$\qquad$

## Culvert Performance Curve Plot: Culvert 02

Performance Curve
Culvert: Culvert 02



## Site Data - Culvert 02

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 17.08 ft
Outlet Station: 62.00 ft
Outlet Elevation: 17.03 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 02

Barrel Shape: Concrete Box
Barrel Span: 8.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 02)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 207.00 | 19.19 | 2.16 |
| 233.30 | 19.40 | 2.37 |
| 259.60 | 19.60 | 2.57 |
| 285.90 | 19.80 | 2.77 |
| 312.20 | 20.00 | 2.97 |
| 316.00 | 20.02 | 2.99 |
| 364.80 | 21.06 | 4.03 |
| 391.10 | 21.06 | 4.03 |
| 417.40 | 21.06 | 4.03 |
| 443.70 | 21.06 | 4.03 |
| 470.00 | 21.06 | 4.03 |

## Tailwater Channel Data - Culvert 02

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 02

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 24.31 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report <br> EXISTING CULVERT 2 ALT

Table 1 - Summary of Culvert Flows at Crossing: Culvert 02 Alt.

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 02 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 02 Alt.
Total Rating Curve
Crossing: Culvert 02 Alt.


Table 2 - Culvert Summary Table: Culvert 02

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100.00 | 100.00 | 20.01 | 2.871 | 2.926 | 3-M2t | 2.612 | 1.697 | 1.990 | 1.990 | 6.281 | 0.000 |
| 170.40 | 170.40 | 21.23 | 4.104 | 4.149 | 2-M2c | 4.000 | 2.420 | 2.413 | 2.170 | 8.827 | 0.000 |
| 240.80 | 240.80 | 22.46 | 5.382 | 5.223 | 2-M2c | 4.000 | 3.048 | 3.039 | 2.370 | 9.904 | 0.000 |
| 311.20 | 311.20 | 24.00 | 6.925 | 6.312 | 7-M2c | 4.000 | 3.616 | 3.607 | 2.570 | 10.783 | 0.000 |
| 381.60 | 330.93 | 24.50 | 7.423 | 6.695 | 7-M2c | 4.000 | 3.768 | 3.758 | 2.770 | 11.007 | 0.000 |
| 452.00 | 336.27 | 24.64 | 7.563 | 6.797 | 7-M2c | 4.000 | 3.808 | 3.798 | 2.990 | 11.066 | 0.000 |
| 453.00 | 336.32 | 24.64 | 7.565 | 6.798 | 7-M2c | 4.000 | 3.808 | 3.799 | 2.990 | 11.067 | 0.000 |
| 592.80 | 344.41 | 24.86 | 7.782 | 6.996 | $4-\mathrm{FFf}$ | 4.000 | 3.869 | 4.000 | 4.030 | 10.763 | 0.000 |
| 663.20 | 347.88 | 24.96 | 7.876 | 7.056 | $4-\mathrm{FFf}$ | 4.000 | 3.895 | 4.000 | 4.030 | 10.871 | 0.000 |
| 733.60 | 351.10 | 25.05 | 7.965 | 7.114 | $4-\mathrm{FFf}$ | 4.000 | 3.919 | 4.000 | 4.030 | 10.972 | 0.000 |
| 804.00 | 354.09 | 25.13 | 8.049 | 7.167 | $4-\mathrm{FFf}$ | 4.000 | 3.942 | 4.000 | 4.030 | 11.065 | 0.000 |

Inlet Elevation (invert): $17.08 \mathrm{ft}, \quad$ Outlet Elevation (invert): 17.03 ft
Culvert Length: $62.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0008
*****************************************************************************************)

## Culvert Performance Curve Plot: Culvert 02

Performance Curve
Culvert: Culvert 02


Water Surface Profile Plot for Culvert: Culvert 02

## Crossing - Culvert 02 Alt., Design Discharge - 453.0 cfs

Culvert - Culvert 02, Culvert Discharge - 336.3 cfs


## Site Data - Culvert 02

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 17.08 ft
Outlet Station: 62.00 ft
Outlet Elevation: 17.03 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 02

Barrel Shape: Concrete Box
Barrel Span: 8.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 02 Alt.)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 100.00 | 19.02 | 1.99 |
| 170.40 | 19.20 | 2.17 |
| 240.80 | 19.40 | 2.37 |
| 311.20 | 19.60 | 2.57 |
| 381.60 | 19.80 | 2.77 |
| 452.00 | 20.02 | 2.99 |
| 453.00 | 20.02 | 2.99 |
| 592.80 | 21.06 | 4.03 |
| 663.20 | 21.06 | 4.03 |
| 733.60 | 21.06 | 4.03 |
| 804.00 | 21.06 | 4.03 |

## Tailwater Channel Data - Culvert 02 Alt.

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 02 Alt.

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 24.31 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

 EXISTING CULVERT 3Table 1 - Summary of Culvert Flows at Crossing: Culvert 03

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 03 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 03
Total Rating Curve
Crossing: Culvert 03


Table 2 - Culvert Summary Table: Culvert 03

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> (cfs) | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 105.00 | 105.00 | 18.46 | 2.548 | 2.870 | 3-M1t | 1.744 | 1.510 | 2.570 | 2.570 | 4.086 | 0.000 |
| 179.60 | 179.60 | 19.34 | 3.754 | 3.706 | 7-M1t | 2.514 | 2.160 | 2.570 | 2.570 | 6.988 | 0.000 |
| 254.20 | 253.64 | 20.80 | 5.214 | 4.709 | 7-M2c | 3.000 | 2.719 | 2.713 | 2.570 | 9.351 | 0.000 |
| 328.80 | 262.47 | 21.01 | 5.418 | 4.938 | 7-M2t | 3.000 | 2.782 | 2.870 | 2.870 | 9.145 | 0.000 |
| 403.40 | 267.56 | 21.13 | 5.539 | 5.272 | $4-\mathrm{FFf}$ | 3.000 | 2.818 | 3.000 | 3.170 | 8.919 | 0.000 |
| 478.00 | 271.56 | 21.23 | 5.636 | 5.640 | $4-\mathrm{FFf}$ | 3.000 | 2.846 | 3.000 | 3.470 | 9.052 | 0.000 |
| 552.60 | 265.89 | 21.33 | 5.499 | 5.744 | $4-\mathrm{FFf}$ | 3.000 | 2.806 | 3.000 | 3.670 | 8.863 | 0.000 |
| 627.20 | 265.19 | 21.42 | 5.483 | 5.832 | $4-\mathrm{FFf}$ | 3.000 | 2.801 | 3.000 | 3.770 | 8.840 | 0.000 |
| 701.80 | 264.14 | 21.50 | 5.458 | 5.914 | $4-\mathrm{FFf}$ | 3.000 | 2.794 | 3.000 | 3.870 | 8.805 | 0.000 |
| 776.40 | 262.78 | 21.58 | 5.425 | 5.992 | $4-\mathrm{FFf}$ | 3.000 | 2.784 | 3.000 | 3.970 | 8.759 | 0.000 |
| 851.00 | 261.26 | 21.66 | 5.390 | 6.167 | $4-\mathrm{FFf}$ | 3.000 | 2.773 | 3.000 | 4.170 | 8.709 | 0.000 |

Inlet Elevation (invert): $15.59 \mathrm{ft}, \quad$ Outlet Elevation (invert): 15.43 ft
Culvert Length: $96.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0017
$\qquad$

## Culvert Performance Curve Plot: Culvert 03

Performance Curve
Culvert: Culvert 03


Water Surface Profile Plot for Culvert: Culvert 03
Crossing - Culvert 03, Design Discharge - 478.0 cfs
Culvert - Culvert 03, Culvert Discharge - 271.6 cfs


## Site Data - Culvert 03

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 15.59 ft
Outlet Station: 96.00 ft
Outlet Elevation: 15.43 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 03

Barrel Shape: Concrete Box
Barrel Span: 10.00 ft
Barrel Rise: 3.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 03)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 105.00 | 18.00 | 2.57 |
| 179.60 | 18.00 | 2.57 |
| 254.20 | 18.00 | 2.57 |
| 328.80 | 18.30 | 2.87 |
| 403.40 | 18.60 | 3.17 |
| 478.00 | 18.90 | 3.47 |
| 552.60 | 19.10 | 3.67 |
| 627.20 | 19.20 | 3.77 |
| 701.80 | 19.30 | 3.87 |
| 776.40 | 19.40 | 3.97 |
| 851.00 | 19.60 | 4.17 |

## Tailwater Channel Data - Culvert 03

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 03

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 250.00 ft
Crest Elevation: 20.81 ft
Roadway Surface: Paved
Roadway Top Width: 57.00 ft

## HY-8 Culvert Analysis Report

## EXISTING CULVERT 3 ALT

Table 1 - Summary of Culvert Flows at Crossing: Culvert 03 Alt

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 03 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 03 Alt
Total Rating Curve
Crossing: Culvert 03 Alt


Table 2 - Culvert Summary Table: Culvert 03

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 105.00 | 105.00 | 18.42 | 2.548 | 2.833 | 3-M1t | 1.744 | 1.510 | 2.500 | 2.500 | 4.200 | 0.000 |
| 126.60 | 126.60 | 18.64 | 2.891 | 3.052 | 7-M1t | 1.978 | 1.711 | 2.520 | 2.520 | 5.024 | 0.000 |
| 148.20 | 148.20 | 18.90 | 3.234 | 3.312 | $7-\mathrm{M1t}$ | 2.202 | 1.901 | 2.570 | 2.570 | 5.767 | 0.000 |
| 169.80 | 169.80 | 19.24 | 3.587 | 3.648 | 7-M1t | 2.419 | 2.081 | 2.870 | 2.870 | 5.916 | 0.000 |
| 191.40 | 191.40 | 19.76 | 3.961 | 4.167 | $4-\mathrm{FFf}$ | 2.628 | 2.254 | 3.000 | 3.170 | 6.380 | 0.000 |
| 213.00 | 213.00 | 20.23 | 4.363 | 4.643 | $4-\mathrm{FFf}$ | 3.000 | 2.420 | 3.000 | 3.370 | 7.100 | 0.000 |
| 218.00 | 218.00 | 20.40 | 4.460 | 4.812 | $4-\mathrm{FFf}$ | 3.000 | 2.458 | 3.000 | 3.470 | 7.267 | 0.000 |
| 256.20 | 232.69 | 20.91 | 4.758 | 5.321 | $4-\mathrm{FFf}$ | 3.000 | 2.567 | 3.000 | 3.770 | 7.756 | 0.000 |
| 277.80 | 229.98 | 20.97 | 4.702 | 5.381 | $4-\mathrm{FFf}$ | 3.000 | 2.547 | 3.000 | 3.870 | 7.666 | 0.000 |
| 299.40 | 226.67 | 21.02 | 4.634 | 5.433 | $4-\mathrm{FFf}$ | 3.000 | 2.523 | 3.000 | 3.970 | 7.556 | 0.000 |
| 321.00 | 222.80 | 21.07 | 4.556 | 5.578 | $4-\mathrm{FFf}$ | 3.000 | 2.494 | 3.000 | 4.170 | 7.427 | 0.000 |

Inlet Elevation (invert): $15.59 \mathrm{ft}, \quad$ Outlet Elevation (invert): 15.43 ft
Culvert Length: $96.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0017
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 03

Performance Curve
Culvert: Culvert 03


Water Surface Profile Plot for Culvert: Culvert 03
Crossing - Culvert 03 Alt, Design Discharge - 218.0 cfs
Culvert - Culvert 03, Culvert Discharge - 218.0 cfs


## Site Data - Culvert 03

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 15.59 ft
Outlet Station: 96.00 ft
Outlet Elevation: 15.43 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 03

Barrel Shape: Concrete Box
Barrel Span: 10.00 ft
Barrel Rise: 3.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 03 Alt)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 105.00 | 17.93 | 2.50 |
| 126.60 | 17.95 | 2.52 |
| 148.20 | 18.00 | 2.57 |
| 169.80 | 18.30 | 2.87 |
| 191.40 | 18.60 | 3.17 |
| 213.00 | 18.80 | 3.37 |
| 218.00 | 18.90 | 3.47 |
| 256.20 | 19.20 | 3.77 |
| 277.80 | 19.30 | 3.87 |
| 299.40 | 19.40 | 3.97 |
| 321.00 | 19.60 | 4.17 |

Tailwater Channel Data - Culvert 03 Alt
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 03 Alt
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 250.00 ft
Crest Elevation: 20.81 ft
Roadway Surface: Paved
Roadway Top Width: 57.00 ft

## HY-8 Culvert Analysis Report

EXISTING CULVERT 4

Table 1 - Summary of Culvert Flows at Crossing: Culvert 04

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 04 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 18.71 | 15.00 | 15.00 | 0.00 | 1 |
| 18.86 | 16.50 | 16.50 | 0.00 | 1 |
| 19.02 | 18.00 | 18.00 | 0.00 | 1 |
| 19.50 | 19.50 | 19.50 | 0.00 | 1 |
| 19.86 | 20.00 | 20.00 | 0.00 | 1 |
| 20.46 | 22.50 | 22.28 | 0.10 | 40 |
| 20.51 | 24.00 | 21.13 | 2.78 | 6 |
| 20.52 | 25.50 | 20.62 | 4.74 | 4 |
| 20.54 | 27.00 | 19.92 | 6.98 | 4 |
| 20.56 | 28.50 | 19.20 | 9.24 | 4 |
| 20.57 | 30.00 | 18.46 | 11.35 | 3 |
| 20.46 | 22.44 | 22.44 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 04
Total Rating Curve
Crossing: Culvert 04


Table 2 - Culvert Summary Table: Culvert 04

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15.00 | 15.00 | 18.71 | 2.259 | 2.990 | $4-\mathrm{FFf}$ | 2.000 | 1.395 | 2.000 | 2.570 | 4.775 | 0.000 |
| 16.50 | 16.50 | 18.86 | 2.445 | 3.139 | $4-\mathrm{FFf}$ | 2.000 | 1.459 | 2.000 | 2.570 | 5.252 | 0.000 |
| 18.00 | 18.00 | 19.02 | 2.647 | 3.302 | $4-\mathrm{FFf}$ | 2.000 | 1.523 | 2.000 | 2.570 | 5.730 | 0.000 |
| 19.50 | 19.50 | 19.50 | 2.866 | 3.780 | $4-\mathrm{FFf}$ | 2.000 | 1.586 | 2.000 | 2.870 | 6.207 | 0.000 |
| 20.00 | 20.00 | 19.86 | 2.943 | 4.142 | $4-\mathrm{FFf}$ | 2.000 | 1.605 | 2.000 | 3.170 | 6.366 | 0.000 |
| 22.50 | 22.28 | 20.46 | 3.323 | 4.745 | $4-\mathrm{FFf}$ | 2.000 | 1.672 | 2.000 | 3.470 | 7.091 | 0.000 |
| 24.00 | 21.13 | 20.51 | 3.126 | 4.789 | $4-\mathrm{FFf}$ | 2.000 | 1.638 | 2.000 | 3.670 | 6.727 | 0.000 |
| 25.50 | 20.62 | 20.52 | 3.042 | 4.822 | $4-\mathrm{FFf}$ | 2.000 | 1.623 | 2.000 | 3.770 | 6.564 | 0.000 |
| 27.00 | 19.92 | 20.54 | 2.930 | 4.831 | $4-\mathrm{FFf}$ | 2.000 | 1.602 | 2.000 | 3.870 | 6.340 | 0.000 |
| 28.50 | 19.20 | 20.56 | 2.821 | 4.843 | $4-\mathrm{FFf}$ | 2.000 | 1.573 | 2.000 | 3.970 | 6.111 | 0.000 |
| 30.00 | 18.46 | 20.57 | 2.713 | 4.955 | $4-\mathrm{FFf}$ | 2.000 | 1.542 | 2.000 | 4.170 | 5.877 | 0.000 |

Inlet Elevation (invert): $15.72 \mathrm{ft}, \quad$ Outlet Elevation (invert): 15.71 ft
Culvert Length: $48.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0002


## Culvert Performance Curve Plot: Culvert 04

Performance Curve
Culvert: Culvert 04


Crossing - Culvert 04, Design Discharge - 20.0 cfs
Culvert - Culvert 04, Culvert Discharge - 20.0 cfs


## Site Data - Culvert 04

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 15.72 ft
Outlet Station: 48.00 ft
Outlet Elevation: 15.71 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 04

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 04)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 15.00 | 18.00 | 2.57 |
| 16.50 | 18.00 | 2.57 |
| 18.00 | 18.00 | 2.57 |
| 19.50 | 18.30 | 2.87 |
| 20.00 | 18.60 | 3.17 |
| 22.50 | 18.90 | 3.47 |
| 24.00 | 19.10 | 3.67 |
| 25.50 | 19.20 | 3.77 |
| 27.00 | 19.30 | 3.87 |
| 28.50 | 19.40 | 3.97 |
| 30.00 | 19.60 | 4.17 |

## Tailwater Channel Data - Culvert 04

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 04

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 20.46 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

## EXISTING CULVERT 5

Table 1 - Summary of Culvert Flows at Crossing: Culvert 05

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 05 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 15.10 | 190.00 | 190.00 | 0.00 | 1 |
| 15.44 | 227.00 | 227.00 | 0.00 | 1 |
| 15.76 | 264.00 | 264.00 | 0.00 | 1 |
| 16.08 | 301.00 | 301.00 | 0.00 | 1 |
| 16.53 | 338.00 | 338.00 | 0.00 | 1 |
| 17.04 | 375.00 | 375.00 | 0.00 | 1 |
| 17.24 | 386.00 | 386.00 | 0.00 | 1 |
| 18.32 | 449.00 | 446.38 | 2.03 | 13 |
| 18.48 | 486.00 | 441.87 | 43.76 | 7 |
| 18.58 | 523.00 | 432.68 | 89.61 | 5 |
| 18.67 | 460.00 | 421.87 | 137.87 | 0.00 |
| 18.30 | 447.58 |  |  | Overtopping |

Rating Curve Plot for Crossing: Culvert 05
Total Rating Curve
Crossing: Culvert 05


Table 2 - Culvert Summary Table: Culvert 05

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190.00 | 190.00 | 15.10 | 2.768 | 2.921 | 3-M2t | 3.000 | 1.640 | 2.260 | 2.260 | 5.254 | 0.000 |
| 227.00 | 227.00 | 15.44 | 3.134 | 3.257 | 3-M2t | 3.000 | 1.846 | 2.460 | 2.460 | 5.767 | 0.000 |
| 264.00 | 264.00 | 15.76 | 3.509 | 3.581 | $3-\mathrm{M} 2 \mathrm{t}$ | 3.000 | 2.042 | 2.660 | 2.660 | 6.203 | 0.000 |
| 301.00 | 301.00 | 16.08 | 3.904 | 3.894 | 3-M2t | 3.000 | 2.228 | 2.860 | 2.860 | 6.578 | 0.000 |
| 338.00 | 338.00 | 16.53 | 4.331 | 4.352 | $4-\mathrm{FFf}$ | 3.000 | 2.407 | 3.000 | 3.060 | 7.042 | 0.000 |
| 375.00 | 375.00 | 17.04 | 4.795 | 4.860 | $4-\mathrm{FFf}$ | 3.000 | 2.580 | 3.000 | 3.260 | 7.813 | 0.000 |
| 386.00 | 386.00 | 17.24 | 4.942 | 5.058 | $4-\mathrm{FFf}$ | 3.000 | 2.630 | 3.000 | 3.360 | 8.042 | 0.000 |
| 449.00 | 446.38 | 18.32 | 5.820 | 6.144 | $4-\mathrm{FFf}$ | 3.000 | 2.898 | 3.000 | 3.860 | 9.300 | 0.000 |
| 486.00 | 441.87 | 18.48 | 5.750 | 6.297 | $4-\mathrm{FFf}$ | 3.000 | 2.878 | 3.000 | 4.060 | 9.206 | 0.000 |
| 523.00 | 432.68 | 18.58 | 5.610 | 6.403 | $4-\mathrm{FFf}$ | 3.000 | 2.838 | 3.000 | 4.260 | 9.014 | 0.000 |
| 560.00 | 421.87 | 18.67 | 5.448 | 6.396 | $4-\mathrm{FFf}$ | 3.000 | 2.791 | 3.000 | 4.360 | 8.789 | 0.000 |

Inlet Elevation (invert): $12.18 \mathrm{ft}, \quad$ Outlet Elevation (invert): 12.14 ft
Culvert Length: $62.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0006


## Culvert Performance Curve Plot: Culvert 05

Performance Curve
Culvert: Culvert 05


Water Surface Profile Plot for Culvert: Culvert 05
Crossing - Culvert 05, Design Discharge - 386.0 cfs
Culvert - Culvert 05, Culvert Discharge - 386.0 cfs


## Site Data - Culvert 05

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 12.18 ft
Outlet Station: 62.00 ft
Outlet Elevation: 12.14 ft
Number of Barrels: 2

## Culvert Data Summary - Culvert 05

Barrel Shape: Concrete Box
Barrel Span: 8.00 ft
Barrel Rise: 3.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 05)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 190.00 | 14.40 | 2.26 |
| 227.00 | 14.60 | 2.46 |
| 264.00 | 14.80 | 2.66 |
| 301.00 | 15.00 | 2.86 |
| 338.00 | 15.20 | 3.06 |
| 375.00 | 15.40 | 3.26 |
| 386.00 | 15.50 | 3.36 |
| 449.00 | 16.00 | 3.86 |
| 486.00 | 16.20 | 4.06 |
| 523.00 | 16.40 | 4.26 |
| 560.00 | 16.50 | 4.36 |

## Tailwater Channel Data - Culvert 05

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 05

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 18.30 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

## EXISTING CULVERT 6

Table 1 - Summary of Culvert Flows at Crossing: Culvert 06

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 06 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 16.87 | 20.00 | 20.00 | 0.00 | 1 |
| 17.50 | 26.70 | 26.70 | 0.00 | 1 |
| 18.06 | 33.40 | 33.40 | 0.00 | 1 |
| 18.85 | 40.10 | 40.10 | 0.00 | 1 |
| 19.44 | 46.80 | 44.34 | 2.24 | 24 |
| 19.50 | 53.50 | 44.73 | 8.67 | 6 |
| 19.54 | 60.20 | 44.58 | 15.55 | 5 |
| 19.56 | 61.00 | 41.83 | 18.94 | 4 |
| 19.65 | 73.60 | 36.28 | 37.13 | 4 |
| 19.68 | 80.30 | 35.47 | 44.59 | 3 |
| 19.71 | 87.00 | 34.64 | 52.21 | 3 |
| 19.40 | 44.07 | 44.07 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 06
Total Rating Curve
Crossing: Culvert 06


Table 2 - Culvert Summary Table: Culvert 06

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20.00 | 20.00 | 16.87 | 2.320 | $0.0^{\star}$ | 1-S2n | 1.494 | 1.516 | 1.495 | 1.740 | 6.528 | 0.000 |
| 26.70 | 26.70 | 17.50 | 2.861 | 2.954 | 2-M2c | 1.847 | 1.760 | 1.761 | 1.740 | 7.224 | 0.000 |
| 33.40 | 33.40 | 18.06 | 3.506 | 3.447 | 2-M2c | 2.500 | 1.962 | 1.966 | 1.740 | 8.073 | 0.000 |
| 40.10 | 40.10 | 18.85 | 4.300 | 4.046 | 2-M2c | 2.500 | 2.115 | 2.130 | 2.040 | 9.031 | 0.000 |
| 46.80 | 44.34 | 19.44 | 4.889 | 4.550 | 7-M2t | 2.500 | 2.204 | 2.340 | 2.340 | 9.344 | 0.000 |
| 53.50 | 44.73 | 19.50 | 4.945 | 4.807 | $4-\mathrm{FFf}$ | 2.500 | 2.212 | 2.500 | 2.640 | 9.112 | 0.000 |
| 60.20 | 44.58 | 19.54 | 4.923 | 4.991 | $4-\mathrm{FFf}$ | 2.500 | 2.209 | 2.500 | 2.840 | 9.081 | 0.000 |
| 61.00 | 41.83 | 19.56 | 4.532 | 5.011 | $4-\mathrm{FFf}$ | 2.500 | 2.151 | 2.500 | 3.140 | 8.521 | 0.000 |
| 73.60 | 36.28 | 19.65 | 3.827 | 5.100 | $4-\mathrm{FFf}$ | 2.500 | 2.034 | 2.500 | 3.740 | 7.390 | 0.000 |
| 80.30 | 35.47 | 19.68 | 3.734 | 5.132 | $4-\mathrm{FFf}$ | 2.500 | 2.017 | 2.500 | 3.840 | 7.226 | 0.000 |
| 87.00 | 34.64 | 19.71 | 3.640 | 5.263 | $4-\mathrm{FFf}$ | 2.500 | 1.999 | 2.500 | 4.040 | 7.056 | 0.000 |

* theoretical depth is impractical. Depth reported is corrected.
$\qquad$


## Culvert Performance Curve Plot: Culvert 06

Performance Curve
Culvert: Culvert 06



## Site Data - Culvert 06

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 14.55 ft
Outlet Station: 42.00 ft
Outlet Elevation: 14.36 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 06

Barrel Shape: Circular
Barrel Diameter: 2.50 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 06)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 20.00 | 16.10 | 1.74 |
| 26.70 | 16.10 | 1.74 |
| 33.40 | 16.10 | 1.74 |
| 40.10 | 16.40 | 2.04 |
| 46.80 | 16.70 | 2.34 |
| 53.50 | 17.00 | 2.64 |
| 60.20 | 17.20 | 2.84 |
| 61.00 | 17.50 | 3.14 |
| 73.60 | 18.10 | 3.74 |
| 80.30 | 18.20 | 3.84 |
| 87.00 | 18.40 | 4.04 |

## Tailwater Channel Data - Culvert 06

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 06

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 19.40 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

 EXISTING CULVERT 7Table 1 - Summary of Culvert Flows at Crossing: Culvert 07

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 07 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 19.77 | 250.00 | 250.00 | 0.00 | 1 |
| 21.03 | 307.20 | 307.20 | 0.00 | 1 |
| 21.24 | 364.40 | 315.91 | 47.85 | 8 |
| 21.34 | 421.60 | 320.03 | 101.20 | 6 |
| 21.42 | 469.00 | 322.85 | 145.80 | 5 |
| 21.50 | 536.00 | 326.35 | 208.83 | 4 |
| 21.58 | 593.20 | 329.09 | 263.68 | 4 |
| 21.64 | 650.40 | 331.63 | 318.53 | 4 |
| 21.70 | 707.60 | 333.98 | 372.63 | 3 |
| 21.76 | 764.80 | 336.25 | 427.78 | 3 |
| 21.82 | 822.00 | 335.60 | 485.72 | 3 |
| 21.08 | 309.33 | 309.33 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 07
Total Rating Curve
Crossing: Culvert 07


Table 2 - Culvert Summary Table: Culvert 07

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 250.00 | 250.00 | 19.77 | 5.565 | 5.357 | 3-M2t | 4.000 | 3.125 | 3.330 | 3.330 | 9.384 | 0.000 |
| 307.20 | 307.20 | 21.03 | 6.828 | 6.227 | 7-M2c | 4.000 | 3.585 | 3.577 | 3.350 | 10.737 | 0.000 |
| 364.40 | 315.91 | 21.24 | 7.041 | 6.394 | 7-M2c | 4.000 | 3.653 | 3.644 | 3.380 | 10.837 | 0.000 |
| 421.60 | 320.03 | 21.34 | 7.144 | 6.472 | 7-M2c | 4.000 | 3.684 | 3.675 | 3.410 | 10.884 | 0.000 |
| 469.00 | 322.85 | 21.42 | 7.216 | 6.526 | 7-M2c | 4.000 | 3.706 | 3.697 | 3.430 | 10.916 | 0.000 |
| 536.00 | 326.35 | 21.50 | 7.305 | 6.592 | 7-M2c | 4.000 | 3.733 | 3.723 | 3.530 | 10.956 | 0.000 |
| 593.20 | 329.09 | 21.58 | 7.376 | 6.644 | 7-M2c | 4.000 | 3.754 | 3.744 | 3.730 | 10.986 | 0.000 |
| 650.40 | 331.63 | 21.64 | 7.442 | 6.711 | 7-M2t | 4.000 | 3.773 | 3.930 | 3.930 | 10.548 | 0.000 |
| 707.60 | 333.98 | 21.70 | 7.503 | 6.997 | 4-FFf | 4.000 | 3.791 | 4.000 | 4.230 | 10.437 | 0.000 |
| 764.80 | 336.25 | 21.76 | 7.563 | 7.335 | 4-FFf | 4.000 | 3.808 | 4.000 | 4.530 | 10.508 | 0.000 |
| 822.00 | 335.60 | 21.82 | 7.546 | 7.524 | 4-FFf | 4.000 | 3.803 | 4.000 | 4.730 | 10.487 | 0.000 |

Inlet Elevation (invert): $14.20 \mathrm{ft}, \quad$ Outlet Elevation (invert): 14.17 ft
Culvert Length: $54.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0006


## Culvert Performance Curve Plot: Culvert 07

Performance Curve
Culvert: Culvert 07


Crossing - Culvert 07, Design Discharge - 469.0 cfs
Culvert - Culvert 07, Culvert Discharge - 322.9 cfs


## Site Data - Culvert 07

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 14.20 ft
Outlet Station: 54.00 ft
Outlet Elevation: 14.17 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 07

Barrel Shape: Concrete Box
Barrel Span: 8.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 07)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 250.00 | 17.50 | 3.33 |
| 307.20 | 17.52 | 3.35 |
| 364.40 | 17.55 | 3.38 |
| 421.60 | 17.58 | 3.41 |
| 469.00 | 17.60 | 3.43 |
| 536.00 | 17.70 | 3.53 |
| 593.20 | 17.90 | 3.73 |
| 650.40 | 18.10 | 3.93 |
| 707.60 | 18.40 | 4.23 |
| 764.80 | 18.70 | 4.53 |
| 822.00 | 18.90 | 4.73 |

## Tailwater Channel Data - Culvert 07

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 07

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 250.00 ft
Crest Elevation: 21.08 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

# HY-8 Culvert Analysis Report EXISTING CULVERT 8 

Table 1 - Summary of Culvert Flows at Crossing: Culvert 08

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 08 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 08


Table 2 - Culvert Summary Table: Culvert 08

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20.00 | 20.00 | 20.06 | 2.943 | 3.006 | 7-M2c | 2.000 | 1.605 | 1.606 | 3.330 | 7.395 | 0.000 |
| 32.10 | 29.18 | 21.81 | 4.755 | 4.536 | 7-M2c | 2.000 | 1.875 | 1.845 | 3.340 | 9.594 | 0.000 |
| 44.20 | 29.55 | 21.89 | 4.844 | 4.608 | 7-M2c | 2.000 | 1.886 | 1.850 | 3.350 | 9.787 | 0.000 |
| 56.30 | 29.82 | 21.96 | 4.909 | 4.660 | 7-M2c | 2.000 | 1.894 | 1.879 | 3.360 | 9.800 | 0.000 |
| 68.40 | 30.04 | 22.01 | 4.964 | 4.704 | 7-M2c | 2.000 | 1.901 | 1.915 | 3.370 | 9.779 | 0.000 |
| 80.50 | 30.25 | 22.06 | 5.014 | 4.744 | 7-M2c | 2.000 | 1.907 | 1.931 | 3.380 | 9.803 | 0.000 |
| 92.60 | 30.43 | 22.11 | 5.059 | 4.780 | 7-M2c | 2.000 | 1.912 | 1.941 | 3.410 | 9.837 | 0.000 |
| 99.00 | 30.52 | 22.13 | 5.083 | 4.798 | 7-M2c | 2.000 | 1.915 | 1.945 | 3.430 | 9.857 | 0.000 |
| 116.80 | 30.77 | 22.19 | 5.143 | 4.846 | 7-M2c | 2.000 | 1.922 | 1.953 | 3.730 | 9.914 | 0.000 |
| 128.90 | 30.92 | 22.23 | 5.182 | 4.877 | 7-M2c | 2.000 | 1.927 | 1.957 | 4.230 | 9.953 | 0.000 |
| 141.00 | 31.07 | 22.27 | 5.219 | 4.906 | 7-M2c | 2.000 | 1.931 | 1.961 | 4.730 | 9.992 | 0.000 |

Inlet Elevation (invert): $17.05 \mathrm{ft}, \quad$ Outlet Elevation (invert): 17.02 ft
Culvert Length: $42.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0007
$\qquad$

## Culvert Performance Curve Plot: Culvert 08

Performance Curve
Culvert: Culvert 08



## Site Data - Culvert 08

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 17.05 ft
Outlet Station: 42.00 ft
Outlet Elevation: 17.02 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 08

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 08)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 20.00 | 17.50 | 3.33 |
| 32.10 | 17.51 | 3.34 |
| 44.20 | 17.52 | 3.35 |
| 56.30 | 17.53 | 3.36 |
| 68.40 | 17.54 | 3.37 |
| 80.50 | 17.55 | 3.38 |
| 92.60 | 17.58 | 3.41 |
| 99.00 | 17.60 | 3.43 |
| 116.80 | 17.90 | 3.73 |
| 128.90 | 18.40 | 4.23 |
| 141.00 | 18.90 | 4.73 |

## Tailwater Channel Data - Culvert 08

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 08

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 21.76 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

EXISTING CULVERT 9

Table 1 - Summary of Culvert Flows at Crossing: Culvert 09

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 09 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 17.26 | 215.00 | 215.00 | 0.00 | 1 |
| 17.72 | 260.20 | 260.20 | 0.00 | 1 |
| 18.21 | 305.40 | 305.40 | 0.00 | 1 |
| 18.74 | 350.60 | 350.60 | 0.00 | 1 |
| 19.06 | 376.00 | 376.00 | 0.00 | 1 |
| 19.95 | 441.00 | 441.00 | 0.00 | 1 |
| 20.64 | 486.20 | 486.20 | 0.00 | 1 |
| 21.15 | 531.40 | 517.83 | 13.19 | 12 |
| 21.27 | 576.60 | 524.71 | 51.19 | 6 |
| 21.36 | 621.80 | 529.97 | 91.21 | 5 |
| 21.43 | 667.00 | 534.61 | 132.16 | 5 |
| 21.07 | 513.01 | 513.01 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 09
Total Rating Curve
Crossing: Culvert 09


Table 2 - Culvert Summary Table: Culvert 09

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 215.00 | 215.00 | 17.26 | 4.106 | 4.316 | 1-S1t | 2.412 | 2.436 | 3.540 | 3.540 | 6.073 | 0.000 |
| 260.20 | 260.20 | 17.72 | 4.666 | 4.780 | 1-S1t | 2.754 | 2.766 | 3.640 | 3.640 | 7.148 | 0.000 |
| 305.40 | 305.40 | 18.21 | 5.220 | 5.275 | 7-M1t | 3.085 | 3.078 | 3.740 | 3.740 | 8.166 | 0.000 |
| 350.60 | 350.60 | 18.74 | 5.786 | 5.800 | 7-M1t | 3.403 | 3.374 | 3.790 | 3.790 | 9.251 | 0.000 |
| 376.00 | 376.00 | 19.06 | 6.116 | 6.102 | 7-M1t | 3.579 | 3.535 | 3.840 | 3.840 | 9.792 | 0.000 |
| 441.00 | 441.00 | 19.95 | 7.013 | 6.820 | 7-M1t | 4.019 | 3.932 | 4.040 | 4.040 | 10.916 | 0.000 |
| 486.20 | 486.20 | 20.64 | 7.697 | 7.275 | 3-M2t | 4.316 | 4.196 | 4.240 | 4.240 | 11.467 | 0.000 |
| 531.40 | 517.83 | 21.15 | 8.210 | 7.582 | 3-M2t | 5.000 | 4.376 | 4.440 | 4.440 | 11.663 | 0.000 |
| 576.60 | 524.71 | 21.27 | 8.325 | 7.619 | 3-M2t | 5.000 | 4.415 | 4.640 | 4.640 | 11.308 | 0.000 |
| 621.80 | 529.97 | 21.36 | 8.415 | 7.652 | 3-M2t | 5.000 | 4.444 | 4.740 | 4.740 | 11.181 | 0.000 |
| 667.00 | 534.61 | 21.43 | 8.494 | 7.682 | 3-M2t | 5.000 | 4.470 | 4.840 | 4.840 | 11.046 | 0.000 |

Inlet Elevation (invert): $12.94 \mathrm{ft}, \quad$ Outlet Elevation (invert): 12.76 ft
Culvert Length: $67.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0027
**************************************************************************************)

## Culvert Performance Curve Plot: Culvert 09

Performance Curve
Culvert: Culvert 09


Water Surface Profile Plot for Culvert: Culvert 09
Crossing - Culvert 09, Design Discharge - 376.0 cfs
Culvert - Culvert 09, Culvert Discharge - 376.0 cfs


## Site Data - Culvert 09

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 12.94 ft
Outlet Station: 67.00 ft
Outlet Elevation: 12.76 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 09

Barrel Shape: Concrete Box
Barrel Span: 10.00 ft
Barrel Rise: 5.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 09)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 215.00 | 16.30 | 3.54 |
| 260.20 | 16.40 | 3.64 |
| 305.40 | 16.50 | 3.74 |
| 350.60 | 16.55 | 3.79 |
| 376.00 | 16.60 | 3.84 |
| 441.00 | 16.80 | 4.04 |
| 486.20 | 17.00 | 4.24 |
| 531.40 | 17.20 | 4.44 |
| 576.60 | 17.40 | 4.64 |
| 621.80 | 17.50 | 4.74 |
| 667.00 | 17.60 | 4.84 |

## Tailwater Channel Data - Culvert 09

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 09

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 21.07 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

HY-8 Culvert Analysis Report

## EXISTING CULVERT 10

Table 1 - Summary of Culvert Flows at Crossing: Culvert 10

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 10 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 10
Total Rating Curve
Crossing: Culvert 10


Table 2 - Culvert Summary Table: Culvert 10

| Total <br> Discharge <br> (cfs) | Culvert <br> Discharge <br> (cfs) | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> (ft/s) | Tailwater <br> Velocity <br> (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10.00 | 10.00 | 20.25 | 1.704 | 1.798 | 3-M2t | 1.350 | 1.128 | 1.160 | 1.160 | 5.293 | 0.000 |
| 12.60 | 12.60 | 20.53 | 1.983 | 2.077 | 2-M2c | 1.657 | 1.272 | 1.276 | 1.260 | 5.955 | 0.000 |
| 15.20 | 15.20 | 20.80 | 2.280 | 2.346 | 2-M2c | 2.000 | 1.405 | 1.405 | 1.360 | 6.445 | 0.000 |
| 17.80 | 17.80 | 21.09 | 2.617 | 2.639 | 2-M2c | 2.000 | 1.514 | 1.520 | 1.460 | 6.948 | 0.000 |
| 20.40 | 20.40 | 21.45 | 3.004 | 2.987 | 7-M2t | 2.000 | 1.617 | 1.660 | 1.660 | 7.340 | 0.000 |
| 23.00 | 23.00 | 21.90 | 3.450 | 3.425 | 7-M2t | 2.000 | 1.693 | 1.860 | 1.860 | 7.598 | 0.000 |
| 25.60 | 25.60 | 22.41 | 3.957 | 3.892 | 4-FFf | 2.000 | 1.770 | 2.000 | 2.000 | 8.149 | 0.000 |
| 26.00 | 26.00 | 22.49 | 4.041 | 3.955 | 4-FFf | 2.000 | 1.782 | 2.000 | 2.000 | 8.276 | 0.000 |
| 30.80 | 28.06 | 22.94 | 4.493 | 4.296 | 4-FFf | 2.000 | 1.842 | 2.000 | 2.000 | 8.932 | 0.000 |
| 33.40 | 28.17 | 22.97 | 4.517 | 4.314 | 4-FFf | 2.000 | 1.846 | 2.000 | 2.000 | 8.966 | 0.000 |
| 36.00 | 28.26 | 22.99 | 4.538 | 4.330 | 4-FFf | 2.000 | 1.848 | 2.000 | 2.000 | 8.995 | 0.000 |

Inlet Elevation (invert): $18.45 \mathrm{ft}, \quad$ Outlet Elevation (invert): 18.34 ft
Culvert Length: $42.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0026
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 10

Performance Curve
Culvert: Culvert 10


Water Surface Profile Plot for Culvert: Culvert 10
Crossing - Culvert 10, Design Discharge - 26.0 cfs
Culvert - Culvert 10, Culvert Discharge - 26.0 cfs


## Site Data - Culvert 10

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 18.45 ft
Outlet Station: 42.00 ft
Outlet Elevation: 18.34 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 10

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 10)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 10.00 | 19.50 | 1.16 |
| 12.60 | 19.60 | 1.26 |
| 15.20 | 19.70 | 1.36 |
| 17.80 | 19.80 | 1.46 |
| 20.40 | 20.00 | 1.66 |
| 23.00 | 20.20 | 1.86 |
| 25.60 | 20.34 | 2.00 |
| 26.00 | 20.34 | 2.00 |
| 30.80 | 20.34 | 2.00 |
| 33.40 | 20.34 | 2.00 |
| 36.00 | 20.34 | 2.00 |

## Tailwater Channel Data - Culvert 10

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 10

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 22.90 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

## EXISTING CULVERT 11

Table 1 - Summary of Culvert Flows at Crossing: Culvert 11

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 11 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 22.08 | 5.00 | 5.00 | 0.00 | 1 |
| 22.11 | 6.00 | 6.00 | 0.00 | 1 |
| 22.15 | 7.00 | 7.00 | 0.00 | 1 |
| 22.20 | 8.00 | 8.00 | 0.00 | 1 |
| 22.25 | 9.00 | 9.00 | 0.00 | 1 |
| 22.31 | 10.00 | 10.00 | 0.00 | 1 |
| 22.38 | 12.00 | 11.00 | 0.00 | 1 |
| 22.45 | 13.00 | 12.00 | 0.00 | 1 |
| 22.53 | 14.00 | 13.00 | 0.00 | 1 |
| 22.61 | 15.00 | 14.00 | 0.00 | 1 |
| 22.70 | 25.75 | 15.00 | 0.00 | 1 |
| 24.07 |  |  | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 11
Total Rating Curve
Crossing: Culvert 11


Table 2 - Culvert Summary Table: Culvert 11

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.00 | 5.00 | 22.08 | 1.087 | 2.138 | $4-\mathrm{FFf}$ | 0.474 | 0.786 | 2.000 | 3.230 | 1.592 | 0.000 |
| 6.00 | 6.00 | 22.11 | 1.222 | 2.172 | $4-\mathrm{FFf}$ | 0.521 | 0.862 | 2.000 | 3.230 | 1.910 | 0.000 |
| 7.00 | 7.00 | 22.15 | 1.346 | 2.213 | $4-\mathrm{FFf}$ | 0.568 | 0.935 | 2.000 | 3.230 | 2.228 | 0.000 |
| 8.00 | 8.00 | 22.20 | 1.462 | 2.259 | $4-\mathrm{FFf}$ | 0.612 | 1.006 | 2.000 | 3.230 | 2.546 | 0.000 |
| 9.00 | 9.00 | 22.25 | 1.573 | 2.312 | $4-\mathrm{FFf}$ | 0.648 | 1.067 | 2.000 | 3.230 | 2.865 | 0.000 |
| 10.00 | 10.00 | 22.31 | 1.681 | 2.372 | $4-\mathrm{FFf}$ | 0.684 | 1.128 | 2.000 | 3.230 | 3.183 | 0.000 |
| 11.00 | 11.00 | 22.38 | 1.788 | 2.437 | $4-\mathrm{FFf}$ | 0.720 | 1.188 | 2.000 | 3.230 | 3.501 | 0.000 |
| 12.00 | 12.00 | 22.45 | 1.895 | 2.509 | $4-\mathrm{FFf}$ | 0.757 | 1.241 | 2.000 | 3.230 | 3.820 | 0.000 |
| 13.00 | 13.00 | 22.53 | 2.004 | 2.587 | $4-\mathrm{FFf}$ | 0.793 | 1.293 | 2.000 | 3.230 | 4.138 | 0.000 |
| 14.00 | 14.00 | 22.61 | 2.116 | 2.671 | $4-\mathrm{FFf}$ | 0.825 | 1.344 | 2.000 | 3.230 | 4.456 | 0.000 |
| 15.00 | 15.00 | 22.70 | 2.233 | 2.762 | $4-\mathrm{FFf}$ | 0.856 | 1.395 | 2.000 | 3.230 | 4.775 | 0.000 |

Inlet Elevation (invert): $19.94 \mathrm{ft}, \quad$ Outlet Elevation (invert): 18.77 ft
Culvert Length: $46.01 \mathrm{ft}, \quad$ Culvert Slope: 0.0254
**************************************************************************************)

## Culvert Performance Curve Plot: Culvert 11

Performance Curve
Culvert: Culvert 11


Water Surface Profile Plot for Culvert: Culvert 11
Crossing - Culvert 11, Design Discharge - 10.0 cfs
Culvert - Culvert 11, Culvert Discharge - 10.0 cfs


## Site Data - Culvert 11

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 19.94 ft
Outlet Station: 46.00 ft
Outlet Elevation: 18.77 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 11

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 11)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 5.00 | 22.00 | 3.23 |
| 6.00 | 22.00 | 3.23 |
| 7.00 | 22.00 | 3.23 |
| 8.00 | 22.00 | 3.23 |
| 9.00 | 22.00 | 3.23 |
| 10.00 | 22.00 | 3.23 |
| 11.00 | 22.00 | 3.23 |
| 12.00 | 22.00 | 3.23 |
| 13.00 | 22.00 | 3.23 |
| 14.00 | 22.00 | 3.23 |
| 15.00 | 22.00 | 3.23 |

Tailwater Channel Data - Culvert 11
Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 22.00 ft

## Roadway Data for Crossing: Culvert 11

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 24.07 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

## EXISTING CULVERT 12

Table 1 - Summary of Culvert Flows at Crossing: Culvert 12

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 12 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 21.41 | 5.00 | 5.00 | 0.00 | 1 |
| 21.44 | 6.00 | 6.00 | 0.00 | 1 |
| 21.48 | 7.00 | 7.00 | 0.00 | 1 |
| 21.53 | 8.00 | 8.00 | 0.00 | 1 |
| 21.58 | 9.00 | 9.00 | 0.00 | 1 |
| 21.64 | 10.00 | 10.00 | 0.00 | 1 |
| 21.71 | 11.00 | 11.00 | 0.00 | 1 |
| 21.78 | 12.00 | 12.00 | 0.00 | 1 |
| 21.86 | 13.00 | 13.00 | 0.00 | 1 |
| 21.94 | 14.00 | 14.00 | 0.00 | 1 |
| 22.03 | 15.00 | 15.00 | 0.00 | 1 |
| 23.97 | 28.56 | 28.56 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 12
Total Rating Curve
Crossing: Culvert 12


Table 2 - Culvert Summary Table: Culvert 12

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.00 | 5.00 | 21.41 | 1.112 | 2.048 | $4-\mathrm{FFf}$ | 1.352 | 0.786 | 2.000 | 2.000 | 1.592 | 0.000 |
| 6.00 | 6.00 | 21.44 | 1.246 | 2.082 | $4-\mathrm{FFf}$ | 1.570 | 0.862 | 2.000 | 2.000 | 1.910 | 0.000 |
| 7.00 | 7.00 | 21.48 | 1.370 | 2.123 | $4-\mathrm{FFf}$ | 2.000 | 0.935 | 2.000 | 2.000 | 2.228 | 0.000 |
| 8.00 | 8.00 | 21.53 | 1.487 | 2.170 | $4-\mathrm{FFf}$ | 2.000 | 1.006 | 2.000 | 2.000 | 2.546 | 0.000 |
| 9.00 | 9.00 | 21.58 | 1.598 | 2.223 | $4-\mathrm{FFf}$ | 2.000 | 1.067 | 2.000 | 2.000 | 2.865 | 0.000 |
| 10.00 | 10.00 | 21.64 | 1.706 | 2.282 | $4-\mathrm{FFf}$ | 2.000 | 1.128 | 2.000 | 2.000 | 3.183 | 0.000 |
| 11.00 | 11.00 | 21.71 | 1.812 | 2.348 | $4-\mathrm{FFf}$ | 2.000 | 1.188 | 2.000 | 2.000 | 3.501 | 0.000 |
| 12.00 | 12.00 | 21.78 | 1.919 | 2.420 | $4-\mathrm{FFf}$ | 2.000 | 1.241 | 2.000 | 2.000 | 3.820 | 0.000 |
| 13.00 | 13.00 | 21.86 | 2.029 | 2.498 | $4-\mathrm{FFf}$ | 2.000 | 1.293 | 2.000 | 2.000 | 4.138 | 0.000 |
| 14.00 | 14.00 | 21.94 | 2.141 | 2.582 | $4-\mathrm{FFf}$ | 2.000 | 1.344 | 2.000 | 2.000 | 4.456 | 0.000 |
| 15.00 | 15.00 | 22.03 | 2.258 | 2.672 | $4-\mathrm{FFf}$ | 2.000 | 1.395 | 2.000 | 2.000 | 4.775 | 0.000 |

Inlet Elevation (invert): $19.36 \mathrm{ft}, \quad$ Outlet Elevation (invert): 19.33 ft
Culvert Length: $46.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0007
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 12

Performance Curve
Culvert: Culvert 12



## Site Data - Culvert 12

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 19.36 ft
Outlet Station: 46.00 ft
Outlet Elevation: 19.33 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 12

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 12)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 5.00 | 21.33 | 2.00 |
| 6.00 | 21.33 | 2.00 |
| 7.00 | 21.33 | 2.00 |
| 8.00 | 21.33 | 2.00 |
| 9.00 | 21.33 | 2.00 |
| 10.00 | 21.33 | 2.00 |
| 11.00 | 21.33 | 2.00 |
| 12.00 | 21.33 | 2.00 |
| 13.00 | 21.33 | 2.00 |
| 14.00 | 21.33 | 2.00 |
| 15.00 | 21.33 | 2.00 |

## Tailwater Channel Data - Culvert 12

Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 21.33 ft

## Roadway Data for Crossing: Culvert 12

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 23.97 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

EXISTING CULVERT 13

Table 1 - Summary of Culvert Flows at Crossing: Culvert 13

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 13 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 13
Total Rating Curve
Crossing: Culvert 13


Table 2 - Culvert Summary Table: Culvert 13

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40.00 | 36.87 | 23.85 | 6.867 | 6.039 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 11.737 | 0.000 |
| 48.00 | 37.07 | 23.91 | 6.931 | 6.082 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 11.800 | 0.000 |
| 56.00 | 37.22 | 23.96 | 6.979 | 6.115 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 11.848 | 0.000 |
| 64.00 | 37.35 | 24.00 | 7.020 | 6.143 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 11.888 | 0.000 |
| 72.00 | 37.47 | 24.04 | 7.058 | 6.169 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 11.925 | 0.000 |
| 80.00 | 37.57 | 24.07 | 7.092 | 6.193 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 11.960 | 0.000 |
| 83.00 | 37.61 | 24.08 | 7.104 | 6.201 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 11.971 | 0.000 |
| 96.00 | 37.76 | 24.13 | 7.154 | 6.235 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 12.020 | 0.000 |
| 104.00 | 37.85 | 24.16 | 7.184 | 6.255 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 12.049 | 0.000 |
| 112.00 | 37.94 | 24.19 | 7.212 | 6.275 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 12.076 | 0.000 |
| 120.00 | 38.02 | 24.22 | 7.239 | 6.293 | $4-\mathrm{FFf}$ | 2.000 | 2.000 | 2.000 | 2.020 | 12.103 | 0.000 |

Inlet Elevation (invert): $16.98 \mathrm{ft}, \quad$ Outlet Elevation (invert): 16.88 ft
Culvert Length: $36.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0028


## Culvert Performance Curve Plot: Culvert 13

Performance Curve
Culvert: Culvert 13



## Site Data - Culvert 13

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 16.98 ft
Outlet Station: 36.00 ft
Outlet Elevation: 16.88 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 13

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 13)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 40.00 | 19.00 | 2.02 |
| 48.00 | 19.00 | 2.02 |
| 56.00 | 19.00 | 2.02 |
| 64.00 | 19.00 | 2.02 |
| 72.00 | 19.00 | 2.02 |
| 80.00 | 19.00 | 2.02 |
| 83.00 | 19.00 | 2.02 |
| 96.00 | 19.00 | 2.02 |
| 104.00 | 19.00 | 2.02 |
| 112.00 | 19.00 | 2.02 |
| 120.00 | 19.00 | 2.02 |

## Tailwater Channel Data - Culvert 13

Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 19.00 ft

## Roadway Data for Crossing: Culvert 13

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 23.80 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

## EXISTING CULVERT 14

Table 1 - Summary of Culvert Flows at Crossing: Culvert 14

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 14 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 22.69 | 3.00 | 3.00 | 0.00 | 1 |
| 22.79 | 4.30 | 4.30 | 0.00 | 1 |
| 22.92 | 5.60 | 5.60 | 0.00 | 1 |
| 23.09 | 6.90 | 6.90 | 0.00 | 1 |
| 23.29 | 8.20 | 8.20 | 0.00 | 1 |
| 23.52 | 10.50 | 9.50 | 0.00 | 1 |
| 23.62 | 12.10 | 10.00 | 0.00 | 1 |
| 24.10 | 13.40 | 12.10 | 0.00 | 1 |
| 24.44 | 14.70 | 13.40 | 0.00 | 1 |
| 24.81 | 16.00 | 14.70 | 0.00 | 0.54 |
| 25.02 | 15.32 | 15.37 | 0.00 | 20 |
| 25.00 |  |  |  | Overtopping |

Rating Curve Plot for Crossing: Culvert 14
Total Rating Curve
Crossing: Culvert 14


Table 2 - Culvert Summary Table: Culvert 14

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.00 | 3.00 | 22.69 | 0.949 | 2.022 | $4-\mathrm{FFf}$ | 0.876 | 0.655 | 1.500 | 2.000 | 1.698 | 0.000 |
| 4.30 | 4.30 | 22.79 | 1.183 | 2.119 | $4-\mathrm{FFf}$ | 1.143 | 0.792 | 1.500 | 2.000 | 2.433 | 0.000 |
| 5.60 | 5.60 | 22.92 | 1.398 | 2.251 | $4-\mathrm{FFf}$ | 1.500 | 0.912 | 1.500 | 2.000 | 3.169 | 0.000 |
| 6.90 | 6.90 | 23.09 | 1.619 | 2.417 | $4-\mathrm{FFf}$ | 1.500 | 1.014 | 1.500 | 2.000 | 3.905 | 0.000 |
| 8.20 | 8.20 | 23.29 | 1.865 | 2.617 | $4-\mathrm{FFf}$ | 1.500 | 1.105 | 1.500 | 2.000 | 4.640 | 0.000 |
| 9.50 | 9.50 | 23.52 | 2.149 | 2.853 | $4-\mathrm{FFf}$ | 1.500 | 1.189 | 1.500 | 2.000 | 5.376 | 0.000 |
| 10.00 | 10.00 | 23.62 | 2.269 | 2.952 | $4-\mathrm{FFf}$ | 1.500 | 1.215 | 1.500 | 2.000 | 5.659 | 0.000 |
| 12.10 | 12.10 | 24.10 | 2.853 | 3.427 | $4-\mathrm{FFf}$ | 1.500 | 1.311 | 1.500 | 2.000 | 6.847 | 0.000 |
| 13.40 | 13.40 | 24.44 | 3.277 | 3.766 | $4-\mathrm{FFf}$ | 1.500 | 1.370 | 1.500 | 2.000 | 7.583 | 0.000 |
| 14.70 | 14.70 | 24.81 | 3.747 | 4.139 | $4-\mathrm{FFf}$ | 1.500 | 1.429 | 1.500 | 2.000 | 8.318 | 0.000 |
| 16.00 | 15.37 | 25.02 | 4.006 | 4.345 | $4-\mathrm{FFf}$ | 1.500 | 1.459 | 1.500 | 2.000 | 8.698 | 0.000 |

Inlet Elevation (invert): $20.67 \mathrm{ft}, \quad$ Outlet Elevation (invert): 20.61 ft
Culvert Length: $36.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0017
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 14

Performance Curve
Culvert: Culvert 14


Water Surface Profile Plot for Culvert: Culvert 14
Crossing - Culvert 14, Design Discharge - 10.0 cfs
Culvert - Culvert 14, Culvert Discharge - 10.0 cfs


## Site Data - Culvert 14

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 20.67 ft
Outlet Station: 36.00 ft
Outlet Elevation: 20.61 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 14

Barrel Shape: Circular
Barrel Diameter: 1.50 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 14)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 3.00 | 22.60 | 2.00 |
| 4.30 | 22.60 | 2.00 |
| 5.60 | 22.60 | 2.00 |
| 6.90 | 22.60 | 2.00 |
| 8.20 | 22.60 | 2.00 |
| 9.50 | 22.60 | 2.00 |
| 10.00 | 22.60 | 2.00 |
| 12.10 | 22.60 | 2.00 |
| 13.40 | 22.60 | 2.00 |
| 14.70 | 22.60 | 2.00 |
| 16.00 | 22.60 | 2.00 |

## Tailwater Channel Data - Culvert 14

Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 22.60 ft

## Roadway Data for Crossing: Culvert 14

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 25.00 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## PRELIMINARY SIZING OF

## PROPOSED CROSSDRAINS

PROPOSED CULVERTS HAVE BEEN PRELIMINARILY SIZED BY MATCHING OR REDUCING THE ESTIMATED 50-YR HEADWATER AT EACH CROSSING. THE TABLE BELOW SUMMARIZES THE RESULTS.

- PROPOSED CULVERTS

| Ex. Size | Prop. Size | Culvert | 50 yr |  |  | Existing <br> Road CL EL | ~ Proposed Road CL EL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Q (cfs) | Pre HW | Post HW |  |  |
| 24" | 30 | 1 | 23 | 24.16 | 23.31 | 24.34 | 25.25 |
| $8 \times 4$ | $8 \times 4$ | 2 | 316 | 24.12 | 24.12 | 24.31 | 25.58 |
| $8 \times 4$ | (2) $6 \times 4$ | 2 Alt | 453 | 24.64 | 23.78 | 24.31 | 25.58 |
| 10x3 | (2) $8 \times 4$ | 3 | 478 | 21.23 | 20.93 | 20.84 | 24.02 |
| 10x3 | 10x3 | 3 Alt | 218 | 20.40 | 20.49 | 20.84 | 24.02 |
| 24" | 30" | 4 | 20 | 19.86 | 19.21 | 20.46 | 24.66 |
| (2) $8 \times 3$ | (2) $8 \times 4$ | 5 | 386 | 17.24 | 16.86 | 18.3 | 22.98 |
| 30" | (2) 30 | 6 | 61 | 19.56 | 19.11 | 19.4 | 23.06 |
| $8 \times 4$ | (2) $6 \times 4$ | 7 | 469 | 21.42 | 21.46 | 21.08 | 23.62 |
| 24 " | (2) $36{ }^{\prime \prime}$ | 8 | 99 | 22.13 | 21.42 | 21.76 | 25.65 |
| 10x5 | 10x5 | 9 | 376 | 19.06 | 19.06 | 21.07 | 25.01 |
| 24 " | 30 | 10 | 25.6 | 22.41 | 21.43 | 22.9 | 22.9 |
| 24 " | 24 " | 11 | 10 | 22.31 | 22.35 | 24.07 | 24.07 |
| 24 " | 30 | 12 | 10 | 21.64 | 21.51 | 23.97 | 23.97 |
| $24 "$ | $36 "$ | 13 | 83 | 24.08 | 24.48 | 23.8 | 24.5 |
| 18" | $24 "$ | 14 | 10 | 23.62 | 22.94 | 25 | 25 |

## HY-8 Culvert Analysis Report

 PROPOSED CULVERT 1Table 1 - Summary of Culvert Flows at Crossing: P_Culvert 1-30" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 01 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 22.98 | 18.00 | 18.00 | 0.00 | 1 |
| 23.03 | 18.80 | 18.80 | 0.00 | 1 |
| 23.08 | 19.60 | 19.60 | 0.00 | 1 |
| 23.13 | 20.40 | 20.40 | 0.00 | 1 |
| 23.18 | 21.20 | 21.20 | 0.00 | 1 |
| 23.24 | 22.00 | 22.00 | 0.00 | 1 |
| 23.29 | 22.80 | 22.80 | 0.00 | 1 |
| 23.31 | 23.00 | 23.00 | 0.00 | 1 |
| 23.41 | 24.40 | 24.40 | 0.00 | 1 |
| 23.46 | 25.20 | 25.20 | 0.00 | 1 |
| 23.52 | 26.00 | 26.00 | 0.00 | 1 |
| 25.25 | 41.13 | 41.13 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: P_Culvert 1-30" RCP


Table 2 - Culvert Summary Table: Culvert 01

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18.00 | 18.00 | 22.98 | 2.171 | 2.460 | 3-M1t | 1.884 | 1.433 | 2.100 | 2.100 | 4.089 | 0.000 |
| 18.80 | 18.80 | 23.03 | 2.232 | 2.509 | 7-M1t | 1.956 | 1.467 | 2.100 | 2.100 | 4.271 | 0.000 |
| 19.60 | 19.60 | 23.08 | 2.293 | 2.559 | 7-M1t | 2.045 | 1.502 | 2.100 | 2.100 | 4.453 | 0.000 |
| 20.40 | 20.40 | 23.13 | 2.354 | 2.610 | 3-M2t | 2.159 | 1.531 | 2.100 | 2.100 | 4.634 | 0.000 |
| 21.20 | 21.20 | 23.18 | 2.416 | 2.663 | 3-M2t | 2.500 | 1.561 | 2.100 | 2.100 | 4.816 | 0.000 |
| 22.00 | 22.00 | 23.24 | 2.478 | 2.718 | 3-M2t | 2.500 | 1.590 | 2.100 | 2.100 | 4.998 | 0.000 |
| 22.80 | 22.80 | 23.29 | 2.541 | 2.773 | 3-M2t | 2.500 | 1.619 | 2.100 | 2.100 | 5.180 | 0.000 |
| 23.00 | 23.00 | 23.31 | 2.557 | 2.787 | 3-M2t | 2.500 | 1.627 | 2.100 | 2.100 | 5.225 | 0.000 |
| 24.40 | 24.40 | 23.41 | 2.670 | 2.886 | 3-M2t | 2.500 | 1.678 | 2.100 | 2.100 | 5.543 | 0.000 |
| 25.20 | 25.20 | 23.46 | 2.736 | 2.944 | 3-M2t | 2.500 | 1.707 | 2.100 | 2.100 | 5.725 | 0.000 |
| 26.00 | 26.00 | 23.52 | 2.804 | 3.000 | 3-M2t | 2.500 | 1.737 | 2.100 | 2.100 | 5.907 | 0.000 |

Inlet Elevation (invert): $20.52 \mathrm{ft}, \quad$ Outlet Elevation (invert): 20.30 ft
Culvert Length: $112.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0020
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 01

Performance Curve
Culvert: Culvert 01


Water Surface Profile Plot for Culvert: Culvert 01
Crossing - P_Culvert 1-30" RCP, Design Discharge - 23.0 cfs
Culvert - Culvert 01, Culvert Discharge - 23.0 cfs


## Site Data - Culvert 01

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 20.52 ft
Outlet Station: 112.00 ft
Outlet Elevation: 20.30 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 01

Barrel Shape: Circular
Barrel Diameter: 2.50 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: P_Culvert 1-30" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 18.00 | 22.40 | 2.10 |
| 18.80 | 22.40 | 2.10 |
| 19.60 | 22.40 | 2.10 |
| 20.40 | 22.40 | 2.10 |
| 21.20 | 22.40 | 2.10 |
| 22.00 | 22.40 | 2.10 |
| 22.80 | 22.40 | 2.10 |
| 23.00 | 22.40 | 2.10 |
| 24.40 | 22.40 | 2.10 |
| 25.20 | 22.40 | 2.10 |
| 26.00 | 22.40 | 2.10 |

Tailwater Channel Data - P_Culvert 1-30" RCP
Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 22.40 ft

## Roadway Data for Crossing: P_Culvert 1-30" RCP

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 25.25 ft
Roadway Surface: Paved
Roadway Top Width: 102.00 ft

HY-8 Culvert Analysis Report PROPOSED CULVERT 2

Table 1 - Summary of Culvert Flows at Crossing: Culvert 02

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 02 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 02
Total Rating Curve
Crossing: Culvert 02


Table 2 - Culvert Summary Table: Culvert 02

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 207.00 | 207.00 | 21.83 | 4.746 | 4.741 | 2-M2c | 4.000 | 2.756 | 2.748 | 2.210 | 9.414 | 0.000 |
| 233.30 | 233.30 | 22.32 | 5.236 | 5.133 | 2-M2c | 4.000 | 2.984 | 2.976 | 2.420 | 9.799 | 0.000 |
| 259.60 | 259.60 | 22.84 | 5.761 | 5.508 | 2-M2c | 4.000 | 3.205 | 3.195 | 2.620 | 10.157 | 0.000 |
| 285.90 | 285.90 | 23.41 | 6.330 | 5.988 | 7-M2c | 4.000 | 3.418 | 3.409 | 2.820 | 10.482 | 0.000 |
| 312.20 | 312.20 | 24.03 | 6.949 | 6.551 | 7-M2c | 4.000 | 3.624 | 3.615 | 3.020 | 10.795 | 0.000 |
| 316.00 | 316.00 | 24.12 | 7.043 | 6.632 | 7-M2c | 4.000 | 3.653 | 3.644 | 3.040 | 10.838 | 0.000 |
| 364.80 | 364.80 | 25.43 | 8.354 | 7.731 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.080 | 11.400 | 0.000 |
| 391.10 | 373.09 | 25.68 | 8.596 | 7.903 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.080 | 11.659 | 0.000 |
| 417.40 | 375.57 | 25.75 | 8.670 | 7.955 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.080 | 11.736 | 0.000 |
| 443.70 | 377.58 | 25.81 | 8.730 | 7.998 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.080 | 11.800 | 0.000 |
| 470.00 | 379.34 | 25.86 | 8.783 | 8.036 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.080 | 11.854 | 0.000 |

Inlet Elevation (invert): $17.08 \mathrm{ft}, \quad$ Outlet Elevation (invert): 16.98 ft
Culvert Length: $126.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0008
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 02

Performance Curve
Culvert: Culvert 02


Crossing - Culvert 02, Design Discharge - 316.0 cfs
Culvert - Culvert 02, Culvert Discharge - 316.0 cfs


## Site Data - Culvert 02

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 17.08 ft
Outlet Station: 126.00 ft
Outlet Elevation: 16.98 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 02

Barrel Shape: Concrete Box
Barrel Span: 8.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 02)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 207.00 | 19.19 | 2.21 |
| 233.30 | 19.40 | 2.42 |
| 259.60 | 19.60 | 2.62 |
| 285.90 | 19.80 | 2.82 |
| 312.20 | 20.00 | 3.02 |
| 316.00 | 20.02 | 3.04 |
| 364.80 | 21.06 | 4.08 |
| 391.10 | 21.06 | 4.08 |
| 417.40 | 21.06 | 4.08 |
| 443.70 | 21.06 | 4.08 |
| 470.00 | 21.06 | 4.08 |

## Tailwater Channel Data - Culvert 02

Tailwater Channel Option: Enter Rating Curve

## Roadway Data for Crossing: Culvert 02

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 25.58 ft
Roadway Surface: Paved
Roadway Top Width: 102.00 ft

HY-8 Culvert Analysis Report PROPOSED CULVERT 2 ALT.

Table 1 - Summary of Culvert Flows at Crossing: Culvert 02 Alt. - (2) 6x4

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 02 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 19.51 | 100.00 | 100.00 | 0.00 | 1 |
| 20.31 | 170.40 | 170.40 | 0.00 | 1 |
| 21.10 | 240.80 | 240.80 | 0.00 | 1 |
| 21.84 | 311.20 | 311.20 | 0.00 | 1 |
| 22.73 | 381.60 | 381.60 | 0.00 | 1 |
| 23.77 | 452.00 | 452.00 | 0.00 | 1 |
| 23.78 | 453.00 | 453.00 | 0.00 | 1 |
| 25.72 | 592.80 | 561.84 | 30.86 | 6 |
| 25.87 | 663.20 | 569.36 | 93.44 | 6 |
| 25.99 | 733.60 | 575.22 | 158.00 | 5 |
| 26.09 | 804.00 | 580.34 | 222.95 | 4 |
| 25.58 | 554.73 | 554.73 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 02 Alt. - (2) 6x4


Table 2 - Culvert Summary Table: Culvert 02

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100.00 | 100.00 | 19.51 | 2.209 | 2.432 | 3-M2t | 2.077 | 1.295 | 2.040 | 2.040 | 4.085 | 0.000 |
| 170.40 | 170.40 | 20.31 | 3.120 | 3.228 | 3-M2t | 3.074 | 1.847 | 2.220 | 2.220 | 6.396 | 0.000 |
| 240.80 | 240.80 | 21.10 | 3.935 | 4.023 | $3-\mathrm{M2t}$ | 4.000 | 2.326 | 2.420 | 2.420 | 8.292 | 0.000 |
| 311.20 | 311.20 | 21.84 | 4.755 | 4.764 | 2-M2c | 4.000 | 2.760 | 2.753 | 2.620 | 9.422 | 0.000 |
| 381.60 | 381.60 | 22.73 | 5.654 | 5.453 | 2-M2c | 4.000 | 3.162 | 3.152 | 2.820 | 10.088 | 0.000 |
| 452.00 | 452.00 | 23.77 | 6.687 | 6.408 | 7-M2c | 4.000 | 3.540 | 3.531 | 3.040 | 10.668 | 0.000 |
| 453.00 | 453.00 | 23.78 | 6.703 | 6.422 | 7-M2c | 4.000 | 3.545 | 3.536 | 3.040 | 10.676 | 0.000 |
| 592.80 | 561.84 | 25.72 | 8.640 | 8.049 | $4-\mathrm{FFf}$ | 4.000 | 4.000 | 4.000 | 4.080 | 11.705 | 0.000 |
| 663.20 | 569.36 | 25.87 | 8.790 | 8.159 | $4-\mathrm{FFf}$ | 4.000 | 4.000 | 4.000 | 4.080 | 11.862 | 0.000 |
| 733.60 | 575.22 | 25.99 | 8.909 | 8.245 | $4-\mathrm{FFf}$ | 4.000 | 4.000 | 4.000 | 4.080 | 11.984 | 0.000 |
| 804.00 | 580.34 | 26.09 | 9.014 | 8.321 | $4-\mathrm{FFf}$ | 4.000 | 4.000 | 4.000 | 4.080 | 12.091 | 0.000 |

Inlet Elevation (invert): $17.08 \mathrm{ft}, \quad$ Outlet Elevation (invert): 16.98 ft
Culvert Length: $126.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0008
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 02

Performance Curve
Culvert: Culvert 02


Water Surface Profile Plot for Culvert: Culvert 02
Crossing - Culvert 02 Alt. - (2) 6x4, Design Discharge - 453.0 cfs
Culvert - Culvert 02, Culvert Discharge - 453.0 cfs


## Site Data - Culvert 02

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 17.08 ft
Outlet Station: 126.00 ft
Outlet Elevation: 16.98 ft
Number of Barrels: 2

## Culvert Data Summary - Culvert 02

Barrel Shape: Concrete Box
Barrel Span: 6.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 02 Alt. - (2) 6x4)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 100.00 | 19.02 | 2.04 |
| 170.40 | 19.20 | 2.22 |
| 240.80 | 19.40 | 2.42 |
| 311.20 | 19.60 | 2.62 |
| 381.60 | 19.80 | 2.82 |
| 452.00 | 20.02 | 3.04 |
| 453.00 | 20.02 | 3.04 |
| 592.80 | 21.06 | 4.08 |
| 663.20 | 21.06 | 4.08 |
| 733.60 | 21.06 | 4.08 |
| 804.00 | 21.06 | 4.08 |

Tailwater Channel Data - Culvert 02 Alt. - (2) $6 \times 4$
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 02 Alt. - (2) 6x4
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 25.58 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

HY-8 Culvert Analysis Report PROPOSED CULVERT 3

Table 1 - Summary of Culvert Flows at Crossing: Culvert 03-(2) 8x4

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 03 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 18.19 | 105.00 | 105.00 | 0.00 | 1 |
| 18.54 | 179.60 | 179.60 | 0.00 | 1 |
| 19.04 | 254.20 | 254.20 | 0.00 | 1 |
| 19.66 | 328.80 | 328.80 | 0.00 | 1 |
| 20.24 | 403.40 | 403.40 | 0.00 | 1 |
| 20.93 | 478.00 | 478.00 | 0.00 | 1 |
| 21.71 | 552.60 | 552.60 | 0.00 | 1 |
| 22.57 | 627.20 | 627.20 | 0.00 | 1 |
| 23.55 | 701.80 | 701.80 | 0.00 | 1 |
| 24.14 | 776.40 | 743.45 | 32.29 | 9 |
| 24.28 | 851.00 | 752.49 | 97.98 | 6 |
| 24.02 | 734.95 | 734.95 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 03 - (2) $8 \times 4$


Table 2 - Culvert Summary Table: Culvert 03

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 105.00 | 105.00 | 18.19 | 1.893 | 2.596 | 3-M1t | 1.303 | 1.104 | 2.620 | 2.620 | 2.505 | 0.000 |
| 179.60 | 179.60 | 18.54 | 2.676 | 2.947 | 3-M1t | 1.877 | 1.579 | 2.620 | 2.620 | 4.284 | 0.000 |
| 254.20 | 254.20 | 19.04 | 3.358 | 3.454 | $3-\mathrm{M1t}$ | 2.395 | 1.991 | 2.620 | 2.620 | 6.064 | 0.000 |
| 328.80 | 328.80 | 19.66 | 3.999 | 4.071 | 7-M1t | 2.877 | 2.363 | 2.920 | 2.920 | 7.038 | 0.000 |
| 403.40 | 403.40 | 20.24 | 4.649 | 4.653 | 3-M2t | 3.338 | 2.708 | 3.220 | 3.220 | 7.830 | 0.000 |
| 478.00 | 478.00 | 20.93 | 5.345 | 5.206 | 3-M2t | 4.000 | 3.033 | 3.520 | 3.520 | 8.487 | 0.000 |
| 552.60 | 552.60 | 21.71 | 6.115 | 5.727 | 3-M2t | 4.000 | 3.341 | 3.720 | 3.720 | 9.284 | 0.000 |
| 627.20 | 627.20 | 22.57 | 6.982 | 6.464 | $7-\mathrm{M} 2 \mathrm{t}$ | 4.000 | 3.635 | 3.820 | 3.820 | 10.262 | 0.000 |
| 701.80 | 701.80 | 23.55 | 7.958 | 7.253 | 7-M2t | 4.000 | 3.918 | 3.920 | 3.920 | 11.189 | 0.000 |
| 776.40 | 743.45 | 24.14 | 8.554 | 7.704 | $4-\mathrm{FFf}$ | 4.000 | 4.000 | 4.000 | 4.020 | 11.616 | 0.000 |
| 851.00 | 752.49 | 24.28 | 8.689 | 8.000 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.220 | 11.758 | 0.000 |

Inlet Elevation (invert): $15.59 \mathrm{ft}, \quad$ Outlet Elevation (invert): 15.38 ft
Culvert Length: $126.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0017


## Culvert Performance Curve Plot: Culvert 03

Performance Curve
Culvert: Culvert 03


Water Surface Profile Plot for Culvert: Culvert 03
Crossing - Culvert 03 - (2) 8x4, Design Discharge - 478.0 cfs
Culvert - Culvert 03, Culvert Discharge - 478.0 cfs


## Site Data - Culvert 03

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 15.59 ft
Outlet Station: 126.00 ft
Outlet Elevation: 15.38 ft
Number of Barrels: 2

## Culvert Data Summary - Culvert 03

Barrel Shape: Concrete Box
Barrel Span: 8.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 03-(2) 8x4)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 105.00 | 18.00 | 2.62 |
| 179.60 | 18.00 | 2.62 |
| 254.20 | 18.00 | 2.62 |
| 328.80 | 18.30 | 2.92 |
| 403.40 | 18.60 | 3.22 |
| 478.00 | 18.90 | 3.52 |
| 552.60 | 19.10 | 3.72 |
| 627.20 | 19.20 | 3.82 |
| 701.80 | 19.30 | 3.92 |
| 776.40 | 19.40 | 4.02 |
| 851.00 | 19.60 | 4.22 |

Tailwater Channel Data - Culvert 03-(2) 8x4
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 03-(2) 8x4
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 250.00 ft
Crest Elevation: 24.02 ft
Roadway Surface: Paved
Roadway Top Width: 102.00 ft

HY-8 Culvert Analysis Report PROPOSED CULVERT 3 ALT

Table 1 - Summary of Culvert Flows at Crossing: Culvert 03 Alt - 10x3

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 03 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 18.42 | 105.00 | 105.00 | 0.00 | 1 |
| 18.65 | 126.60 | 126.60 | 0.00 | 1 |
| 18.91 | 148.20 | 148.20 | 0.00 | 1 |
| 19.24 | 169.80 | 169.80 | 0.00 | 1 |
| 19.82 | 191.40 | 191.40 | 0.00 | 1 |
| 20.31 | 213.00 | 213.00 | 0.00 | 1 |
| 20.49 | 218.00 | 218.00 | 0.00 | 1 |
| 21.39 | 256.20 | 256.20 | 0.00 | 1 |
| 21.88 | 277.80 | 277.80 | 0.00 | 1 |
| 22.39 | 299.40 | 299.40 | 0.00 | 1 |
| 23.04 | 321.00 | 321.00 | 0.00 | 1 |
| 24.02 | 360.43 | 360.43 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 03 Alt - 10x3


Table 2 - Culvert Summary Table: Culvert 03

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 105.00 | 105.00 | 18.42 | 2.548 | 2.832 | 3-M1t | 1.744 | 1.510 | 2.550 | 2.500 | 4.118 | 0.000 |
| 126.60 | 126.60 | 18.65 | 2.891 | 3.057 | 7-M1t | 1.978 | 1.711 | 2.570 | 2.520 | 4.926 | 0.000 |
| 148.20 | 148.20 | 18.91 | 3.234 | 3.318 | $7-\mathrm{M1t}$ | 2.202 | 1.901 | 2.620 | 2.570 | 5.656 | 0.000 |
| 169.80 | 169.80 | 19.24 | 3.587 | 3.654 | 7-M1t | 2.419 | 2.081 | 2.920 | 2.870 | 5.815 | 0.000 |
| 191.40 | 191.40 | 19.82 | 3.961 | 4.233 | $4-\mathrm{FFf}$ | 2.628 | 2.254 | 3.000 | 3.170 | 6.380 | 0.000 |
| 213.00 | 213.00 | 20.31 | 4.363 | 4.724 | $4-\mathrm{FFf}$ | 3.000 | 2.420 | 3.000 | 3.370 | 7.100 | 0.000 |
| 218.00 | 218.00 | 20.49 | 4.460 | 4.896 | $4-\mathrm{FFf}$ | 3.000 | 2.458 | 3.000 | 3.470 | 7.267 | 0.000 |
| 256.20 | 256.20 | 21.39 | 5.273 | 5.801 | $4-\mathrm{FFf}$ | 3.000 | 2.738 | 3.000 | 3.770 | 8.540 | 0.000 |
| 277.80 | 277.80 | 21.88 | 5.789 | 6.286 | $4-\mathrm{FFf}$ | 3.000 | 2.889 | 3.000 | 3.870 | 9.260 | 0.000 |
| 299.40 | 299.40 | 22.39 | 6.350 | 6.802 | $4-\mathrm{FFf}$ | 3.000 | 3.000 | 3.000 | 3.970 | 9.980 | 0.000 |
| 321.00 | 321.00 | 23.04 | 6.957 | 7.450 | $4-\mathrm{FFf}$ | 3.000 | 3.000 | 3.000 | 4.170 | 10.700 | 0.000 |

Inlet Elevation (invert): $15.59 \mathrm{ft}, \quad$ Outlet Elevation (invert): 15.38 ft
Culvert Length: $126.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0017


## Culvert Performance Curve Plot: Culvert 03

Performance Curve
Culvert: Culvert 03


Water Surface Profile Plot for Culvert: Culvert 03
Crossing - Culvert 03 Alt - 10x3, Design Discharge - 218.0 cfs
Culvert - Culvert 03, Culvert Discharge - 218.0 cfs


## Site Data - Culvert 03

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 15.59 ft
Outlet Station: 126.00 ft
Outlet Elevation: 15.38 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 03

Barrel Shape: Concrete Box
Barrel Span: 10.00 ft
Barrel Rise: 3.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 03 Alt - 10x3)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 105.00 | 17.93 | 2.50 |
| 126.60 | 17.95 | 2.52 |
| 148.20 | 18.00 | 2.57 |
| 169.80 | 18.30 | 2.87 |
| 191.40 | 18.60 | 3.17 |
| 213.00 | 18.80 | 3.37 |
| 218.00 | 18.90 | 3.47 |
| 256.20 | 19.20 | 3.77 |
| 277.80 | 19.30 | 3.87 |
| 299.40 | 19.40 | 3.97 |
| 321.00 | 19.60 | 4.17 |

Tailwater Channel Data - Culvert 03 Alt - 10x3
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 03 Alt - 10x3
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 250.00 ft
Crest Elevation: 24.02 ft
Roadway Surface: Paved
Roadway Top Width: 57.00 ft

## HY-8 Culvert Analysis Report

PROPOSED CULVERT 4

Table 1-Summary of Culvert Flows at Crossing: Culvert 04-30" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 04 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 18.34 | 15.00 | 15.00 | 0.00 | 1 |
| 18.42 | 16.50 | 16.50 | 0.00 | 1 |
| 18.50 | 18.00 | 18.00 | 0.00 | 1 |
| 18.88 | 19.50 | 19.50 | 0.00 | 1 |
| 19.21 | 20.00 | 20.00 | 0.00 | 1 |
| 19.67 | 22.50 | 22.50 | 0.00 | 1 |
| 19.98 | 24.00 | 24.00 | 0.00 | 1 |
| 20.20 | 25.50 | 25.50 | 0.00 | 1 |
| 20.42 | 27.00 | 27.00 | 0.00 | 1 |
| 20.64 | 28.50 | 28.50 | 0.00 | 1 |
| 20.98 | 30.00 | 30.00 | 0.00 | 1 |
| 24.66 | 50.00 | 50.00 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 04-30" RCP


Table 2 - Culvert Summary Table: Culvert 04

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15.00 | 15.00 | 18.34 | 1.939 | 2.624 | $4-\mathrm{FFf}$ | 1.633 | 1.302 | 2.500 | 2.570 | 3.056 | 0.000 |
| 16.50 | 16.50 | 18.42 | 2.056 | 2.697 | $4-\mathrm{FFf}$ | 1.748 | 1.367 | 2.500 | 2.570 | 3.361 | 0.000 |
| 18.00 | 18.00 | 18.50 | 2.171 | 2.776 | $4-\mathrm{FFf}$ | 1.884 | 1.433 | 2.500 | 2.570 | 3.667 | 0.000 |
| 19.50 | 19.50 | 18.88 | 2.285 | 3.162 | $4-\mathrm{FFf}$ | 2.030 | 1.498 | 2.500 | 2.870 | 3.973 | 0.000 |
| 20.00 | 20.00 | 19.21 | 2.324 | 3.492 | $4-\mathrm{FFf}$ | 2.102 | 1.516 | 2.500 | 3.170 | 4.074 | 0.000 |
| 22.50 | 22.50 | 19.67 | 2.517 | 3.955 | $4-\mathrm{FFf}$ | 2.500 | 1.608 | 2.500 | 3.470 | 4.584 | 0.000 |
| 24.00 | 24.00 | 19.98 | 2.637 | 4.262 | $4-\mathrm{FFf}$ | 2.500 | 1.663 | 2.500 | 3.670 | 4.889 | 0.000 |
| 25.50 | 25.50 | 20.20 | 2.761 | 4.475 | $4-\mathrm{FFf}$ | 2.500 | 1.718 | 2.500 | 3.770 | 5.195 | 0.000 |
| 27.00 | 27.00 | 20.42 | 2.890 | 4.696 | $4-\mathrm{FFf}$ | 2.500 | 1.769 | 2.500 | 3.870 | 5.500 | 0.000 |
| 28.50 | 28.50 | 20.64 | 3.024 | 4.923 | $4-\mathrm{FFf}$ | 2.500 | 1.815 | 2.500 | 3.970 | 5.806 | 0.000 |
| 30.00 | 30.00 | 20.98 | 3.165 | 5.258 | $4-\mathrm{FFf}$ | 2.500 | 1.860 | 2.500 | 4.170 | 6.112 | 0.000 |

Inlet Elevation (invert): $15.72 \mathrm{ft}, \quad$ Outlet Elevation (invert): 15.50 ft
Culvert Length: $112.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0020
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 04

Performance Curve
Culvert: Culvert 04


Water Surface Profile Plot for Culvert: Culvert 04
Crossing - Culvert 04-30" RCP, Design Discharge - 20.0 cfs
Culvert - Culvert 04, Culvert Discharge - 20.0 cfs


## Site Data - Culvert 04

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 15.72 ft
Outlet Station: 112.00 ft
Outlet Elevation: 15.50 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 04

Barrel Shape: Circular
Barrel Diameter: 2.50 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 04-30" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 15.00 | 18.00 | 2.57 |
| 16.50 | 18.00 | 2.57 |
| 18.00 | 18.00 | 2.57 |
| 19.50 | 18.30 | 2.87 |
| 20.00 | 18.60 | 3.17 |
| 22.50 | 18.90 | 3.47 |
| 24.00 | 19.10 | 3.67 |
| 25.50 | 19.20 | 3.77 |
| 27.00 | 19.30 | 3.87 |
| 28.50 | 19.40 | 3.97 |
| 30.00 | 19.60 | 4.17 |

Tailwater Channel Data - Culvert 04-30" RCP
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 04-30" RCP
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 24.66 ft
Roadway Surface: Paved
Roadway Top Width: 102.00 ft

## HY-8 Culvert Analysis Report

## PROPOSED CULVERT 5

Table 1 - Summary of Culvert Flows at Crossing: Culvert 05-(2) 8x4

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 05 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 15.18 | 190.00 | 190.00 | 0.00 | 1 |
| 15.52 | 227.00 | 227.00 | 0.00 | 1 |
| 15.84 | 264.00 | 264.00 | 0.00 | 1 |
| 16.16 | 301.00 | 301.00 | 0.00 | 1 |
| 16.46 | 338.00 | 338.00 | 0.00 | 1 |
| 16.76 | 375.00 | 375.00 | 0.00 | 1 |
| 16.86 | 386.00 | 386.00 | 0.00 | 1 |
| 17.48 | 449.00 | 449.00 | 0.00 | 1 |
| 17.95 | 486.00 | 486.00 | 0.00 | 1 |
| 18.43 | 523.00 | 523.00 | 0.00 | 1 |
| 18.82 | 560.00 | 560.00 | 0.00 | 1 |
| 22.98 | 819.44 | 819.44 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 05 - (2) $8 \times 4$


Table 2 - Culvert Summary Table: Culvert 05

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190.00 | 190.00 | 15.18 | 2.778 | 2.976 | 3-M2t | 3.321 | 1.640 | 2.260 | 2.260 | 5.254 | 0.000 |
| 227.00 | 227.00 | 15.52 | 3.119 | 3.316 | 3-M2t | 4.000 | 1.846 | 2.460 | 2.460 | 5.767 | 0.000 |
| 264.00 | 264.00 | 15.84 | 3.446 | 3.643 | 3-M2t | 4.000 | 2.042 | 2.660 | 2.660 | 6.203 | 0.000 |
| 301.00 | 301.00 | 16.16 | 3.764 | 3.958 | 3-M2t | 4.000 | 2.228 | 2.860 | 2.860 | 6.578 | 0.000 |
| 338.00 | 338.00 | 16.46 | 4.081 | 4.263 | 3-M2t | 4.000 | 2.407 | 3.060 | 3.060 | 6.904 | 0.000 |
| 375.00 | 375.00 | 16.76 | 4.401 | 4.557 | 3-M2t | 4.000 | 2.580 | 3.260 | 3.260 | 7.189 | 0.000 |
| 386.00 | 386.00 | 16.86 | 4.497 | 4.657 | 3-M2t | 4.000 | 2.630 | 3.360 | 3.360 | 7.180 | 0.000 |
| 449.00 | 449.00 | 17.48 | 5.069 | 5.277 | 7-M2t | 4.000 | 2.909 | 3.860 | 3.860 | 7.270 | 0.000 |
| 486.00 | 486.00 | 17.95 | 5.426 | 5.751 | 4-FFf | 4.000 | 3.067 | 4.000 | 4.060 | 7.594 | 0.000 |
| 523.00 | 523.00 | 18.43 | 5.802 | 6.228 | 4-FFf | 4.000 | 3.220 | 4.000 | 4.260 | 8.172 | 0.000 |
| 560.00 | 560.00 | 18.82 | 6.199 | 6.625 | 4-FFf | 4.000 | 3.370 | 4.000 | 4.360 | 8.750 | 0.000 |

Inlet Elevation (invert): $12.20 \mathrm{ft}, \quad$ Outlet Elevation (invert): 12.14 ft
Culvert Length: $160.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0004
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 05

Performance Curve
Culvert: Culvert 05


Water Surface Profile Plot for Culvert: Culvert 05
Crossing - Culvert 05 - (2) 8x4, Design Discharge - 386.0 cfs
Culvert - Culvert 05, Culvert Discharge - 386.0 cfs


## Site Data - Culvert 05

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 12.20 ft
Outlet Station: 160.00 ft
Outlet Elevation: 12.14 ft
Number of Barrels: 2

## Culvert Data Summary - Culvert 05

Barrel Shape: Concrete Box
Barrel Span: 8.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 05-(2) 8x4)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 190.00 | 14.40 | 2.26 |
| 227.00 | 14.60 | 2.46 |
| 264.00 | 14.80 | 2.66 |
| 301.00 | 15.00 | 2.86 |
| 338.00 | 15.20 | 3.06 |
| 375.00 | 15.40 | 3.26 |
| 386.00 | 15.50 | 3.36 |
| 449.00 | 16.00 | 3.86 |
| 486.00 | 16.20 | 4.06 |
| 523.00 | 16.40 | 4.26 |
| 560.00 | 16.50 | 4.36 |

Tailwater Channel Data - Culvert 05-(2) 8x4
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 05-(2) 8x4
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 22.98 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

 PROPOSED CULVERT 6Table 1 - Summary of Culvert Flows at Crossing: Culvert 06-(2) 30" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 06 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 16.56 | 20.00 | 20.00 | 0.00 | 1 |
| 16.85 | 26.70 | 26.70 | 0.00 | 1 |
| 17.12 | 33.40 | 33.40 | 0.00 | 1 |
| 17.37 | 40.10 | 40.10 | 0.00 | 1 |
| 17.75 | 46.80 | 46.80 | 0.00 | 1 |
| 18.24 | 53.50 | 53.50 | 0.00 | 1 |
| 18.77 | 60.20 | 60.20 | 0.00 | 1 |
| 19.11 | 61.00 | 61.00 | 0.00 | 1 |
| 20.45 | 73.60 | 73.60 | 0.00 | 1 |
| 20.99 | 80.30 | 80.30 | 0.00 | 1 |
| 21.68 | 87.00 | 87.00 | 0.00 | 1 |
| 23.06 | 102.29 | 102.29 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 06 - (2) 30" RCP


Table 2 - Culvert Summary Table: Culvert 06

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20.00 | 20.00 | 16.56 | 1.508 | $0.0^{\star}$ | 1-S2n | 0.994 | 1.052 | 0.994 | 1.740 | 5.497 | 0.000 |
| 26.70 | 26.70 | 16.85 | 1.803 | $0.0^{\star}$ | 1-S2n | 1.166 | 1.227 | 1.166 | 1.740 | 5.941 | 0.000 |
| 33.40 | 33.40 | 17.12 | 2.068 | $0.0^{*}$ | 1-S2n | 1.332 | 1.376 | 1.335 | 1.740 | 6.265 | 0.000 |
| 40.10 | 40.10 | 17.37 | 2.324 | $0.0^{*}$ | 1-S2n | 1.495 | 1.518 | 1.497 | 2.040 | 6.534 | 0.000 |
| 46.80 | 46.80 | 17.75 | 2.586 | 2.703 | 7-M1t | 1.664 | 1.641 | 2.340 | 2.340 | 4.899 | 0.000 |
| 53.50 | 53.50 | 18.24 | 2.865 | 3.189 | $4-\mathrm{FFf}$ | 1.847 | 1.762 | 2.500 | 2.640 | 5.449 | 0.000 |
| 60.20 | 60.20 | 18.77 | 3.171 | 3.719 | $4-\mathrm{FFf}$ | 2.073 | 1.863 | 2.500 | 2.840 | 6.132 | 0.000 |
| 61.00 | 61.00 | 19.11 | 3.210 | 4.061 | $4-\mathrm{FFf}$ | 2.111 | 1.875 | 2.500 | 3.140 | 6.213 | 0.000 |
| 73.60 | 73.60 | 20.45 | 3.889 | 5.396 | $4-\mathrm{FFf}$ | 2.500 | 2.045 | 2.500 | 3.740 | 7.497 | 0.000 |
| 80.30 | 80.30 | 20.99 | 4.307 | 5.942 | $4-\mathrm{FFf}$ | 2.500 | 2.116 | 2.500 | 3.840 | 8.179 | 0.000 |
| 87.00 | 87.00 | 21.68 | 4.766 | 6.628 | $4-\mathrm{FFf}$ | 2.500 | 2.187 | 2.500 | 4.040 | 8.862 | 0.000 |

* theoretical depth is impractical. Depth reported is corrected.
$\qquad$


## Culvert Performance Curve Plot: Culvert 06

Performance Curve
Culvert: Culvert 06


Water Surface Profile Plot for Culvert: Culvert 06
Crossing - Culvert 06 - (2) 30" RCP, Design Discharge - 61.0 cfs
Culvert - Culvert 06, Culvert Discharge - 61.0 cfs


## Site Data - Culvert 06

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 15.05 ft
Outlet Station: 152.00 ft
Outlet Elevation: 14.36 ft
Number of Barrels: 2

## Culvert Data Summary - Culvert 06

Barrel Shape: Circular
Barrel Diameter: 2.50 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 06-(2)30" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 20.00 | 16.10 | 1.74 |
| 26.70 | 16.10 | 1.74 |
| 33.40 | 16.10 | 1.74 |
| 40.10 | 16.40 | 2.04 |
| 46.80 | 16.70 | 2.34 |
| 53.50 | 17.00 | 2.64 |
| 60.20 | 17.20 | 2.84 |
| 61.00 | 17.50 | 3.14 |
| 73.60 | 18.10 | 3.74 |
| 80.30 | 18.20 | 3.84 |
| 87.00 | 18.40 | 4.04 |

Tailwater Channel Data - Culvert 06 - (2) 30" RCP
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 06-(2) 30" RCP
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 23.06 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

## PROPOSED CULVERT 7

Table 1 - Summary of Culvert Flows at Crossing: Culvert 07-(2) 6x4

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 07 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 18.68 | 250.00 | 250.00 | 0.00 | 1 |
| 19.21 | 307.20 | 307.20 | 0.00 | 1 |
| 19.92 | 364.40 | 364.40 | 0.00 | 1 |
| 20.72 | 421.60 | 421.60 | 0.00 | 1 |
| 21.46 | 469.00 | 469.00 | 0.00 | 1 |
| 22.64 | 536.00 | 536.00 | 0.00 | 1 |
| 23.66 | 593.20 | 587.38 | 5.15 | 8 |
| 23.80 | 650.40 | 594.08 | 55.66 | 7 |
| 23.90 | 707.60 | 598.72 | 108.00 | 5 |
| 23.98 | 764.80 | 602.63 | 161.83 | 5 |
| 24.05 | 822.00 | 606.07 | 215.31 | 4 |
| 23.62 | 585.60 | 585.60 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 07-(2) 6x4


Table 2 - Culvert Summary Table: Culvert 07

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 250.00 | 250.00 | 18.68 | 4.037 | 4.180 | 7-M1t | 2.878 | 2.385 | 3.330 | 3.330 | 6.256 | 0.000 |
| 307.20 | 307.20 | 19.21 | 4.704 | 4.711 | 3-M2t | 3.361 | 2.736 | 3.350 | 3.350 | 7.642 | 0.000 |
| 364.40 | 364.40 | 19.92 | 5.421 | 5.259 | 3-M2t | 4.000 | 3.066 | 3.380 | 3.380 | 8.984 | 0.000 |
| 421.60 | 421.60 | 20.72 | 6.220 | 5.794 | 3-M2t | 4.000 | 3.379 | 3.410 | 3.410 | 10.303 | 0.000 |
| 469.00 | 469.00 | 21.46 | 6.958 | 6.562 | 7-M2c | 4.000 | 3.628 | 3.619 | 3.430 | 10.800 | 0.000 |
| 536.00 | 536.00 | 22.64 | 8.138 | 7.600 | 7-M2c | 4.000 | 3.966 | 3.955 | 3.530 | 11.293 | 0.000 |
| 593.20 | 587.38 | 23.66 | 9.157 | 8.391 | 6-FFc | 4.000 | 4.000 | 4.000 | 3.730 | 12.237 | 0.000 |
| 650.40 | 594.08 | 23.80 | 9.297 | 8.500 | 6-FFc | 4.000 | 4.000 | 4.000 | 3.930 | 12.377 | 0.000 |
| 707.60 | 598.72 | 23.90 | 9.396 | 8.805 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.230 | 12.473 | 0.000 |
| 764.80 | 602.63 | 23.98 | 9.479 | 9.170 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.530 | 12.555 | 0.000 |
| 822.00 | 606.07 | 24.05 | 9.553 | 9.427 | 4-FFf | 4.000 | 4.000 | 4.000 | 4.730 | 12.626 | 0.000 |

Inlet Elevation (invert): $14.50 \mathrm{ft}, \quad$ Outlet Elevation (invert): 14.17 ft
Culvert Length: $162.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0020
*************************************************************************************)

## Culvert Performance Curve Plot: Culvert 07

Performance Curve
Culvert: Culvert 07


Water Surface Profile Plot for Culvert: Culvert 07
Crossing - Culvert 07 - (2) 6x4, Design Discharge - 469.0 cfs
Culvert - Culvert 07, Culvert Discharge - 469.0 cfs


## Site Data - Culvert 07

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 14.50 ft
Outlet Station: 162.00 ft
Outlet Elevation: 14.17 ft
Number of Barrels: 2

## Culvert Data Summary - Culvert 07

Barrel Shape: Concrete Box
Barrel Span: 6.00 ft
Barrel Rise: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 07-(2) 6x4)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 250.00 | 17.50 | 3.33 |
| 307.20 | 17.52 | 3.35 |
| 364.40 | 17.55 | 3.38 |
| 421.60 | 17.58 | 3.41 |
| 469.00 | 17.60 | 3.43 |
| 536.00 | 17.70 | 3.53 |
| 593.20 | 17.90 | 3.73 |
| 650.40 | 18.10 | 3.93 |
| 707.60 | 18.40 | 4.23 |
| 764.80 | 18.70 | 4.53 |
| 822.00 | 18.90 | 4.73 |

Tailwater Channel Data - Culvert 07-(2) 6x4
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 07-(2) 6x4
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 250.00 ft
Crest Elevation: 23.62 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

## PROPOSED CULVERT 8

Table 1 - Summary of Culvert Flows at Crossing: Culvert 08-(2) 36" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 08 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 18.72 | 20.00 | 20.00 | 0.00 | 1 |
| 19.18 | 32.10 | 32.10 | 0.00 | 1 |
| 19.58 | 44.20 | 44.20 | 0.00 | 1 |
| 19.96 | 56.30 | 56.30 | 0.00 | 1 |
| 20.33 | 68.40 | 68.40 | 0.00 | 1 |
| 20.70 | 80.50 | 80.50 | 0.00 | 1 |
| 21.14 | 92.60 | 92.60 | 0.00 | 1 |
| 21.42 | 99.00 | 99.00 | 0.00 | 1 |
| 22.26 | 116.80 | 116.80 | 0.00 | 1 |
| 22.89 | 128.90 | 128.90 | 0.00 | 1 |
| 23.54 | 141.00 | 141.00 | 0.00 | 1 |
| 25.65 | 171.39 | 171.39 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 08 - (2) 36" RCP


Table 2 - Culvert Summary Table: Culvert 08

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20.00 | 20.00 | 18.72 | 1.380 | 1.533 | 2-M2c | 1.211 | 0.992 | 1.000 | 3.330 | 4.847 | 0.000 |
| 32.10 | 32.10 | 19.18 | 1.834 | 1.988 | 2-M2c | 1.588 | 1.273 | 1.279 | 3.340 | 5.586 | 0.000 |
| 44.20 | 44.20 | 19.58 | 2.232 | 2.390 | 2-M2c | 1.956 | 1.511 | 1.512 | 3.350 | 6.190 | 0.000 |
| 56.30 | 56.30 | 19.96 | 2.592 | 2.766 | 2-M2c | 2.374 | 1.711 | 1.716 | 3.360 | 6.734 | 0.000 |
| 68.40 | 68.40 | 20.33 | 2.944 | 3.137 | 2-M2c | 3.000 | 1.894 | 1.899 | 3.370 | 7.249 | 0.000 |
| 80.50 | 80.50 | 20.70 | 3.316 | 3.515 | 2-M2c | 3.000 | 2.063 | 2.065 | 3.380 | 7.756 | 0.000 |
| 92.60 | 92.60 | 21.14 | 3.724 | 3.953 | 2-M2c | 3.000 | 2.208 | 2.216 | 3.410 | 8.270 | 0.000 |
| 99.00 | 99.00 | 21.42 | 3.960 | 4.233 | 7-M2c | 3.000 | 2.281 | 2.290 | 3.430 | 8.549 | 0.000 |
| 116.80 | 116.80 | 22.26 | 4.702 | 5.075 | 7-M2c | 3.000 | 2.460 | 2.473 | 3.730 | 9.370 | 0.000 |
| 128.90 | 128.90 | 22.89 | 5.285 | 5.697 | 7-M2c | 3.000 | 2.557 | 2.574 | 4.230 | 9.984 | 0.000 |
| 141.00 | 141.00 | 23.54 | 5.933 | 6.349 | 7-M2c | 3.000 | 2.654 | 2.662 | 4.730 | 10.634 | 0.000 |

Inlet Elevation (invert): $17.19 \mathrm{ft}, \quad$ Outlet Elevation (invert): 16.95 ft
Culvert Length: $148.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0016


## Culvert Performance Curve Plot: Culvert 08

Performance Curve
Culvert: Culvert 08


Water Surface Profile Plot for Culvert: Culvert 08
Crossing - Culvert 08 - (2) 36 " RCP, Design Discharge - 99.0 cfs
Culvert - Culvert 08, Culvert Discharge - 99.0 cfs


## Site Data - Culvert 08

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 17.19 ft
Outlet Station: 148.00 ft
Outlet Elevation: 16.95 ft
Number of Barrels: 2

## Culvert Data Summary - Culvert 08

Barrel Shape: Circular
Barrel Diameter: 3.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 08-(2) 36" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 20.00 | 17.50 | 3.33 |
| 32.10 | 17.51 | 3.34 |
| 44.20 | 17.52 | 3.35 |
| 56.30 | 17.53 | 3.36 |
| 68.40 | 17.54 | 3.37 |
| 80.50 | 17.55 | 3.38 |
| 92.60 | 17.58 | 3.41 |
| 99.00 | 17.60 | 3.43 |
| 116.80 | 17.90 | 3.73 |
| 128.90 | 18.40 | 4.23 |
| 141.00 | 18.90 | 4.73 |

Tailwater Channel Data - Culvert 08-(2) 36" RCP
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 08-(2) 36" RCP
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 25.65 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

HY-8 Culvert Analysis Report PROPOSED CULVERT 9

Table 1 - Summary of Culvert Flows at Crossing: Culvert 09-10x5

| Headwater Elevation <br> $(\mathrm{ft})$ | Total Discharge (cfs) | Culvert 09 Discharge <br> $(\mathrm{cfs})$ | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |

Rating Curve Plot for Crossing: Culvert 09-10x5
Total Rating Curve
Crossing: Culvert 09 - 10x5


Table 2 - Culvert Summary Table: Culvert 09

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 215.00 | 215.00 | 17.26 | 4.106 | 4.321 | 1-S1t | 2.413 | 2.436 | 3.870 | 3.540 | 5.556 | 0.000 |
| 260.20 | 260.20 | 17.72 | 4.666 | 4.784 | 1-S1t | 2.755 | 2.766 | 3.970 | 3.640 | 6.554 | 0.000 |
| 305.40 | 305.40 | 18.22 | 5.220 | 5.276 | 7-M1t | 3.086 | 3.078 | 4.070 | 3.740 | 7.504 | 0.000 |
| 350.60 | 350.60 | 18.73 | 5.786 | 5.793 | 7-M1t | 3.404 | 3.374 | 4.120 | 3.790 | 8.510 | 0.000 |
| 376.00 | 376.00 | 19.06 | 6.116 | 6.087 | 7-M1t | 3.580 | 3.535 | 4.170 | 3.840 | 9.017 | 0.000 |
| 441.00 | 441.00 | 19.95 | 7.013 | 6.798 | 7-M1t | 4.020 | 3.932 | 4.370 | 4.040 | 10.092 | 0.000 |
| 486.20 | 486.20 | 20.64 | 7.697 | 7.257 | 7-M1t | 4.317 | 4.196 | 4.570 | 4.240 | 10.639 | 0.000 |
| 531.40 | 531.40 | 21.38 | 8.439 | 7.661 | 3-M2t | 5.000 | 4.452 | 4.770 | 4.440 | 11.140 | 0.000 |
| 576.60 | 576.60 | 22.19 | 9.246 | 8.105 | 3-M2t | 5.000 | 4.701 | 4.970 | 4.640 | 11.602 | 0.000 |
| 621.80 | 621.80 | 23.06 | 10.121 | 9.126 | 4-FFf | 5.000 | 4.944 | 5.000 | 4.740 | 12.436 | 0.000 |
| 667.00 | 667.00 | 24.01 | 11.068 | 9.914 | 4-FFf | 5.000 | 5.000 | 5.000 | 4.840 | 13.340 | 0.000 |

Inlet Elevation (invert): $12.94 \mathrm{ft}, \quad$ Outlet Elevation (invert): 12.43 ft
Culvert Length: $190.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0027


## Culvert Performance Curve Plot: Culvert 09

Performance Curve
Culvert: Culvert 09


Water Surface Profile Plot for Culvert: Culvert 09
Crossing - Culvert 09-10x5 , Design Discharge - 376.0 cfs
Culvert - Culvert 09, Culvert Discharge - 376.0 cfs


## Site Data - Culvert 09

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 12.94 ft
Outlet Station: 190.00 ft
Outlet Elevation: 12.43 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 09

Barrel Shape: Concrete Box
Barrel Span: 10.00 ft
Barrel Rise: 5.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge ( $90^{\circ}$ ) Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 09-10x5 )

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 215.00 | 16.30 | 3.54 |
| 260.20 | 16.40 | 3.64 |
| 305.40 | 16.50 | 3.74 |
| 350.60 | 16.55 | 3.79 |
| 376.00 | 16.60 | 3.84 |
| 441.00 | 16.80 | 4.04 |
| 486.20 | 17.00 | 4.24 |
| 531.40 | 17.20 | 4.44 |
| 576.60 | 17.40 | 4.64 |
| 621.80 | 17.50 | 4.74 |
| 667.00 | 17.60 | 4.84 |

Tailwater Channel Data-Culvert 09-10x5
Tailwater Channel Option: Enter Rating Curve
Roadway Data for Crossing: Culvert 09-10x5
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 200.00 ft
Crest Elevation: 25.01 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

HY-8 Culvert Analysis Report
PROPOSED CULVERT 10

Table 1 - Summary of Culvert Flows at Crossing: Culvert 10-30" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 10 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 20.17 | 10.00 | 10.00 | 0.00 | 1 |
| 20.34 | 12.00 | 12.00 | 0.00 | 1 |
| 20.51 | 14.00 | 14.00 | 0.00 | 1 |
| 20.59 | 15.00 | 15.00 | 0.00 | 1 |
| 20.83 | 18.00 | 18.00 | 0.00 | 1 |
| 20.98 | 20.00 | 20.00 | 0.00 | 1 |
| 21.13 | 22.00 | 22.00 | 0.00 | 1 |
| 21.29 | 24.00 | 24.00 | 0.00 | 1 |
| 21.43 | 26.00 | 26.00 | 0.00 | 1 |
| 21.60 | 28.00 | 28.00 | 0.00 | 1 |
| 21.76 | 30.00 | 30.00 | 0.00 | 1 |
| 22.90 | 40.53 | 40.53 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 10-30" RCP
Total Rating Curve
Crossing: Culvert 10-30" RCP


Table 2 - Culvert Summary Table: Culvert 10


## Culvert Performance Curve Plot: Culvert 10

Performance Curve
Culvert: Culvert 10


Water Surface Profile Plot for Culvert: Culvert 10
Crossing - Culvert 10-30" RCP, Design Discharge - 15.0 cfs
Culvert - Culvert 10, Culvert Discharge - 15.0 cfs


## Site Data - Culvert 10

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 18.54 ft

See previous page for Elevation 21.43 for 50 yr flow of 26.0 cfs

Outlet Station: 74.00 ft
Outlet Elevation: 18.34 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 10

Barrel Shape: Circular
Barrel Diameter: 2.50 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 10-30" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 10.00 | 19.50 | 1.16 |
| 12.00 | 19.50 | 1.16 |
| 14.00 | 19.50 | 1.16 |
| 15.00 | 19.50 | 1.16 |
| 18.00 | 19.50 | 1.16 |
| 20.00 | 19.50 | 1.16 |
| 22.00 | 19.50 | 1.16 |
| 24.00 | 19.50 | 1.16 |
| 26.00 | 19.50 | 1.16 |
| 28.00 | 19.50 | 1.16 |
| 30.00 | 19.50 | 1.16 |

Tailwater Channel Data - Culvert 10-30" RCP
Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 19.50 ft

## Roadway Data for Crossing: Culvert 10-30" RCP

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 22.90 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

HY-8 Culvert Analysis Report

## PROPOSED CULVERT 11

Table 1 - Summary of Culvert Flows at Crossing: Culvert 11-24" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 11 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 22.09 | 5.00 | 5.00 | 0.00 | 1 |
| 22.13 | 6.00 | 6.00 | 0.00 | 1 |
| 22.17 | 7.00 | 7.00 | 0.00 | 1 |
| 22.22 | 8.00 | 8.00 | 0.00 | 1 |
| 22.28 | 9.00 | 9.00 | 0.00 | 1 |
| 22.35 | 10.00 | 10.00 | 0.00 | 1 |
| 22.43 | 11.00 | 11.00 | 0.00 | 1 |
| 22.51 | 12.00 | 12.00 | 0.00 | 1 |
| 22.59 | 13.00 | 13.00 | 0.00 | 1 |
| 22.69 | 14.00 | 14.00 | 0.00 | 1 |
| 22.79 | 15.00 | 15.00 | 0.00 | 1 |
| 24.07 | 24.26 | 24.26 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 11-24" RCP


Table 2 - Culvert Summary Table: Culvert 11

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.00 | 5.00 | 22.09 | 1.087 | 2.147 | $4-\mathrm{FFf}$ | 0.474 | 0.786 | 2.000 | 3.840 | 1.592 | 0.000 |
| 6.00 | 6.00 | 22.13 | 1.222 | 2.186 | $4-\mathrm{FFf}$ | 0.521 | 0.862 | 2.000 | 3.840 | 1.910 | 0.000 |
| 7.00 | 7.00 | 22.17 | 1.346 | 2.232 | $4-\mathrm{FFf}$ | 0.568 | 0.935 | 2.000 | 3.840 | 2.228 | 0.000 |
| 8.00 | 8.00 | 22.22 | 1.462 | 2.285 | $4-\mathrm{FFf}$ | 0.612 | 1.006 | 2.000 | 3.840 | 2.546 | 0.000 |
| 9.00 | 9.00 | 22.28 | 1.573 | 2.344 | $4-\mathrm{FFf}$ | 0.648 | 1.067 | 2.000 | 3.840 | 2.865 | 0.000 |
| 10.00 | 10.00 | 22.35 | 1.681 | 2.411 | $4-\mathrm{FFf}$ | 0.684 | 1.128 | 2.000 | 3.840 | 3.183 | 0.000 |
| 11.00 | 11.00 | 22.43 | 1.788 | 2.485 | $4-\mathrm{FFf}$ | 0.721 | 1.188 | 2.000 | 3.840 | 3.501 | 0.000 |
| 12.00 | 12.00 | 22.51 | 1.895 | 2.566 | $4-\mathrm{FFf}$ | 0.757 | 1.241 | 2.000 | 3.840 | 3.820 | 0.000 |
| 13.00 | 13.00 | 22.59 | 2.004 | 2.654 | $4-\mathrm{FFf}$ | 0.793 | 1.293 | 2.000 | 3.840 | 4.138 | 0.000 |
| 14.00 | 14.00 | 22.69 | 2.116 | 2.749 | $4-\mathrm{FFf}$ | 0.825 | 1.344 | 2.000 | 3.840 | 4.456 | 0.000 |
| 15.00 | 15.00 | 22.79 | 2.233 | 2.851 | $4-\mathrm{FFf}$ | 0.857 | 1.395 | 2.000 | 3.840 | 4.775 | 0.000 |

Inlet Elevation (invert): $19.94 \mathrm{ft}, \quad$ Outlet Elevation (invert): 18.16 ft
Culvert Length: $70.02 \mathrm{ft}, \quad$ Culvert Slope: 0.0254


## Culvert Performance Curve Plot: Culvert 11

Performance Curve
Culvert: Culvert 11


Water Surface Profile Plot for Culvert: Culvert 11
Crossing - Culvert 11-24" RCP, Design Discharge - 10.0 cfs
Culvert - Culvert 11, Culvert Discharge - 10.0 cfs


## Site Data - Culvert 11

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 19.94 ft
Outlet Station: 70.00 ft
Outlet Elevation: 18.16 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 11

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 11-24" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 5.00 | 22.00 | 3.84 |
| 6.00 | 22.00 | 3.84 |
| 7.00 | 22.00 | 3.84 |
| 8.00 | 22.00 | 3.84 |
| 9.00 | 22.00 | 3.84 |
| 10.00 | 22.00 | 3.84 |
| 11.00 | 22.00 | 3.84 |
| 12.00 | 22.00 | 3.84 |
| 13.00 | 22.00 | 3.84 |
| 14.00 | 22.00 | 3.84 |
| 15.00 | 22.00 | 3.84 |

Tailwater Channel Data - Culvert 11-24" RCP
Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 22.00 ft

## Roadway Data for Crossing: Culvert 11-24" RCP

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 24.07 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## HY-8 Culvert Analysis Report

 PROPOSED CULVERT 12Table 1-Summary of Culvert Flows at Crossing: Culvert 12-30" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 12 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 21.37 | 5.00 | 5.00 | 0.00 | 1 |
| 21.39 | 6.00 | 6.00 | 0.00 | 1 |
| 21.42 | 7.00 | 7.00 | 0.00 | 1 |
| 21.44 | 8.00 | 8.00 | 0.00 | 1 |
| 21.47 | 9.00 | 9.00 | 0.00 | 1 |
| 21.51 | 10.00 | 10.00 | 0.00 | 1 |
| 21.54 | 11.00 | 11.00 | 0.00 | 1 |
| 21.58 | 12.00 | 12.00 | 0.00 | 1 |
| 21.62 | 13.00 | 13.00 | 0.00 | 1 |
| 21.67 | 14.00 | 14.00 | 0.00 | 1 |
| 21.71 | 15.00 | 15.00 | 0.00 | 1 |
| 23.97 | 40.73 | 40.73 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 12-30" RCP


Table 2 - Culvert Summary Table: Culvert 12

| Total Discharge (cfs) | Culvert Discharge (cfs) | Headwater Elevation (ft) | Inlet Control Depth (ft) | Outlet Control Depth (ft) | Flow <br> Type | Normal Depth (ft) | Critical Depth (ft) | Outlet Depth (ft) | Tailwater Depth (ft) | Outlet Velocity (ft/s) | Tailwater Velocity (ft/s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.00 | 5.00 | 21.37 | 1.014 | 1.975 | 3-M1t | 0.959 | 0.735 | 2.040 | 2.000 | 1.166 | 0.000 |
| 6.00 | 6.00 | 21.39 | 1.117 | 1.994 | 3-M1t | 1.061 | 0.804 | 2.040 | 2.000 | 1.399 | 0.000 |
| 7.00 | 7.00 | 21.42 | 1.213 | 2.017 | 3-M1t | 1.157 | 0.869 | 2.040 | 2.000 | 1.632 | 0.000 |
| 8.00 | 8.00 | 21.44 | 1.314 | 2.043 | 3-M1t | 1.253 | 0.935 | 2.040 | 2.000 | 1.865 | 0.000 |
| 9.00 | 9.00 | 21.47 | 1.416 | 2.073 | 3-M1t | 1.345 | 1.000 | 2.040 | 2.000 | 2.099 | 0.000 |
| 10.00 | 10.00 | 21.51 | 1.512 | 2.106 | 3-M1t | 1.436 | 1.052 | 2.040 | 2.000 | 2.332 | 0.000 |
| 11.00 | 11.00 | 21.54 | 1.604 | 2.142 | 3-M1t | 1.529 | 1.104 | 2.040 | 2.000 | 2.565 | 0.000 |
| 12.00 | 12.00 | 21.58 | 1.693 | 2.180 | 3-M1t | 1.624 | 1.156 | 2.040 | 2.000 | 2.798 | 0.000 |
| 13.00 | 13.00 | 21.62 | 1.778 | 2.222 | 3-M1t | 1.718 | 1.208 | 2.040 | 2.000 | 3.031 | 0.000 |
| 14.00 | 14.00 | 21.67 | 1.860 | 2.267 | 3-M1t | 1.825 | 1.259 | 2.040 | 2.000 | 3.264 | 0.000 |
| 15.00 | 15.00 | 21.71 | 1.940 | 2.315 | 3-M1t | 1.937 | 1.302 | 2.040 | 2.000 | 3.498 | 0.000 |

Inlet Elevation (invert): $19.40 \mathrm{ft}, \quad$ Outlet Elevation (invert): 19.29 ft
Culvert Length: $86.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0013
**************************************************************************************)

## Culvert Performance Curve Plot: Culvert 12

Performance Curve
Culvert: Culvert 12


Water Surface Profile Plot for Culvert: Culvert 12
Crossing - Culvert 12 - $30^{\prime \prime}$ RCP, Design Discharge - 10.0 cfs
Culvert - Culvert 12, Culvert Discharge - 10.0 cfs


## Site Data - Culvert 12

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 19.40 ft
Outlet Station: 86.00 ft
Outlet Elevation: 19.29 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 12

Barrel Shape: Circular
Barrel Diameter: 2.50 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 12-30" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 5.00 | 21.33 | 2.00 |
| 6.00 | 21.33 | 2.00 |
| 7.00 | 21.33 | 2.00 |
| 8.00 | 21.33 | 2.00 |
| 9.00 | 21.33 | 2.00 |
| 10.00 | 21.33 | 2.00 |
| 11.00 | 21.33 | 2.00 |
| 12.00 | 21.33 | 2.00 |
| 13.00 | 21.33 | 2.00 |
| 14.00 | 21.33 | 2.00 |
| 15.00 | 21.33 | 2.00 |

Tailwater Channel Data - Culvert 12-30" RCP
Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 21.33 ft
Roadway Data for Crossing: Culvert 12-30" RCP
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 23.97 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

# HY-8 Culvert Analysis Report 

PROPOSED CULVERT 13

Culvert \#13 is part of the storm sewer system east of Marie Street. Results for existing conditions indicate overtopping of roadway where no problems are reported. Either runoff shifts to nearby inlet or basin area is different than assumed. Large pipe for proposed condition assumes downstream portion of storm sewer system is upsized to handle. Roadway profile affects peak stage if overtopping is present.

Table 1 - Summary of Culvert Flows at Crossing: Culvert 13-36" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 13 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 20.46 | 40.00 | 40.00 | 0.00 | 1 |
| 20.94 | 48.00 | 48.00 | 0.00 | 1 |
| 21.50 | 56.00 | 56.00 | 0.00 | 1 |
| 22.25 | 64.00 | 64.00 | 0.00 | 1 |
| 23.11 | 72.00 | 72.00 | 0.00 | 1 |
| 24.09 | 80.00 | 80.00 | 0.00 | 1 |
| 24.48 | 83.00 | 83.00 | 0.00 | 1 |
| 24.62 | 96.00 | 83.99 | 11.86 | 7 |
| 24.66 | 104.00 | 84.33 | 19.57 | 5 |
| 24.70 | 112.00 | 84.63 | 27.21 | 4 |
| 24.74 | 120.00 | 84.90 | 35.01 | 4 |
| 24.50 | 83.12 | 83.12 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 13-36" RCP


Table 2 - Culvert Summary Table: Culvert 13

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40.00 | 40.00 | 20.46 | 3.301 | 3.447 | 2-M2c | 3.000 | 2.056 | 2.059 | 2.020 | 7.735 | 0.000 |
| 48.00 | 48.00 | 20.94 | 3.849 | 3.935 | 2-M2c | 3.000 | 2.247 | 2.256 | 2.020 | 8.417 | 0.000 |
| 56.00 | 56.00 | 21.50 | 4.490 | 4.488 | 7-M2c | 3.000 | 2.421 | 2.427 | 2.020 | 9.132 | 0.000 |
| 64.00 | 64.00 | 22.25 | 5.240 | 5.143 | 7-M2c | 3.000 | 2.550 | 2.568 | 2.020 | 9.971 | 0.000 |
| 72.00 | 72.00 | 23.11 | 6.104 | 5.826 | 7-M2c | 3.000 | 2.678 | 2.685 | 2.020 | 10.795 | 0.000 |
| 80.00 | 80.00 | 24.09 | 7.080 | 6.600 | 7-M2c | 3.000 | 2.807 | 2.775 | 2.020 | 11.778 | 0.000 |
| 83.00 | 83.00 | 24.48 | 7.474 | 6.904 | 7-M2c | 3.000 | 2.855 | 2.883 | 2.020 | 11.985 | 0.000 |
| 96.00 | 83.99 | 24.62 | 7.607 | 7.007 | 7-M2c | 3.000 | 2.871 | 2.915 | 2.020 | 12.061 | 0.000 |
| 104.00 | 84.33 | 24.66 | 7.653 | 7.042 | 7-M2c | 3.000 | 2.876 | 2.922 | 2.020 | 12.094 | 0.000 |
| 112.00 | 84.63 | 24.70 | 7.693 | 7.072 | 7-M2c | 3.000 | 2.881 | 2.927 | 2.020 | 12.126 | 0.000 |
| 120.00 | 84.90 | 24.74 | 7.730 | 7.100 | 7-M2c | 3.000 | 2.885 | 2.932 | 2.020 | 12.155 | 0.000 |

Inlet Elevation (invert): $17.01 \mathrm{ft}, \quad$ Outlet Elevation (invert): 16.95 ft
Culvert Length: $60.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0010

## Culvert Performance Curve Plot: Culvert 13

Performance Curve
Culvert: Culvert 13


Culvert - Culvert 13, Culvert Discharge - 83.0 cfs


## Site Data - Culvert 13

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 17.01 ft
Outlet Station: 60.00 ft
Outlet Elevation: 16.95 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 13

Barrel Shape: Circular
Barrel Diameter: 3.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 13-36" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 40.00 | 19.00 | 2.02 |
| 48.00 | 19.00 | 2.02 |
| 56.00 | 19.00 | 2.02 |
| 64.00 | 19.00 | 2.02 |
| 72.00 | 19.00 | 2.02 |
| 80.00 | 19.00 | 2.02 |
| 83.00 | 19.00 | 2.02 |
| 96.00 | 19.00 | 2.02 |
| 104.00 | 19.00 | 2.02 |
| 112.00 | 19.00 | 2.02 |
| 120.00 | 19.00 | 2.02 |

Tailwater Channel Data - Culvert 13-36" RCP
Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 19.00 ft

## Roadway Data for Crossing: Culvert 13-36" RCP

Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 24.50 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

HY-8 Culvert Analysis Report
PROPOSED CULVERT 14

Table 1 - Summary of Culvert Flows at Crossing: Culvert 14-24" RCP

| Headwater Elevation <br> (ft) | Total Discharge (cfs) | Culvert 14 Discharge <br> (cfs) | Roadway Discharge <br> (cfs) | Iterations |
| :---: | :---: | :---: | :---: | :---: |
| 22.64 | 3.00 | 3.00 | 0.00 | 1 |
| 22.68 | 4.30 | 4.30 | 0.00 | 1 |
| 22.75 | 5.60 | 5.60 | 0.00 | 1 |
| 22.76 | 6.90 | 6.90 | 0.00 | 1 |
| 22.83 | 8.20 | 8.20 | 0.00 | 1 |
| 22.90 | 9.50 | 9.50 | 0.00 | 1 |
| 22.94 | 10.00 | 10.00 | 0.00 | 1 |
| 23.09 | 12.10 | 12.10 | 0.00 | 1 |
| 23.20 | 13.40 | 13.40 | 0.00 | 1 |
| 23.32 | 14.70 | 14.70 | 0.00 | 1 |
| 23.46 | 16.00 | 16.00 | 0.00 | 1 |
| 25.00 | 26.75 | 26.75 | 0.00 | Overtopping |

Rating Curve Plot for Crossing: Culvert 14-24" RCP


Table 2 - Culvert Summary Table: Culvert 14

| Total <br> Discharge <br> $(\mathrm{cfs})$ | Culvert <br> Discharge <br> $(\mathrm{cfs})$ | Headwater <br> Elevation <br> (ft) | Inlet Control <br> Depth (ft) | Outlet <br> Control <br> Depth (ft) | Flow <br> Type | Normal <br> Depth (ft) | Critical <br> Depth (ft) | Outlet <br> Depth (ft) | Tailwater <br> Depth (ft) | Outlet <br> Velocity <br> $(\mathrm{ft/s})$ | Tailwater <br> Velocity <br> $(\mathrm{ft/s})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3.00 | 3.00 | 22.64 | 0.832 | 1.935 | 3-M1f | 0.727 | 0.604 | 2.000 | 2.000 | 0.955 | 0.000 |
| 4.30 | 4.30 | 22.68 | 1.009 | 1.982 | 3-M1f | 0.888 | 0.722 | 2.000 | 2.000 | 1.369 | 0.000 |
| 5.60 | 5.60 | 22.75 | 1.193 | 2.045 | $3-\mathrm{M1f}$ | 1.038 | 0.833 | 2.000 | 2.000 | 1.783 | 0.000 |
| 6.90 | 6.90 | 22.76 | 1.357 | 2.060 | $4-\mathrm{FFf}$ | 1.182 | 0.927 | 2.000 | 2.000 | 2.196 | 0.000 |
| 8.20 | 8.20 | 22.83 | 1.508 | 2.125 | $4-\mathrm{FFf}$ | 1.331 | 1.018 | 2.000 | 2.000 | 2.610 | 0.000 |
| 9.50 | 9.50 | 22.90 | 1.651 | 2.203 | $4-\mathrm{FFf}$ | 1.495 | 1.097 | 2.000 | 2.000 | 3.024 | 0.000 |
| 10.00 | 10.00 | 22.94 | 1.705 | 2.235 | $4-\mathrm{FFf}$ | 1.562 | 1.128 | 2.000 | 2.000 | 3.183 | 0.000 |
| 12.10 | 12.10 | 23.09 | 1.929 | 2.391 | $4-\mathrm{FFf}$ | 2.000 | 1.247 | 2.000 | 2.000 | 3.852 | 0.000 |
| 13.40 | 13.40 | 23.20 | 2.072 | 2.502 | $4-\mathrm{FFf}$ | 2.000 | 1.313 | 2.000 | 2.000 | 4.265 | 0.000 |
| 14.70 | 14.70 | 23.32 | 2.221 | 2.625 | $4-\mathrm{FFf}$ | 2.000 | 1.380 | 2.000 | 2.000 | 4.679 | 0.000 |
| 16.00 | 16.00 | 23.46 | 2.380 | 2.758 | $4-\mathrm{FFf}$ | 2.000 | 1.438 | 2.000 | 2.000 | 5.093 | 0.000 |

Inlet Elevation (invert): $20.70 \mathrm{ft}, \quad$ Outlet Elevation (invert): 20.59 ft
Culvert Length: $60.00 \mathrm{ft}, \quad$ Culvert Slope: 0.0018
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## Culvert Performance Curve Plot: Culvert 14

Performance Curve
Culvert: Culvert 14


## Water Surface Profile Plot for Culvert: Culvert 14

Crossing - Culvert 14-24" RCP, Design Discharge - 10.0 cfs
Culvert - Culvert 14, Culvert Discharge - 10.0 cfs


## Site Data - Culvert 14

Site Data Option: Culvert Invert Data
Inlet Station: 0.00 ft
Inlet Elevation: 20.70 ft
Outlet Station: 60.00 ft
Outlet Elevation: 20.59 ft
Number of Barrels: 1

## Culvert Data Summary - Culvert 14

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in
Barrel Manning's n: 0.0120
Inlet Type: Conventional
Inlet Edge Condition: Square Edge with Headwall
Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert 14-24" RCP)

| Flow (cfs) | Water Surface Elev (ft) | Depth (ft) |
| :---: | :---: | :---: |
| 3.00 | 22.60 | 2.00 |
| 4.30 | 22.60 | 2.00 |
| 5.60 | 22.60 | 2.00 |
| 6.90 | 22.60 | 2.00 |
| 8.20 | 22.60 | 2.00 |
| 9.50 | 22.60 | 2.00 |
| 10.00 | 22.60 | 2.00 |
| 12.10 | 22.60 | 2.00 |
| 13.40 | 22.60 | 2.00 |
| 14.70 | 22.60 | 2.00 |
| 16.00 | 22.60 | 2.00 |

## Tailwater Channel Data - Culvert 14-24" RCP

Tailwater Channel Option: Enter Constant Tailwater Elevation
Constant Tailwater Elevation: 22.60 ft
Roadway Data for Crossing: Culvert 14-24" RCP
Roadway Profile Shape: Constant Roadway Elevation
Crest Length: 100.00 ft
Crest Elevation: 25.00 ft
Roadway Surface: Paved
Roadway Top Width: 32.00 ft

## APPENDIX C

## STRAIGHT LINE DIAGRAMS





[^0]:    ${ }^{(1)}$ Stormsewer conveyance pipe

[^1]:    ${ }^{\text {a }}$ Weighted coefficient based on percentage of impervious surfaces and green areas must be selected for each site.
    ${ }^{\mathrm{b}}$ Coefficients assume good ground cover and conservation treatment.
    ${ }^{c}$ Depends on depth and degree of permeability of underlying strata.
    Note: $\quad$ SFR $=$ Single Family Residential
    MFR = Multi-Family Residential

